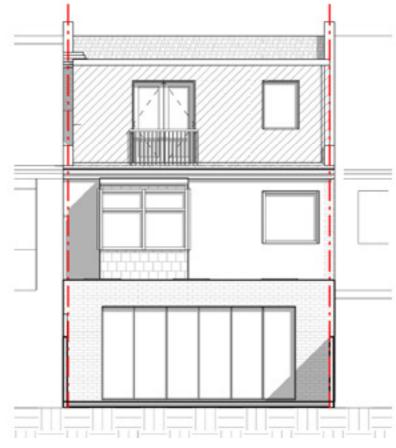


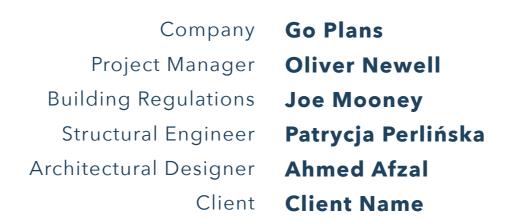
# S S ш ADDR PROJECT





# SCOPE OF WORK

# PROJECT INFORMATION



# JOB DESCRIPTION

Single storey rear extension New kitchen, shower room & utility and all associated works

This package contains the scope of works and mechanical and electrical design documents required for construction pricing.

For any further questions, please refer to Go Plans immediately.

# PLANNING PROPOSAL

Existing Plan

Proposed Plan

# BUILDING REGULATIONS

Building Regulations Drawing

STRUCTURAL ENGINEERING Structural Engineering Plan

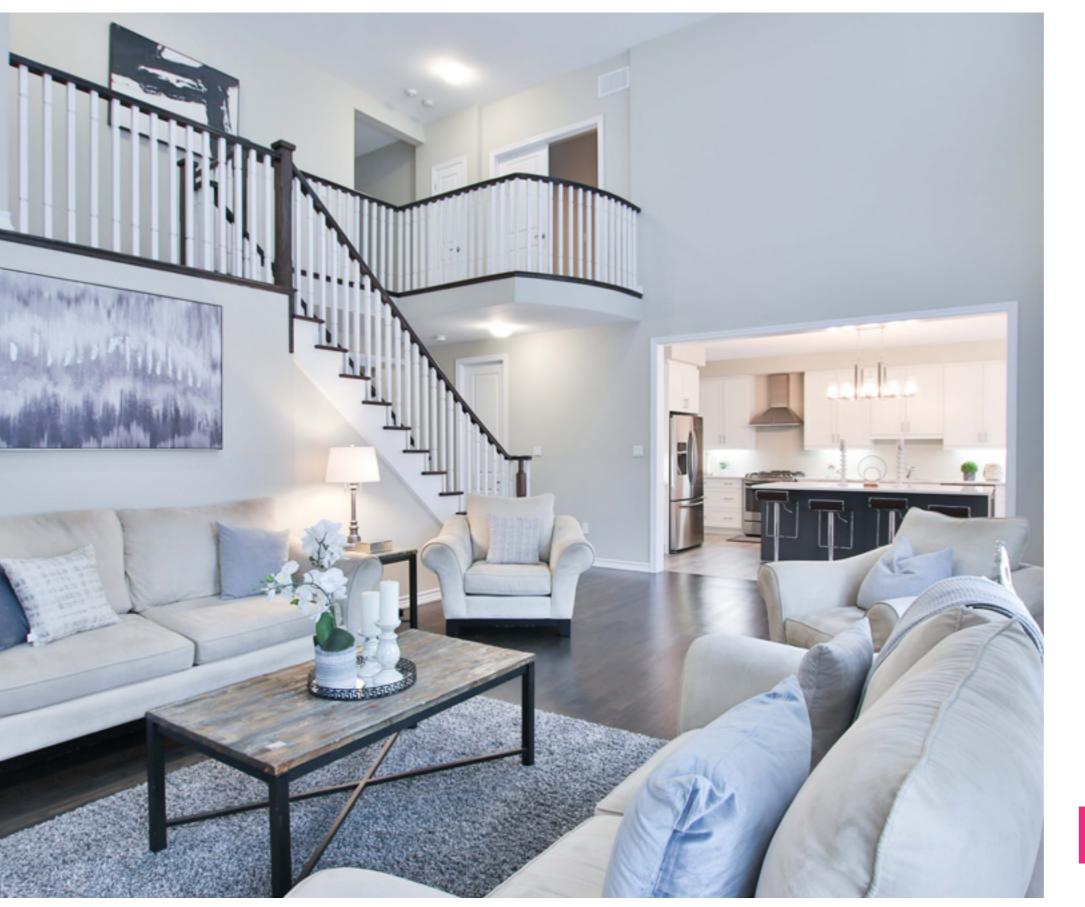
W&D PLANS Window & Door Plan

# M&E PLANS Plumbing Plan Electrical Plan

# FIXTURES, FITTINGS & FINISHES

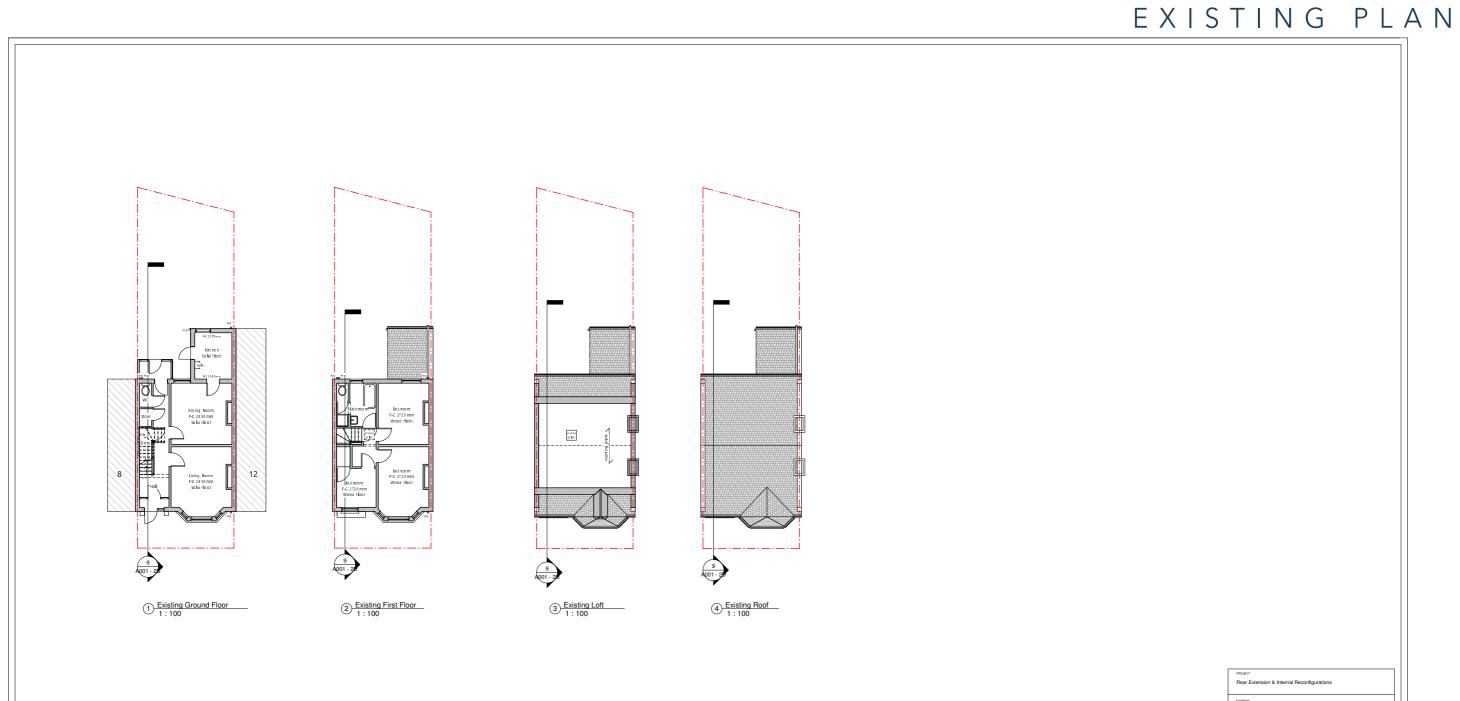
# SITE INFORMATION

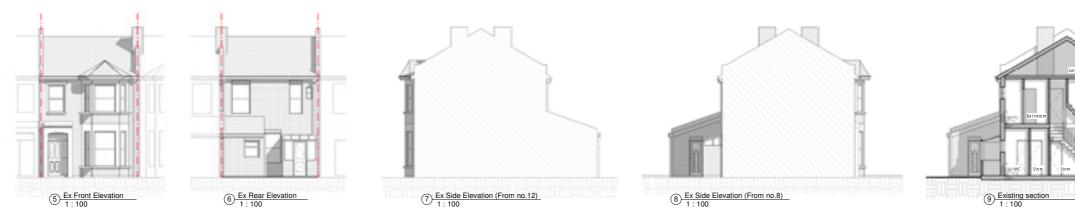
# goplans



PROJECT ADDRESS

# PLANNING PROPOSAL

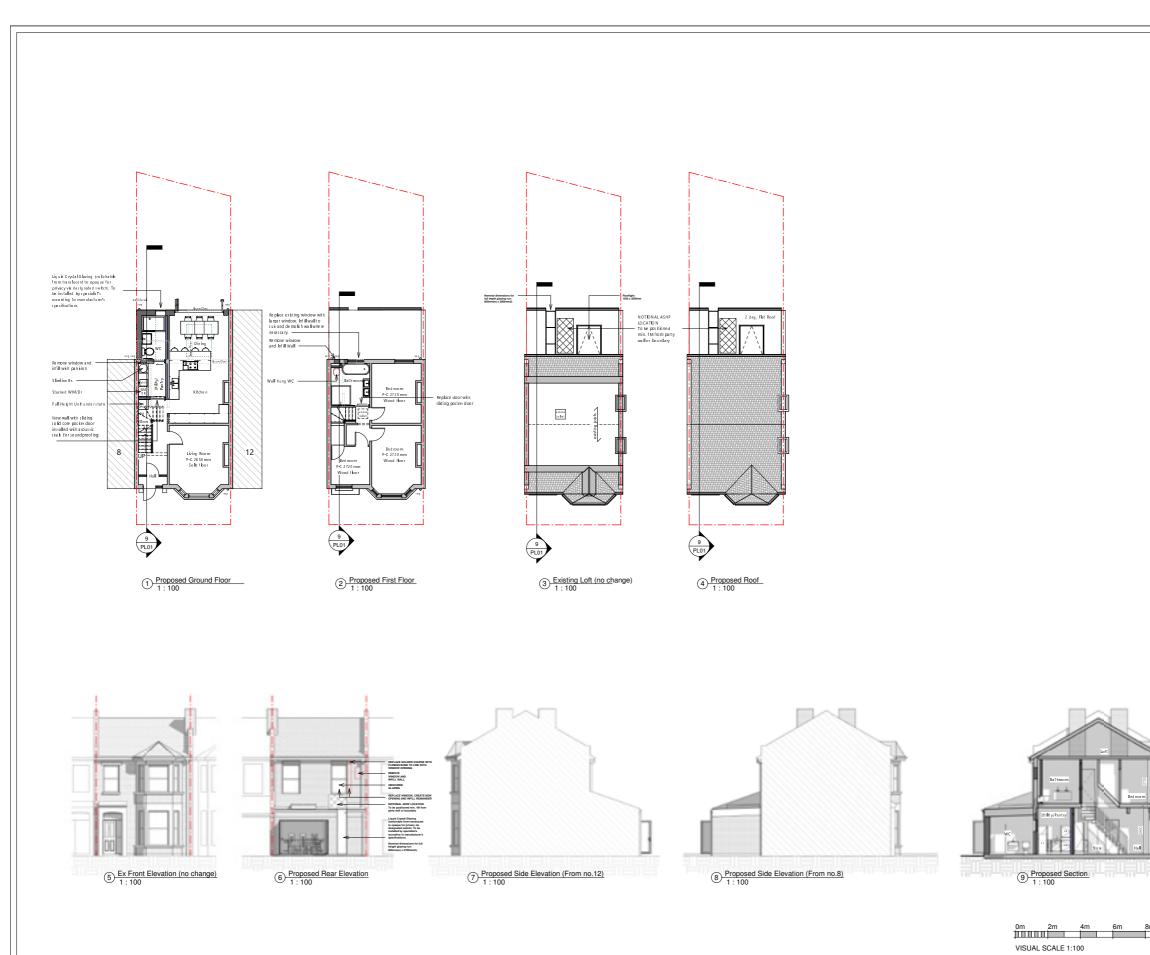




0m 2m 4m



PROJECT		
Rear Extension & Inter	nal Reconfigurations	
ADDRESS		
10 Trelawn Road, Lond	ion E10 5QD	
CLIENT NAME		
D. Verrall		
PROJECT STATUS		
Project Status		
SHEET N.	DRAWING TITLE	
A001 - 2D	Existing Drawings	
DESIGNED BY:	DRAWN BY:	CHECKED BY:
Goplans	KC	Goplans
DATE:	SCALE	
05/11/2024	As In	dicated @ A1
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Item above cut		
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All dimensions to be cross-checked o	n site prior to completing drawings for	a party wall process, ordering and/or
structural purposes		
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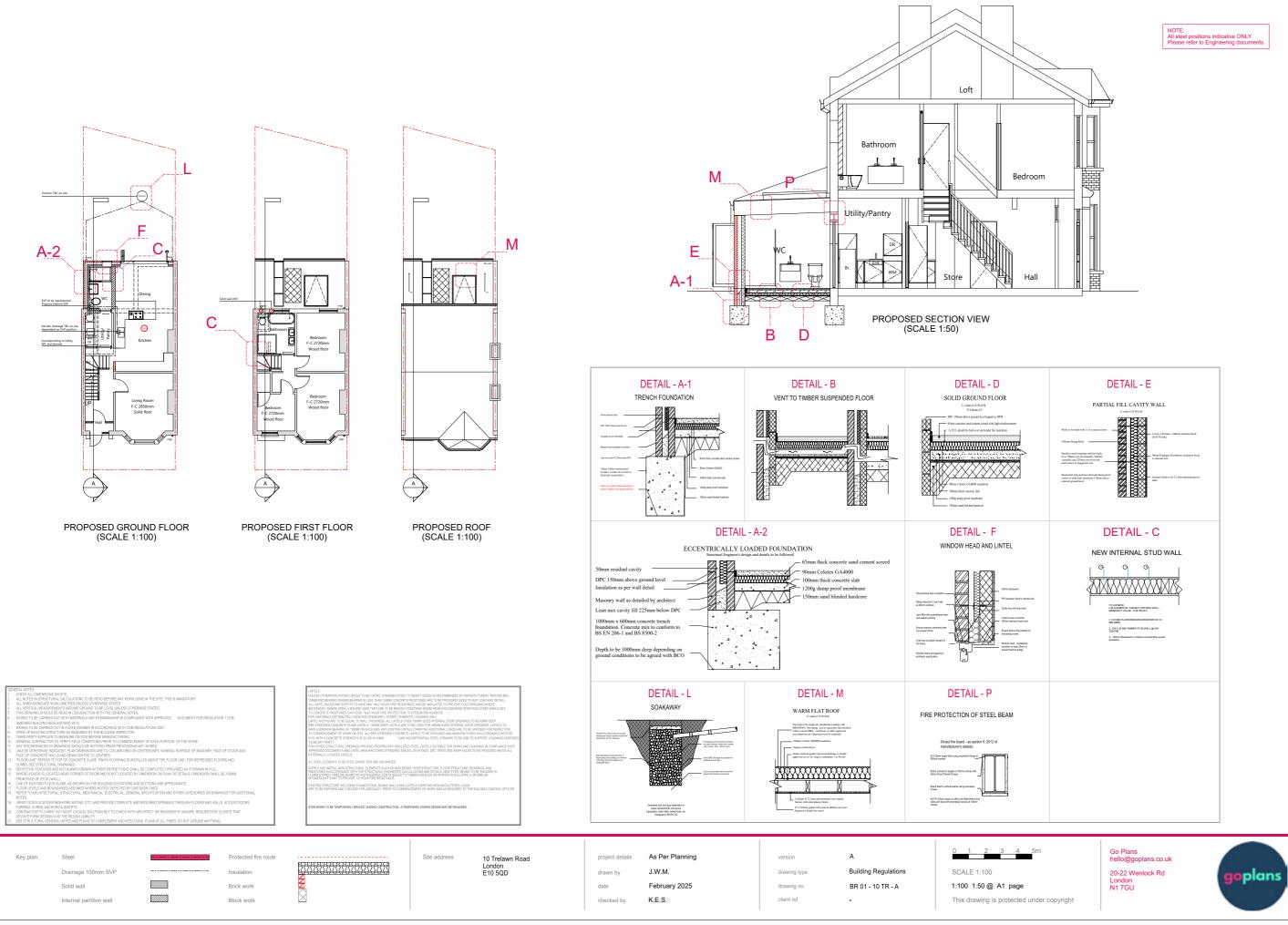
# PROPOSED PLAN

	Rev: Description: PL1 Externalglazing to incorporated. Prev window removed.		Drawn by: Date: AA 22.01.25
	MOJECT Single Storey Rear Ext Reconfiguration	tension and Internal	
	ADDRESS 10 Trelawn, London, E CLENT NAME D. Verrall PROJECT STATUS Planning	10 5QD	
	SHEET N.	DRAWING TITLE	
	PL01	Proposed Drawings	
12	DESIGNED BY:	DRAWN BY: AA	CHECKED BY:
	Goplans DATE:	SCALE	Goplans
T1	17/12/2024		dicated @ A1
-	Demolished exis	Un	undproofing its below a party wall process, ordering and/or
3m 10m		pla	
	doplans.co	uk   0203	633 0928



# PROJECT ADDRESS

BUILDING REGULATIONS





NOTICE OF COMMENCEMENT A notice of commencement is to be submitted to Building Control within 5 days of work being regarded as commenced, under regulation 16 of The Building Regulations etc. (Amendment) (England) Regulations 2010. Work will be deemed to have commenced when the build has progressed to at least one of the following:

For complex buildings – Foundations are constructed, and the structure of the lowest floor level is complete. For new buildings and horizontal extensions - Sub surface structure of the building or the extension including all foundations and the structure of the ground floor level is completed. For all other works – constructed 15% of the overall work.

## CDM REGULATIONS 2015

CDM REGULATIONS 2015 The client must abide by the Construction Design and Management Regulations 2015. The Client must appoint a Contractor, if more than one Contractor is to be involved, the Client will need to appoint (in writing) a Principal Designer (to plan, manage and coordinate the planning and design work), and a Principal Contractor (to plan, manage and coordinate the construction and ensure there are arrangements in place for managing and organising the project).

### Domestic Clients

DOMESING CARENTS The Domestic Client is to appoint a Principal Designer and a Principal Contractor when there is more than one Contractor, if not your duties will automatically be transferred to the Contractor or Principal Contractor

### The Designer can take on the duties, provided there is a written agreement between you and the Designer to do so.

The Health and Safety Executive is to be notified as soon as possible before construction work starts if the works:

(a) Last longer than 30 working days and has more than 20 workers working simultaneously at any point in the project

### b) Exceeds 500 person days.

PARTY WALL ACT Should they need to do so under the requirements of the Party Wall Act 1996, the owner has a duty to serve a Party Structure Notice on any adjoining owner if the building work involves any of the following to a Party Wall: - Insertion of DPC through wall - Raising a wall or cutting off projections - Demolition and rebuilding In-serving

- Underpinning - Insertion of lead flashings

A Party Wall Notice is also required for: - Any excavations within 3 metres of any part of a neighbouring owner's building or structure, where any part of that work will go deeper than the neighbour's foundations; or - Any excavations for a new building or structure, within 6 metres of any part of a neighbouring owner's building or structure, where any part of that work will meet a line drawn downwards at 45° in the direction of the excavation from the bottom of the neighbour's foundations; see diagram 7 in the following Government guidance, https://www.gov.uk/government/publications/preventing-and-resolving-disputes-in-relation-to-party-wall-stt-act-1996-explanatory-booklet#para\_28

### A Party Wall Agreement is to be in place prior to start of works on site.

### THERMAL BRIDGING

Care shall be taken to limit the occurrence of thermal bridging in the insulation layers caused by gaps within the thermal element, (i.e. around windows and door openings). Reasonable growing on shall also he made to ensure the extension is cognizivated to minimise junvanted at leafagee through the new builtion fabric.

### MATERIALS AND WORKMANSHIP

MATERIALS AND WORKMANSHIP All works are to be carried out in a workmanike manner. All materials and workmanship must comply with Regulation 7 of the Building Regulations, all relevant British Standards, European Standards, Agreement Certificates, Product Certification of Schemes (Kite Marks) etc. Products conforming to a European technical standard or harmonised European should have a CE marking. The latest edition of the British Standard (including any amendments) applies to any undated references within these specifications.

### SITE PREPARATION

SILE TREEPARTNING Ground to be prepared for new works by removing all unsuitable material, vegetable matter and tree or shrub roots to a suitable depth to prevent future growth. Seal up, cap off, disconnect and remove existing redundant services as necessary. Reasonable precautions must also be taken to avoid danger to health and safety caused by contaminants and ground gases, e.g. familit gases, radio, unamilit gases, radio, vapours etc. or or in the ground overed, or to be covered by the building.

EXISTING STRUCTURE Existing structure including foundations, beams, walls and lintels carrying new and altered loads are to be exposed and checked for adequacy prior to commencement of work and as

and install new structural elements such as new beams, roof structure, floor structure, bearings, and padstones in accordance with the Structural Engineer's calculations and New steel beams to be encased in 12.5mm Gyproc FireLme board with staggered joints, Gyproc FireCase or painted in Nutilifies S or similar intumescent paint to provide 1/2 hour tance, as agreed with Building Control. All fire protection to be installed as detailed by specialist manufacturer. Supply and install r details. New steel b fire resistance, as a

STRAPPING OF FLOORS S IXAPPING OF FLOORS Lateral restraint to be provided where joists run parallel to walls. Floors to be strapped to walls at max 2.0m centres with 1200mm x 30mm x.5mm galvanised mild steel straps or other approved, in compliance with BS EN 845-1 (+A1:2016). Straps to be taken across minimum of 3 joists and built into walls. Provide 38mm wide x % depth solid noggins between joists a strap costion.

FLAT ROOF RESTRAINT 100m x 50mm C16 grade timber wall plates to be strapped to walls using 1200mm x 30mm x 5mm galvanised mild steel straps at maximum 2.0m centres, straps to be fixed to internal wall foce.

## OPENINGS AND RETURNS An opening or recess greater than 0.1m<sup>2</sup> shall be at least 550mm from the supported wall (measured internally).

An Opening of recess greater that 0. In a share de a reast Johnin Holl the supported wan (measured internally). - For uniformly distributed loads and standard 2 storey domestic loadings only Lintel width are to be equal to will thickness. All finels over 750mm sized internal door openings to be 65mm deep pre-stressed concrete plank lintels. 150mm deep intels are to be used for 900mm sized internal door openings. Lintels to have a minimum bearing of 150mm on each end. Any existing lintels carrying additional loads are to be exposed for inspection at commencement of work on site. All pre-stressed concrete lintels to be designed and manufactured in accordance with BS H 1992-1-12023 Eurocode 2, with a concrete strength of 50 or 40 Nmm<sup>2</sup> and incorporating steel strands to BS 5896 to support loadings assessed to BS EN 845-22013. For other structural openings provide providerary insulated steel lintels suitable for spans and loadings in compliance with Approved Document A and lintel manufactured's Stop ends, DPC trays and weep holes to be provided above all externally located lintels. Uniteds only supporting a roof, lintels to be encased in 12 Smm Opyroc FireLine board with staggered joints, Opyroc FireCase or painted in Nutliffer S or similar intumescent pain to provide 1/2 hour fire resistance. All fire protections to be installed as detailed by specialist manufacturer.

### STEEL LINTELS

STEEL LINTELS Linkel and linkel installation to be in accordance with BS 5977-1 Linkels. Method of assessment of load and BS EN 845-2 Specification for ancillary components for masonry. Linkel to be galvanised steel, powder coated linkel, such as Cathic, with a built-in damp-proof ocurse. The linkel to be wide encough to provide adequates support to the valing above, to be installed with a nominal 150 mm bearing area at each end and be fully bedded on a solid bed of motar. Only full bricks or blocks to be part of the bearing area - linkels not to be placed directly onto part bricks. Padatones and spreaders to be provided under the bearings, where required. Installation to be in accordance with mandicture's recommendations. Or an of any many of the back manufacture's recommendations. Or all on of any many the back manufacture's recommendations. He manufacturer around and all the back on the back of the window head externally.

Risk of condensation at potential cold bridges to be minimised, wall insulation should abut the head of the window frame and insulation to be provided at the underside of the lintel unless the manufacture produces an allemantative. (In severely exposed locations or where the lintel does not offer a built-in DPC, a separate membrane to be fitted, turned up at the edge to ensure the water is not directed into the cavity. For casatal areas, the use of soffic idading to also be considered to provide further protection). Unless only supporting a roof, lintels to be encased in 12.5mm Gyproc FireIne board with staggered joints, Gyproc FireCase or painted in Nullifire S or similar intumescent paint to provide 1/2 hour fire resistance. All fire protection to be installed as detailed by specialist manufacturer.

### TRENCH FOUNDATION

TRENCH FOUNDATION Provide 750mm thick trench fill concrete foundations with a minimum width equal to the width of the wall plus 300mm. Concrete mix to conform to BS EN 206:2013 (+A2:2021) and BS 8004:2015 Code of practice for foundations (+A1:2020). All foundations to be a minimum of 1000mm below ground level, depth and size of foundation to be approved on site by Building Control to suit alle conditions. All constructed in accordance with 2010 Building Regulations A1/2 and BS 8004-Code of Practice for Foundations (+A1:2020). Ensure foundations are constructed below invert level of any adjacent draine. Base of foundations supporting internal walls to be min 600mm below ground level. Sulphate resistant carent to be used if require Please note that should any adverse soil conditions or difference in soil type be found, or any major tree roots in excavations, Building Control to be contacted and the advice of a Structural Engineer should be sought.

PIPES PASSING THROUGH TRENCH FOUNDATIONS. The load-bearing capability of foundations must not be affected where services pass through. The pipe work to be seleved. Frexible material to be provided around pipe and flexible joints to be provided where pipes exit the foundation.

Atternatively Pipework should pass through a suitably strengthened opening in the foundation, i.e. foundation shuttered and a provided with suitable lintel over the pipe allowing for sufficient space for movement to ensure that the drain is capable of maintaining line and gradient. Opening should be masked with granular backfill (pea shingle) around pipe. DPC to be provided, as required by Building Control. Advice from the Structural Engineer to be sought on suitability of pipe running through foundation before construction.

PIPES PASSING THROUGH WALLS

PIPES PASSING THROUGH WALLS Walls above pipes passing through substructure walls to be supported on suitable lintel on semi-engineering bricks. Pipe to be provided with a 50mm clearance all round, opening to be masked with granular backfill (pea shingle) around pipe. DPC to be provided, as required by Building Control. Alternatively Where new pipework passes through external walls the pipe work is to be provided with 'rocker pipes' at a distance of 150mm either side of the wall face. The 'rocker pipes' must have fiestibe joints and be a maximum length of 600mm.

SOLID FLOOR INSULATION OVER SLAB To meet min U value required of 0.18 W/m<sup>2</sup>K

Steel

Solid wall

Drainage 100mm SVP

Internal partition wall

Key plan:

10 meet min U value required or U.1s w/mrk PArtatio 26 PARTATION PARTA GAPUOU insulaution. Sizmin insulaution to continue around floor perimeters to avoid thermal bridging. A VCL should be laid over the insulation boards and turned up 100mm at room perimeters behind the skirting, all joints to be lapped by 150mm and sealed. Finish with 65mm sand/cement finishing screed with light mesh reinforcement. Where drain purs pass under person floor, provide AI2 mesh 10 mw wide and min 57mm encoreste prover ourse length of drain.

Protected fire route

Insulation

Brick work

Block work

WALLS BELOW GROUND WALLS BELOW GROUND All new walls below ground to be constructed using blockwork compliant with BS EN 771 and suitable for below ground level or semi engineering brickwork. Walls to be built using 1:4 masonry mortar mix or equal approved specification to BS EN 1996-1-1. Cavilies below ground level to be filled with lean mix concrete min 225mm below damp proof course. Or provide lean mix backfill tabse of cavity wall (150m below damp course) aid to fail to veepholes.

PARTIAL FILL CAVITY WALL To achieve minimum U Value of 0.18 W/m?K Provide 103mm suitable facing brick. Ensure a 50mm clear residual cavity and provide 90mm Kingspan Kooltherm insulation fixed to internal leaf. Inner leaf constructed using 100mm, 0.45 W/m?K standard block. Internal finish to be 12.5mm plasterboard on dabs. Walls to be built with 1:1:6 cement mortar.

, vide horizontal strip polymer (hyload) damp proof course to both internal and external skins, DPC to be placed a minimum 150mm above external ground level. New DPC to be made inuous with existing DPC's and with floor DPM. Vertical DPC to be installed at all reveals where cavity is closed.

WALL TIES WALL in Its All waits constructed using stainless steel vertical twist type retaining wall lies built in at 750mm drs horizontally, 450mm vertically and 225mm drs at reveals and comers in staggered Mail lies for calvels over 150mm to be suitable for can'ty width, and installed as manufacturer's details.

# CAVITIES Provide cavity trays over openings and where roofs abut walls. All cavities to be closed at eaves and around openings using Thermabate or similar non combustible inst. closers: Provide vertical NPCs around openings and abutments. All cavity trays must have 150mm upstands and suitable cavity weep holes (min 2) at max 900mm cent

CAVITY BARRIERS 30 minute fire resistant cavity barriers to be provided around openings, at tops of walls, gable end walls, vertically at junctions with separating walls and horizontally at separating floors. Cavity trays to be provided over barriers where required. Trays and cavity barriers to be installed according to manufacturer's details.

MOVEMENT JOINTS Movement joints to be provided at the following maximum spacing:

Calay brickwork - 12m. Calay brickwork - 12m. Lightweight concrete block - density not exceeding 1,500kg/m<sup>3</sup> - 6m. Dense concrete block - density exceeding 1,500kg/m<sup>3</sup> - 7.5-9m.

Dense concrete block - density exceeding 1,500kg/m<sup>2</sup> - 7,5-9m. Any masony in a parapet wall (enght to height ratio greater than 3:1) - half the above spacings and 1.5m from corners. Movement joint widths for clay bricks to be not less than 1.3mm/m i.e. 12m - 16mm and for other masony not less than 10mm. Additional movement joints may be required where the aspect ratio of the wall (length -height) is more than 3:1. Considerations to be given to BS EN 1996-1-2:2005 Eurocode 6. Design of masonry structure.

WARM FLAT ROOF

# To achieve U value 0.15 W. Flat roof covering to be sing

leve 0 value 0.15 wimrs of ocwening to be single ply nofing membrane with BROOF(4) fire rating in accordance with BS EN 13501-1:2018 and with a current BBA or other approved accreditation. Roof ng to be laid in compliance with manufacturer's details by flat roofing specialist. Single ply membrane to be fixed to 18mm exterior quality plywood (if required by manufacturer) ove 0mm Celotex XR4000 insulation. ulation bonded to vice on 18mm external quality plywood decking or similar approved on sw firings to minimum 1 in 40 fall on sw treated 47 x 145mm flat roof C24 timber joists at 0mm ctrs to give a max span of 3.22m or as Structural Engineer's details and calculations. Fix 12.5mm plasterboard over vapour barrier to underside of joists, finish a with plaster skim

Provide cavity tray where new roof abuts existing house. Provide restraints to fair toof by tigging of 30 x 5 x 120mm ms galvanised lateral restraint straps at maximum 2000mm centres fixed to 100 x 50mm wall plates and anchored to wall. THIS IS A GENERAL GUIDE BASED ON NORMAL LOADING CONDITIONS FOUND IN DOMESTIC CONSTRUCTION. IT IS YOUR RESPONSIBILITY TO ASSESS YOUR DESIGN TO ASCERTIAIN WHETHER ENGINEER'S DETAILSCALCULATIONS ARE REQUIRED. PLEASE REFER TO THE TRADA DOCUMENT – SPAN TABLES FOR SOLID TIMBER MEMBERS IN FLOORS, CELINGS AND ROOTS FOR DWELLINGS OR ASK YOUR STRUCTURAL ENGINEER FOR ADVICE.

# LEAD WORK AND FLASHINGS All lead flashings, any valleys or seakers to be Code 5 lead and laid in accordance with BS 5534 and BS EN 12588. Flashings to be provided to all jambs and below window openings with welded upstands. Joints to be lapped min 150mm and lead to be dressed 200mm under tiles, etc.

INTERNAL STUD PARTITIONS 100mm x 50mm softwood treated timbers studs at 400mm ctrs with 50 x 100mm head and sole plates and solid intermediate horizontal noggins at 1/3 height or 450mm c/cs. Provide min 10kg/m<sup>2</sup> density accustic soundproof quilt tightly packed (e.g. 100mm Rockwool or Isowool mineral fibre sound insulation) in all voids the full depth of the stud. Partitions to be built off doubled up joists where partitions run parallel or provide noggins where at right angles, or to be built off DPC on thickneed concrete siab if solid ground floor. Walls faced throughout with 12.5mm plasterboard with skim plaster finish. Plasterboard to be taged and jointed complete with beaks and stops.

## ELECTRICAL All electrical work required to meet the requirements of Part P (electrical safety) must be designed, installed, inspected and tested by a Competent Person registered under a Competent Person Self Certification Scheme such as BRE certification Ltd, BSI, NICEIC Certification Services or Zurich Ltd. An appropriate BS7671 Electrical Installation Certificate is to be issued for the work by a person competent to do so. A covor da certificate will be diven to Building Control on completion.

INTERNAL LIGHTING NI EXTURL LIGHT INC Install low energy light fittings that only take lamps having a luminous efficiency better than 80 lumens per circuit watt. All fixed to have lighting capacity (Im) 185 x total floor area, to comply with Part L of the current Building Regulations and the Domestic Building Services Compliance Guide.

Extend all heating and hot water services from existing and provide new TRVs to radiators. Heating system to be designed, installed, tested and fully certified by a GAS SAFE registered specialist. All work to be in accordance with the Local Water Authorities bye laws, the Gas Safety (Installation and Use) Regulations 1998 and IEE Regulations. The energy performance of the new components to be assessed. The results should be recorded and given to the building owner. All accessible pipes to be insulated to the standards in Table 4.4 Approved Document L.

SMOKE DETECTION Provide a linked smoke almked smoke almost observed to BS EN 14604 and BS 5839-6-2019 to at least a Grade D2 category LD3 standard. System to be mains powered with battery back At least one smoke detector to be provided in each hallway and landing. In hallways exceeding 7.5m in length, no point within the hallway should exceed 7.5m from the nearest det and no bedroom door should be further than 3m from the nearest smoke alarm. If ceiling mounted they should be 30mm from the walls and light fittings. Where the kitchen area is separated from the stairway or circulation space by a door, there should be an interlinked heat detector in the kitchen. Mains-wired, interlinked heat detector to be provided to the kitchen and smoke detectors to principal living rooms, if required by Building Control. A design, installation, and commissioning certificate for the fire detection and alarm system to be issued to Building Control on the works.

# ACCEPTABLE UNPROTECTED AREAS Unprotected areas more than 1m from the boundary. The unprotected area should not exceed the following



ROOF LIGHTS Min U-value of 2.2 W/m<sup>2</sup>K. RooFlights to be double glazed with 16mm argon gap and soft low-E glass. Roof lights to be fitted in accordance with manufacturer's instructions, with rafters doubled up to sides and suitable flashings provided.

SAFETY GLAZING APE - IT OEDE INFO Ill glazing in critical locations to be toughened or laminated safety glass to BS EN 12600:2002, BS EN 14179 or BS EN ISO 12543-1 and Part K of the current Building Regulations, i.e. within 1500mm above floor level in doors and side panels within 300mm of door opening and within 600mm above floor level in windows.

# NEW AND REPLACEMENT WINDOWS New and replacement windows to be double glazed with 16-20mm argon gap and soft coat low-E glass. Window Energy Rating to be Band B or better and to achieve U-value of 1.4 WinrX. The door and window openings should be limited to 25% of the extension floor area plus the area of any existing openings covered by the extension. Insulated plasterboard to be used in reveals to abut jambs and to be considered within reveal softlis. Fully insulated and continuous cavity closers to be used around reveals. Windows and door frames to be taped to surrounding openings arealing at peel. Windows to be fitted with trickle vents to provide adequate background ventilation in accordance with Approved Document F.

ned and a commissioning notice given to the Building Control Body

### NEW AND REPLACEMENT DOORS

NEW AND REPLACEMENT DOORS New and replacement doors to achieve a U-Value of 1.4Wm<sup>2</sup>K. Glazed areas to be double glazed with 16-20mm argon gap and soft low-E glass. Glass to be toughened or laminated safety glass to BS 6206, BS EN 14179 or BS EN ISO 12543-1 and Part K of the current Building Regulations. Insulated plasthoard to be used in reveals to abuil jambs and to be considered within reveal softis. Fully insulated and continuous cavity closers to be used around reveals. Windows and door frames to be taped to surrounding openings using air sealing tape.

EXTRACT TO BATHROOM Bathroom to have mechanical vent ducted to external air to provide min 15 l/s. Vent to be connected to light switch and to have 15 minute over run if no window in room. Internal doors should be provided with a 10mm gap below the door to aid air circulation. Intermittent extract fans to BS EN 13141-4. All fixed mechanical ventilation systems, where they can be tested and adjusted, shall be commissioned and a commissioning notice given to the Building Control Body.

EXTRACT TO KITCHEN

10 Trelawn Road

E10.50D

Site address

<del>19999999999999999999</del>

EXTRACT TO WC WC to have mechanical ventilation ducted to external air with an extract rating of 15 l/s operated via the light switch. Vent to have a 15min overrun if no window in room. Internal doors should be provided with a 10mm gap below the door to aid air circulation. Intermittent extract fans to BS EN 13141-4. All fixed mechanical ventilation systems, where they can be tested and adjusted, shall be commissioned and a commissioning notice given to the Building Control Body.

To utility room provide mechanical ventilation ducted to external air capable of extracting at a rate of 30 l/s. Internal doors should be provided with a 10mm gap below the door to aid air circulation. Intermittent extract fans to BS EN 13141-4. All fixed mechanical ventilation systems, where they can be tested and adjusted, shall be commissioned and a commissioning notice given to the Building Control Body.

Kitchen to have mechanical ventilation with an extract rating of 60 l/s, or 30 l/s if adjacent to hob to external air. Internal doors should be provided with a 10mm gap below the door to aid air circulation. Intermittent extract fans to BS EN 13141-4. Cooker hoods to BS EN 13141-3. All fixed mechanical ventilation systems, where they can be tested and adjusted, shall be

PURCE VENTILATION Minimum total area of opening in accordance with Table 1.4 Approved Document F1. Hinged or pivot vindows with an opening angle of 15 to 30 degrees to have an openable area in excess 1/10 of the floor area of the room. External doors and asah, hinged or pivot windows with an opening angle of equal to or greater than 30 degrees to have an openable area in excess of 1/20 of the floor area of the room. External doors and asah, hinged or pivot windows with an opening angle of equal to or greater than 30 degrees to have an openable area in excess of 1/20 of the floor area of the room. External doors and asability of the adable of extracting at least 4 air changes per hour per room directly to the outside. Internal doors should be provided with a 10mm gap below the door to aid air circulation.

project details

drawn by

checked by

date

As Per Planning

February 2025

J.W.M.

K.E.S

tion at least 1700mm above floor level to be provided to habitable rooms and kitchens at a rate of min 8,000mm<sup>2</sup>, and to bathrooms at a rate of min Total number of ventilators installed in a dwellings habitable rooms to be at least 4 ventilators for one bedroom dwellings and 5 ventilators for dwellings with more than one bedroom. Tackground ventilators to be tested to BS EN 13141-1.

Background ventilators of between to be Environment of the term of term of

BACKGROUND VENTILATION

Materia The jur

RAINWATER DRAINAGE

PUBLIC SEWER REQUIREMENTS

Special measures may be required for the following:

Other provisions that may apply to Sewers:

EIXED EXTERNAL LIGHTING

А

drawing type

drawing no

client ref

Building Regulations

BR 02 - 10 TR - A

Where the extension connects to in an existing room and as a result the existing room is left with no windows or background ventilation less than 5000mm<sup>2</sup>, then the new room background ventilation to be at least 10 000mm<sup>2</sup> enuivalent area background ventilation to be at least 10.000m<sup>2</sup> equivalent area. Where the extension connects to in an existing room and as a result the existing room is left with background ventilation at least 5000mm<sup>2</sup>, then both the following is to be provided: - Background ventilators of at least 12,000m<sup>2</sup> equivalent area should be provided between the two rooms. - Background ventilators of at least 12,000m<sup>2</sup> equivalent area should be provided between the outside.

C2\_CONDENSATION While, factors and cool of the building to be designed and constructed so that their structural and thermal performance will not be adversely affected by interstitial condensation, surface condensation or mould growth. Account to be taken of the building's form and orientation in relation to topography, prevailing winds, sunlight and over-shadowing, and the rate at which wildly is generated. enable the second of the second of

RAINWATER DRAINAGE New rainwater goods to be new 110mm UPVC half round gutters taken and connected into 68mm dia UPVC downpipes. Rainwater taken to new soakaway, situated a min distance of 5.0m away from any building, via 110mm dia UPVC pipes surrounded in 150mm granular fill. Soakaway to be min of 1 cubic meter capacity (or to depth to Local Authority approval), filled with suitable granular fill and provided with geotextile surround to prevent migration of fines. If necessary carry out a porosity test to determine design and depth of soakaway.

UNDERGROUND FOUL DRAINAGE Underground drainage to consist of 100mm diameter UPVC proprietary pipework to give a 1:40 fall. Surround pipes in 100mm pea shingle. Provide 600mm suitable cover (900mm under drives). Shallow pipes to be covered with 100mm reinforced concrete slab over compressible material. Provide rodding access at all changes of direction and junctions. All below ground drainage to comply with BS EN 1401-1 (+A1:2023).

ABOVE GROUND DRAINAGE All new above ground drainage and plumbing to comply with BS EN 12056-2 for sanitary pipework. All drainage to be in accordance with Part H of the Building Regulations. Wastes to have 75mm deep anti-vac bottle traps and rodding eyes to be provided at changes of direction.

Size of wastes pipes and max length of branch connections (if max length is exceeded then anti-vac traps to be used). Wash basin - 1.7m for 32mm pipe 3m for 40mm pipe. Bath/shower - 3m for 40mm pipe 4m for 50mm pipe. WC - 6m for 100mm pipe for single WC. All branch pipes to connect to 110mm soil and went pipe terminating min 900mm above any openings within 3m. All branch pipes to connect to 110mm soil and vent pipe terminating min 900mm above any openings within 3m. Or to 110mm upvc soil pipe with accessible internal air admittance valve complying with BS EN 12380, placed at a height so that the outlet is above the trap of the highest fitting. Waste pipes not to connect on to SVP within 200mm of the WC connection. Supply hot and cold water to all fittings as appropriate.

SOIL AND VENT PIPE Svp to be extended up in 110mm dia UPVC and to terminate min 900mm above any openings within 3m. Provide a long radius bend at foot of SVP.

HA BUILDING OVER OR NEAR PUBLIC SEWERS The developer is to consult the Local Sewers Undertaker when constructing, extending or underpinning over a sewer or within 3m of the centreline of sewer shown on the sewer undertakers sewer records and when the following applies: - The building or extension is to be constructed over a manhole or inspection chamber or other access fitting on a sewer. - The building or extension is to be constructed over or within 3m of any drain or sewer more than 3m deep or greater than 225m in diameter.

Soils scally proded by ground water leaking into the drain or sever, e.g. silty sands, saturated silts and peat.
 A rising main (exact from use for the building only).
 Any service of the source of the several service of the several service

Any repairs or replacements of a sewer public or drain is to be carried out by the sewerage undertaker.
 Access points to sewers to be in places where they are accessible and apparent for use in a emergency.
 Ald drains or sewers running under a building to be provided with a minimum of 100mm of granulate fill around the pipe.
 The crown of a pipe is within 300mm of the underside of a floor slab special protection to be provided.
 Where a pipe ins more than 2m deep to the invert and passes beneath the foundation, the foundation is to be designed as a lintel, spanning over the drain, the lintel should span 1.5m
 ether side of the pipe.
 A drain trench is not to be excavated lower than the foundations of any building nearby.
 A drain trench is not to be excavated lower than the foundations of any building nearby.

I low energy light fittings that only take lamps having a luminous efficiency better than 80 lumens per circuit watt. nal light fittings to have both the followiing: External light fittings to have both the following. Automatic controls which switch luminaires off after the lit area becomes unoccupied, if luminous efficacy is 75 light source lumens or less, provide automatic controls which switch luminaires off after the lit area becomes unoccupied, if luminous efficacy is greater than 75 light source lumens, manual control can be installed.

0 1 2 3 4

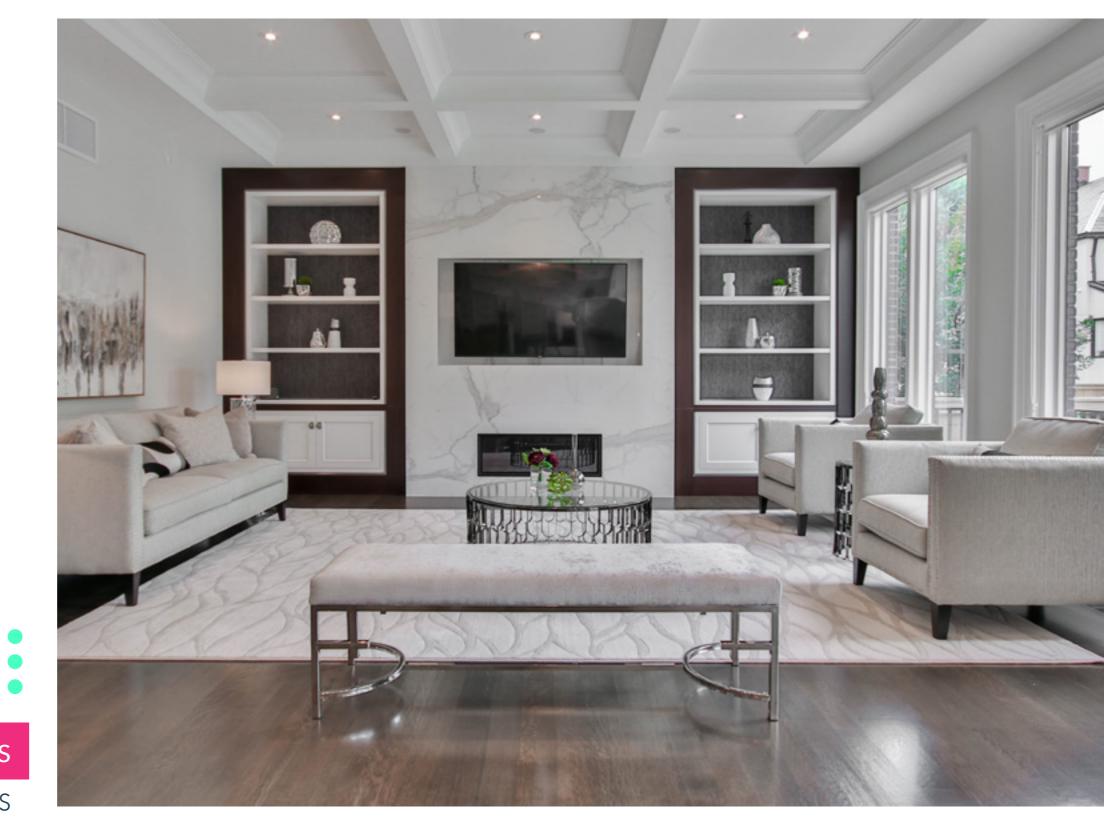
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Go Plans hello@goplans.co.uk 20-22 Wenlock Rd N1 7GU



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# PROJECT ADDRESS

ENGINEERING PLANS

Project	10 Trelawn, L	ondon E10 5QD	
Subject	Structural	Calculations	
	Calc. No.	Rev	Date
К-	25-02-80-C01	0	24.02.25

### Note to Contractor:

### PLEASE READ BEFORE COMMENCING ON SITE

- 1. If you require any additional information before starting the works please email us.
- 2. Whilst carrying out the works, if you uncover any additional structural elements not noted within this calculation package please

contact us as this may require a check and revised structural calculations

- 3. The contractor should carry out their own measured survey and investigations prior to starting works on site and ordering materials to confirm any critical assumptions noted in this document on page 3!
- 4. Please carefully read all notes on next two pages.

5. These calculations should be submitted for a full plans submission to building control prior to starting the works, a compliance report must be issued to the structural engineer prior to the works commencing on site. If you proceed with the works using a Building Notice, you are assuming the risk for the project and we will not accept responsibility or liability for any delays on site or associated costs or damages in connection with the delay or materials and labour cost associated with the re-design.

# **IMPORTANT NOTES**

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### **General Notes**

- All works are to be in accordance with the current British Standard and Building Regulations. 1.
- 2. This document to be read in conjunction with all relevant drawings issued by the Architect and specialist sub-contractors together with the specifications. Any discrepancies to be reported to Engineer.
- Please note that the lengths of structural elements indicated in these calculations are not for fabrication purposes. The length of elements may differ slightly to allow for bearing, etc. The lengths of elements should always be based on onsite measurements. If the lengths of elements should differ from these calculations by more than 10%, please contact Engineer.
- All setting out, levels, DPC, insulation, fire protection & waterproofing information is to be obtained from the Architect. 4
- 5. The Party Wall Act may apply.
- Structural elements not shown in this document are out of scope and to be designed by others. 6.
- 7. Balustrade and balustrade fixing details to be provided by manufacturer.
- 8. Off-the-shelf items to be installed as per manufacturer's details/recommendations.
- All specified structural elements (i.e. steel beams & columns, timber beams&posts, etc.) are to be installed in a single continuous length unless stated otherwise. 9.
- 10. No holes, chases, cut-outs, existing or proposed services or the like may be formed in or pass through any beam, column, or load bearing wall.
- This document is intended to be printed in colour. 11.
- 12. CALCULATIONS ARE SUBJECT TO BUILDING CONTROL APPROVAL. ANY WORKS CARRIED OUT PRIOR TO APPROVAL OF CALCULATIONS BY BUILDING CONTROL ARE AT OWN RISK. WE WILL NOT ACCEPT LIABILITY FOR ANY REQUIREMENTS, ALTERNATIONS, COSTS OR DELAYS RESULTING FROM THIS.

### Construction Notes / Health & Safety Notes

- We do not provide monitoring on site and the experience, diligence and management of the building contractor's team must be relied on. The Contractor must provide 1. permanent, experienced site managers capable of understanding the requirements of our specifications and design.
- The Contractor shall ensure that stability of the building and adjacent premises is maintained at all stages of construction. The contractor is to design, install and maintain all 2. necessary temporary works and programme the work accordingly.
- In addition to the usual risks associated with building works and materials, of which competent builder should be aware, the following site and work specific health and safety 3. risks have been identified: demolition, excavation, drilling and cutting into existing structure or materials should be carried out carefully in case there are any unknows services hidden in the area.
- 4. The project requires the introduction of heavy structural elements such as steel beams or concrete lintels. Builder is to take into consideration the placement of all structural elements, ensuring that the method of lifting and placement is safely carried out. Responsibility for this element lies with the Contractor. As the existing walls need to be propped in order to introduce some of the lintels, this should also be considered in relationship to the risk assessment of the Contractor. Safe working procedures must be adopted. Responsibility for this element lies with the Contractor. Splice details for long-span beams can often be accommodated if required.
- 5. The design has been based on the assumption that the construction will be undertaken by a Competent Building Contractor used to undertaking this form of building works, of this type and complexity, and in accordance with Good Building Practice and general accepted standards and methods of construction.

### Steelwork Notes

- 1. All steel beams / columns to be of steel grade min. S355. All plates to be of steel grade min. S275.
- 2. All bolts to be grade 8.8 unless noted otherwise.
- 3. All welds to be min 6mm fillet welds unless noted otherwise.
- Steel elements end bearing to be equal to full width of any spreader or post / min. 100mm end bearing unless noted otherwise. 4.
- 5 Corus "The Prevention of corrosion on structural steelwork" to be used as a guidance for steelwork finish/paint system.
- Design of all connections is the responsibility of the steelwork sub-contractor unless noted otherwise. 6.
- 7. Steel fabricator drawings to be submitted to engineer for checking before fabrication begins.
- Padstones and steel beams to avoid clashes with chimney breast. Please contact Engineer if otherwise. 8
- All padstones to be C35 grade 9.
- 10. As an alternative to padstones, 25mm thick steel spreader plates for padstones less than 440mm long can be used and 45mm thick steel spreader plates for padstones longer or equal than 440mm long but shorter than 700mm can be used. Steel plates plan dimensions to be the same as padstones plan dimensions.
- 11. Provide clearance to under-side of steelwork at intersecting wall locations where no bearing information is shown to prevent unintended load transfer.
- 12. Where pair of beams is presented, steel beams to be bolted together with M16 bolts @ spacer tubes @max 600mm centres.
- 13. Beams and columns to be placed centrally on bearings, ie beams/posts/padstones unless noted otherwise. Beams to be located centrally under walls, unless they are working as lintels on external cavity walls.
- 14. All steelwork below ground to have a minimum of 50mm concrete encasement unless noted otherwise.
- 15. All new columns to be tied to walls using shot fired wall ties or galvanized frame cramps at 450mm centres.
- 16. In places where beam is located parallel to padstone, beam must be centralized on the padstone. End bearing length of the beam to be equal to half padstone length. In places where beam is located perpendicular to padstone, end bearing length to be equal to padstone width. See drawings for details.
- 17. Site welding is not allowed unless noted otherwise.
- 18. Site modifications to structural steelwork shall not be carried out.

### Timber Notes

- All structural timber to be grade C24 unless noted otherwise. 1.
- 2. All bolts to be grade 8.8 unless noted otherwise
- 3. All timbers to be treated with an approved preservative to BS 5268 PT5
- 4. All cut ends to be retreated before fixing. 5. Timber elements end bearing length to be equal to full width of any spreader or post / min. 100mm end bearing unless noted
- All joist hangers are to be galvanised mild steel with minimum thickness of 2.5mm specified and designed by the specialist manufacturer. Timber joints between members are to be created using either traditional joinery techniques or proprietary fixings. Where input is required contact with engineer.
- 7. Floor and roof constructions, walls require lateral restraints by straps in accordance with the provisions in Building Regulation requirements.
- 8. Where two or more pieces of timber are specified in one element the timbers are to be fixed together to Building Control Officer approval.
- New timber joists spanning more than 2.5m to be restrained by solid noggins in 1/3 of their length. 9. 10. Provide clearance to under-side of timber joists at intersecting wall locations where no bearing information is shown to prevent
- unintended load transfer. 11. Double joists shall be provided under non-load bearing studwork partitions running parallel with joists spans, under baths and under airing cupboards.
- 12. Using notch for timber elements at support is not permitted. If it is required then contact engineer.
- 450mm CTRS or angle brackets (if preferred).
- 14. Timber to timber/steel connections to be specified by others.

### Masonry Notes

- All proposed bricks to be standard format clay 20N/mm2 bricks unless noted otherwise.
- All proposed blockwork to be 7.3N blocks unless noted otherwise
- 3. Mortar below DPC to be designation M6 (ii), above designation M4 (iii).
- Existing loadbearing masonry wall to be minimum 100mm thick wall. 4.
- 100mm wide blocks shall not be laid flat if load bearing. 5.
- Any disturbed and loose masonry should be removed and rebuilt. 6.
- 7. Wall ties to be provided in accordance with the provisions in Building Regulation requirements.
- 8. Movement joints to be provided in accordance with masonry manufacturers recommendations.

### Foundation Notes

- 1. For calculation purposes allowable bearing capacity of 100kN/m2 is assumed. Building Control Officer or other suitably qualified individual to ensure that formation level bearing stratum is valid.
- 2. Concrete to be grade C28/35, reinforcement to be high yield (fy = 500 N/mm2) unless noted otherwise.
- 3. All new foundations to be mass concrete strip footing minimum width 0.6m, minimum depth 1.0m (final depth to building control officer) unless noted otherwise. These depths may need to be increased in order to transfer the loading onto
- satisfactory ground, or where there are trees nearby. 4. Minimum cover to reinforcement to be 50mm unless noted otherwise.
- 5. Existing foundations are assumed sufficient to carry the existing building.
- Main contractor to check condition of existing walls and foundations prior to construction.
- 7. When additional load is added onto existing foundations, the existing foundations to be exposed and inspected by the Building Control Officer to checked/approved if adequate prior to commencement of works.
- 8. If soil is found to be shrinkable clays and trees are located nearby, foundations depth may need to be calculated in accordance with NHBC standard chapter 4.2. Spread foundations may not be suitable to use.
- 9. Pad footing to be placed centrally under columns/piers unless noted otherwise.
- 10. Pad footing near existing foundations should be at least equal in depth to existing foundation depth. Local underpinning may be required to prevent undermining if new pad footing proposed formation level is deeper than adjacent existing footing.
- 11. Footing near existing foundations should be at least equal in depth to existing foundation depth. Local underpinning may be required to prevent undermining if new footing proposed formation level is deeper than adjacent existing footing. New foundations to be excavated in 1.0m long bays; bays being excavated at the same time must not be adjacent to each other.
- 12. New foundations to be connected to existing foundations to Building Control Officer approval.
- 13. OBTAIN APPROVAL FROM LOCAL AUTHORITY BUILDING CONTROL BEFORE CASTING ANY FOUNDATIONS.

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13. Timber post adjacent to existing masonry wall need to be resin anchored into the masonry using min M12 anchors @ max

# **IMPORTANT NOTES**

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### SYMBOL KEY

# LOAD BEARING MASONRY WALL LOAD BEARING STUD / DORMER WALL

APPROX LINE OF LOAD BEARING STUD / DORMER WALL OVER SHOWN DASHED NON-LOADBEARING TIMBER PARTITION WALL SHEATHED IN PLYWOOD / OSB EITHER SIDE. WALL TO BE STRAPPED TO WALLS AND FLOORS. SEE SUMMARY PAGE FOR DETAILS. OSB BOARDED JOISTS WITH ADDITIONAL LATERAL RESTRAINT BY STRAPS. SEE PLYBOARDING OF TIMBER JOISTS NOTE ON GENERAL ARRANGEMENT PAGE.

STEEL BEAM ON PLAN/ COLUMN ON SECTION / ELEVATION

- STEEL UB / UC COLUMN ON PLAN / STEEL BEAM ON SECTION / ELEVATION
- STEEL UB / UC COLUMN OVER SHOWN DASHED
- STEEL SHS COLUMN

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- STEEL SHS COLUMN OVER SHOWN DASHED TIMBER BEAM ON PLAN / TIMBER POST ON SECTION / ELEVATION TIMBER POST / RAKING STRUT
- APPROX BEARING OF TIMBER POST / RAKING STRUT OVER SHOWN DASHED LINTEL EXISTING BEAM / EXISTING LINTEL EXISTING JOISTS SPAN DIRECTION UNLESS NOTED OTHERWISE
- FLEXIBLE ENDPLATE CONNECTION. SEE DRAWING DETAILS NEW RAFTERS SPAN DIRECTION NEW FLAT ROOF JOISTS SPAN DIRECTION
- NEW CEILING JOISTS SPAN DIRECTION
- NEW FLOOR JOISTS SPAN DIRECTION
- NEW GROUND FLOOR JOISTS SPAN DIRECTION
- PADSTONE SHAPE
- BEARING DETAIL NUMBER

## DOCUMENT CONTROL

Document Prepared by:	Patrycja Perlińska MEng
Document Checked by:	Katarzyna Jaworska-Kanarek MEng
Document Approved by:	Katarzyna Jaworska-Kanarek MEng
Revision:	0
Date:	24.02.25

### 1. WE DO NOT PROVIDE MONITORING ON SITE AND THE EXPERIENCE. DILIGENCE AND MANAGEMENT OF THE BUILDING CONTRACTOR'S TEAM MUST BE RELIED ON. THE CONTRACTOR MUST PROVIDE PERMANENT, EXPERIENCED SITE MANAGERS CAPABLE OF UNDERSTANDING THE REQUIREMENTS OF OUR SPECIFICATIONS AND DESIGN.

2. THE CONTRACTOR SHALL ENSURE THAT STABILITY OF THE BUILDING AND ADJACENT PREMISES IS MAINTAINED AT ALL STAGES OF CONSTRUCTION. THE CONTRACTOR IS TO DESIGN. INSTALL AND MAINTAIN ALL NECESSARY TEMPORARY WORKS AND PROGRAMME THE WORK ACCORDINGLY.

3. THE DESIGN HAS BEEN BASED ON THE ASSUMPTION THAT THE CONSTRUCTION WILL BE UNDERTAKEN BY A COMPETENT BUILDING CONTRACTOR USED TO UNDERTAKING THIS FORM OF BUILDING WORKS, OF THIS TYPE AND COMPLEXITY, AND IN ACCORDANCE WITH GOOD BUILDING PRACTICE AND GENERAL ACCEPTED STANDARDS AND METHODS OF CONSTRUCTION.

	DESIGN APPROACH
BS 6399 P1/P2/P3	Loading for Building. Code of practice for dead and imposed loads. Code of practice for wind loads. Code of practice for imposed roof loads.
BS 8103 P3	Structural design of low-rise buildings. Code of practice for timber floors and roofs for housing.
BS 5950 P1	Structural use of steelwork in building. Code of practice for design – Rolled and welded sections
BS 8110 P1	Structural use of concrete. Code of practice for design and construction
BS 5628 P1	Code of practice for the use of masonry. Structural use of unreinforced masonry.
BS 5268 P2	Structural use of timber.

# DESIGN ASSUMPT

MAY NEED TO CHANGE:

- 100mm wide loadbearing masonry walls (and not 65mm "brick on edge" walls) with foundations underneath.
- 2. Existing floors above the ground floor are timber construction (with no concrete screed on top).
- 3. If ground is shrinkable clay and there are trees within 30m of the proposed development, then a tree survey to be forwarded to engineer, as foundations may need to be updated.
- 4. The existing ground floor is a ground-bearing slab.

5. Allowable bearing capacity of 100kN/m2. Building Control Officer or other suitably qualified individual to ensure that formation level bearing stratum is valid.

### 6. Air source heat pump total weight does not exceed 200kg.

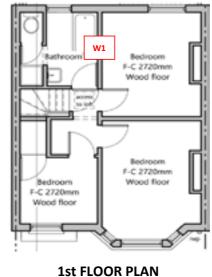
CONSERVATIVE ASSUMPTIONS - THESE CAN BE CONFIRMED BY CONTRACTOR TO POTENTIALLY OPTIMISE DESIGN BUT ARE NOT CRUCIAL:

- 2. The existing floor joists span direction is unknown (worst case assumed).
- 3. Existing walls marked below as W1 is 100mm wide masonry walls.

## INPUT REQUIRED BY 3rd PARTIES / OTHER CONTRACTORS

- Liquid Crystal Glazing and trimmers design and specification
- Foundation design; verification of Presumed Allowable Bearing Pressure.

- Acceptability of ground bearing slab / foundations depth with local ground conditions.
- Steelwork connections (Steel fabricator drawings to be submitted to us for checking before fabrication begins).
- Timber connections to contractor (if any guidance required, please come back to us)



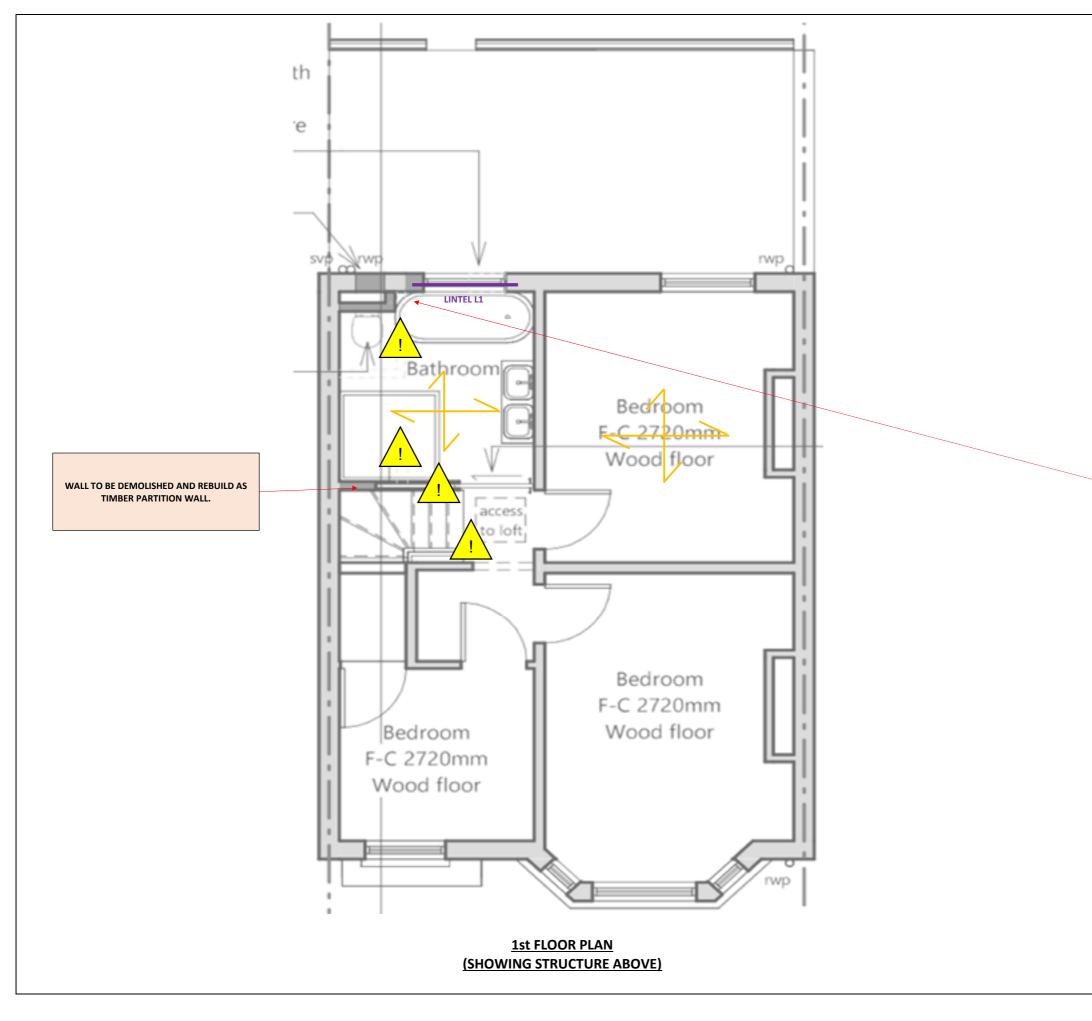


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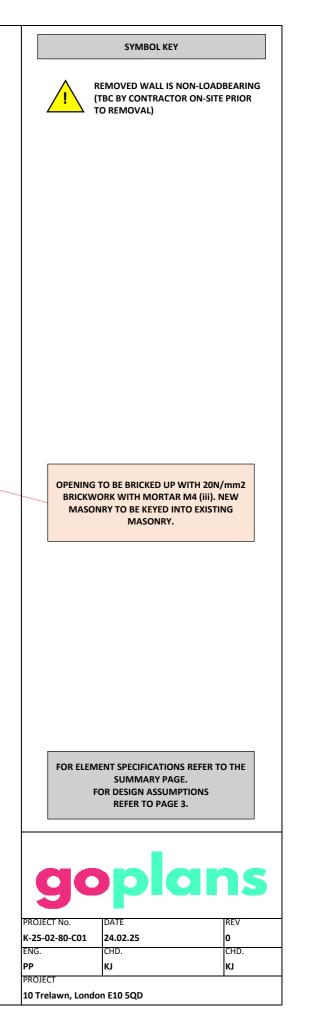
## CRITICAL ASSUMPTIONS - THESE MUST BE CONFIRMED BY CONTRACTOR BEFORE COMMENCING THE WORK ON SITE AS DESIGN

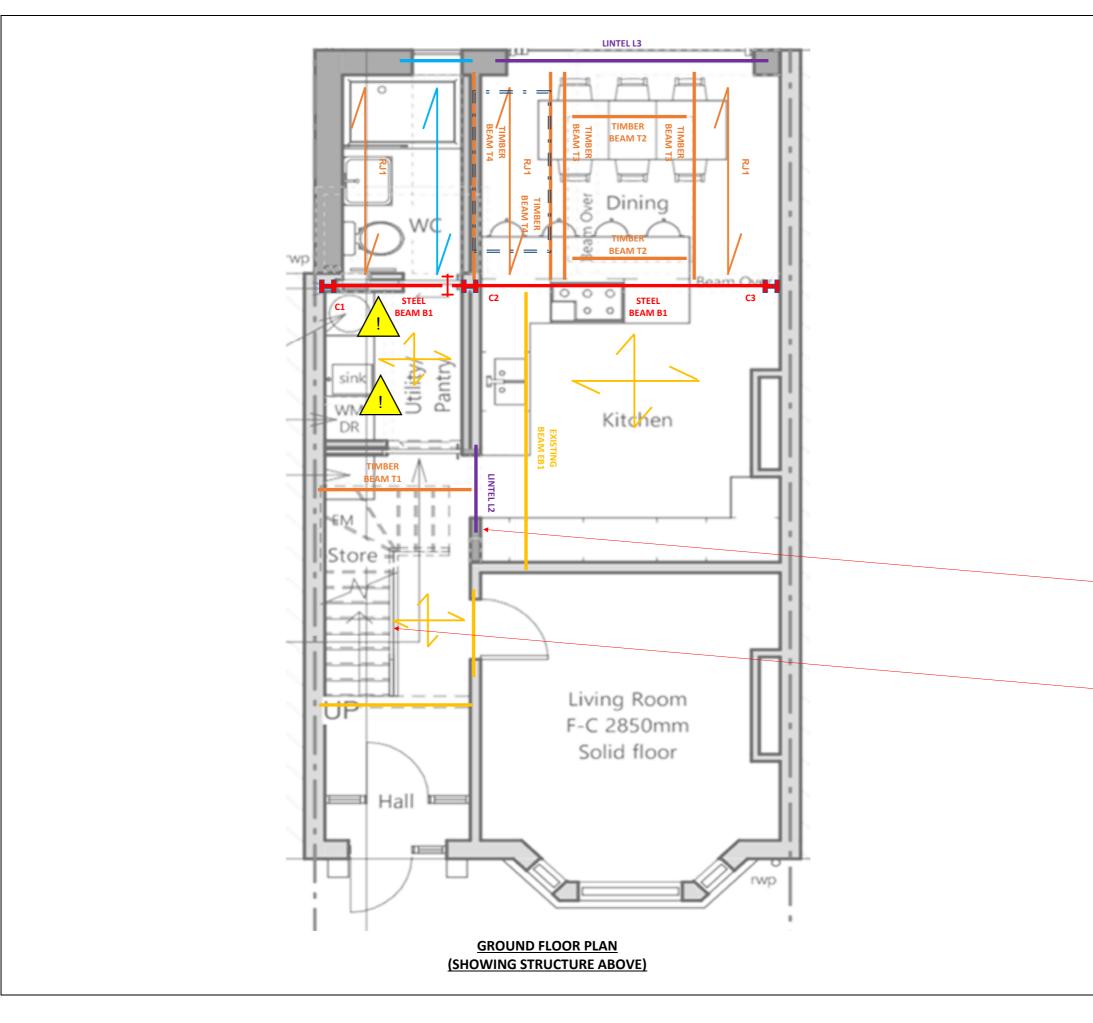
1. Masonry load-bearing wall locations (hatched on general arrangement / steel beam bearing positions). Existing walls to be min.

1. The existing masonry is assumed to be poor-quality brickwork/stonework for padstone design, where relevant.

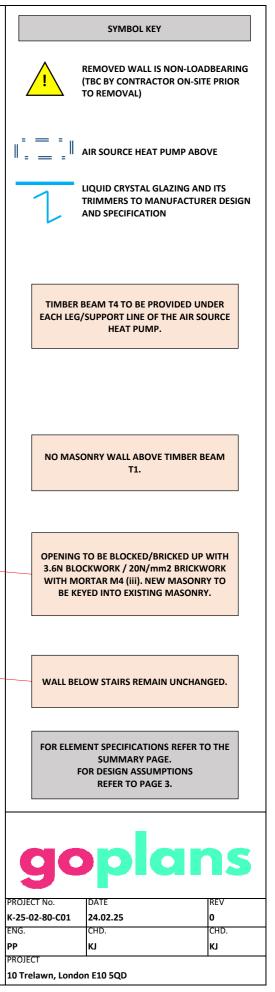


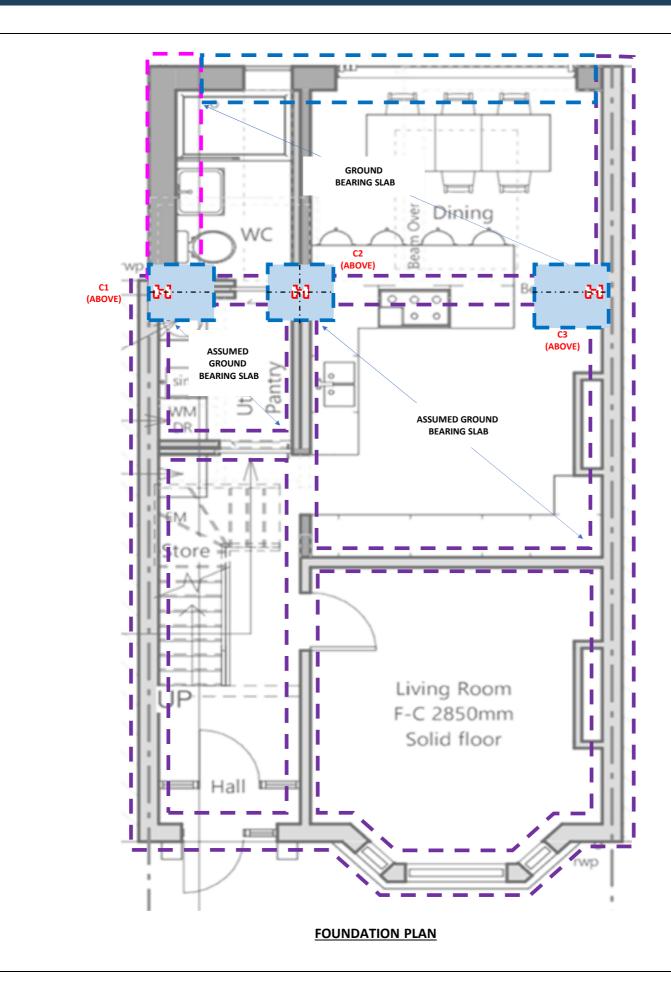
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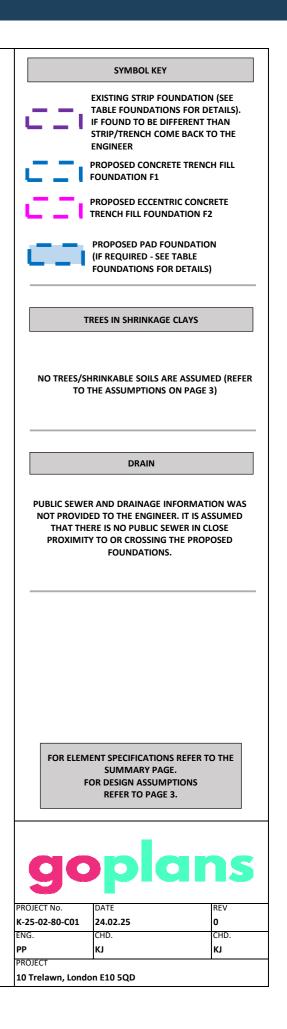




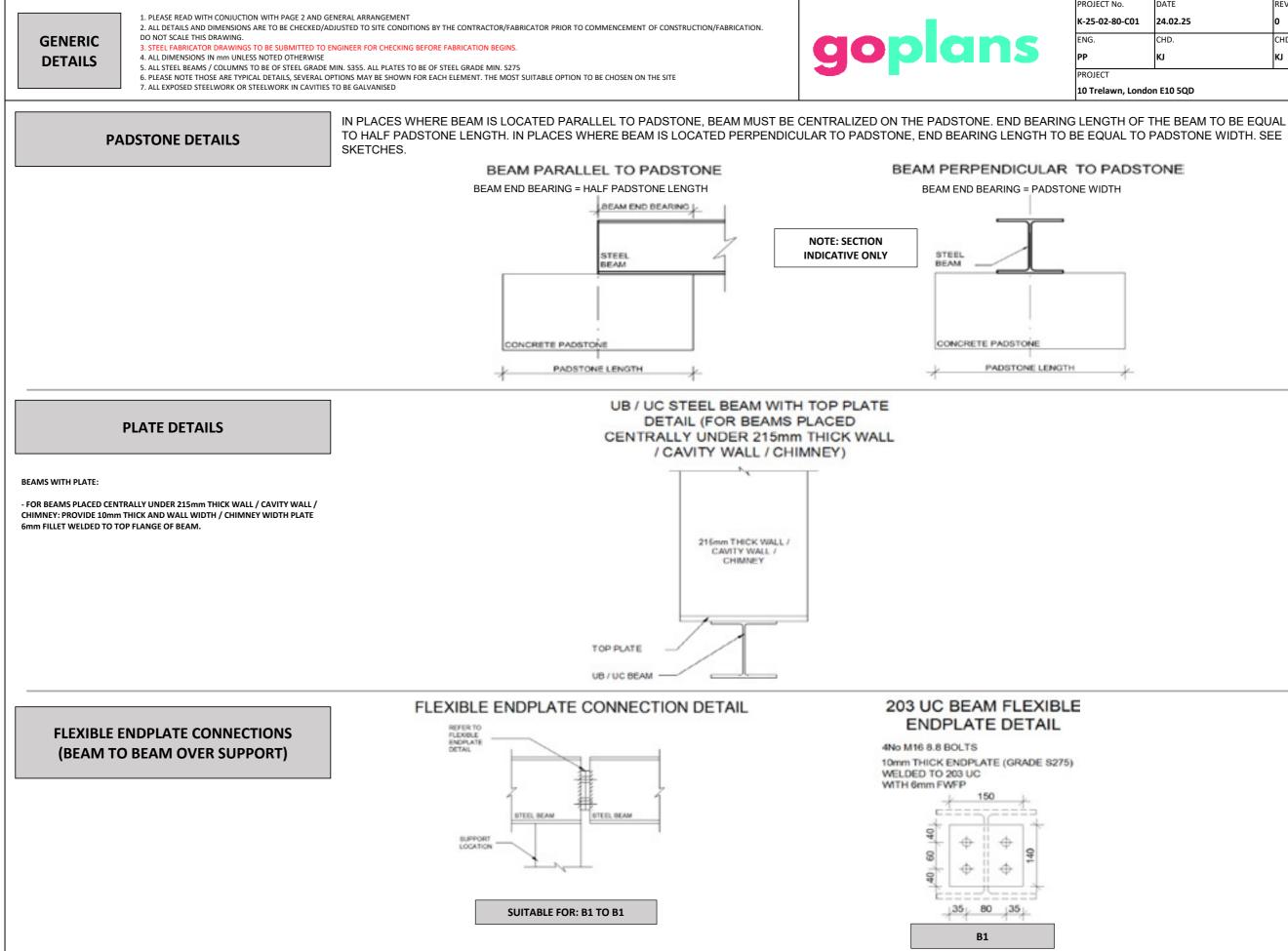
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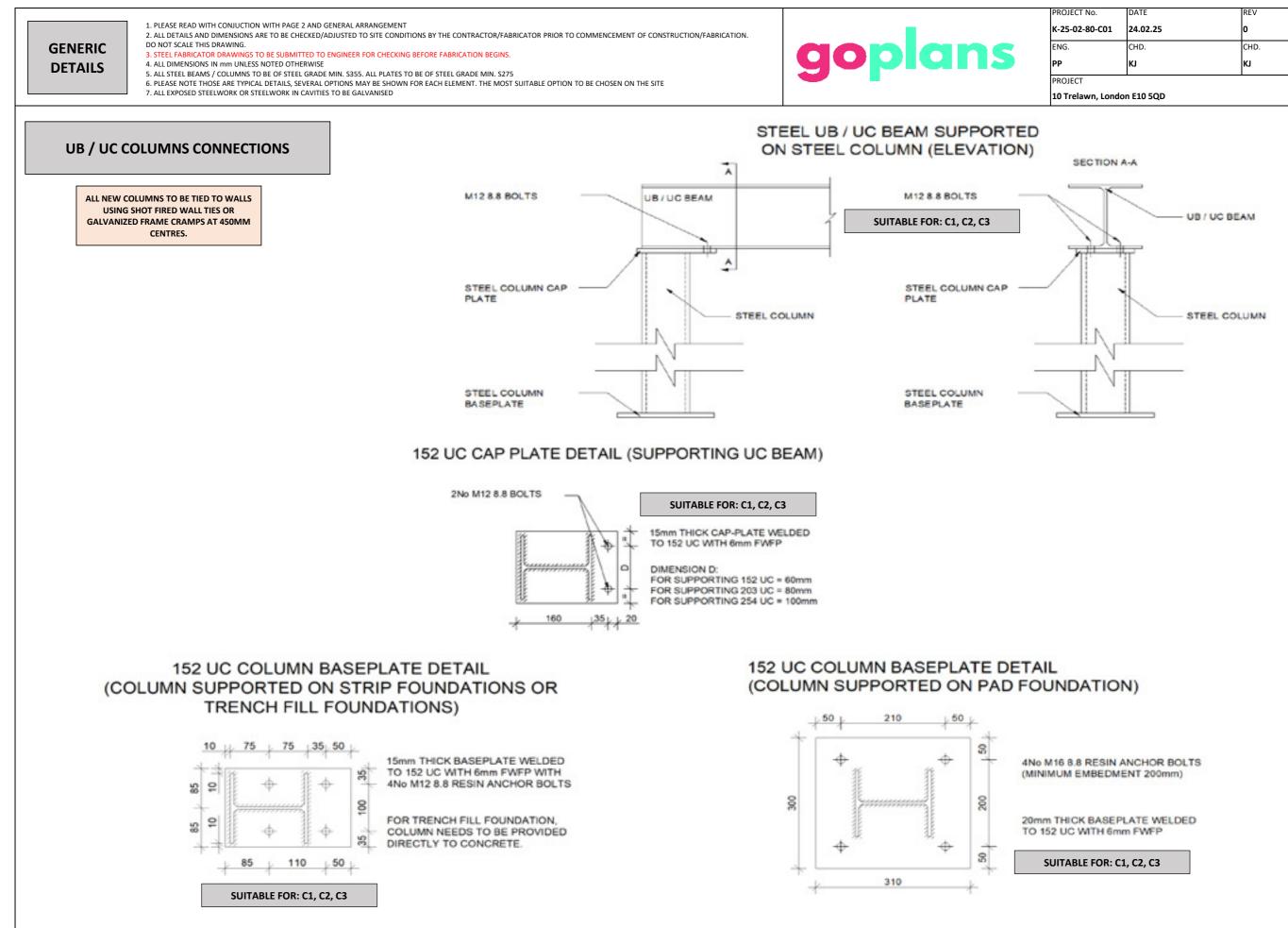


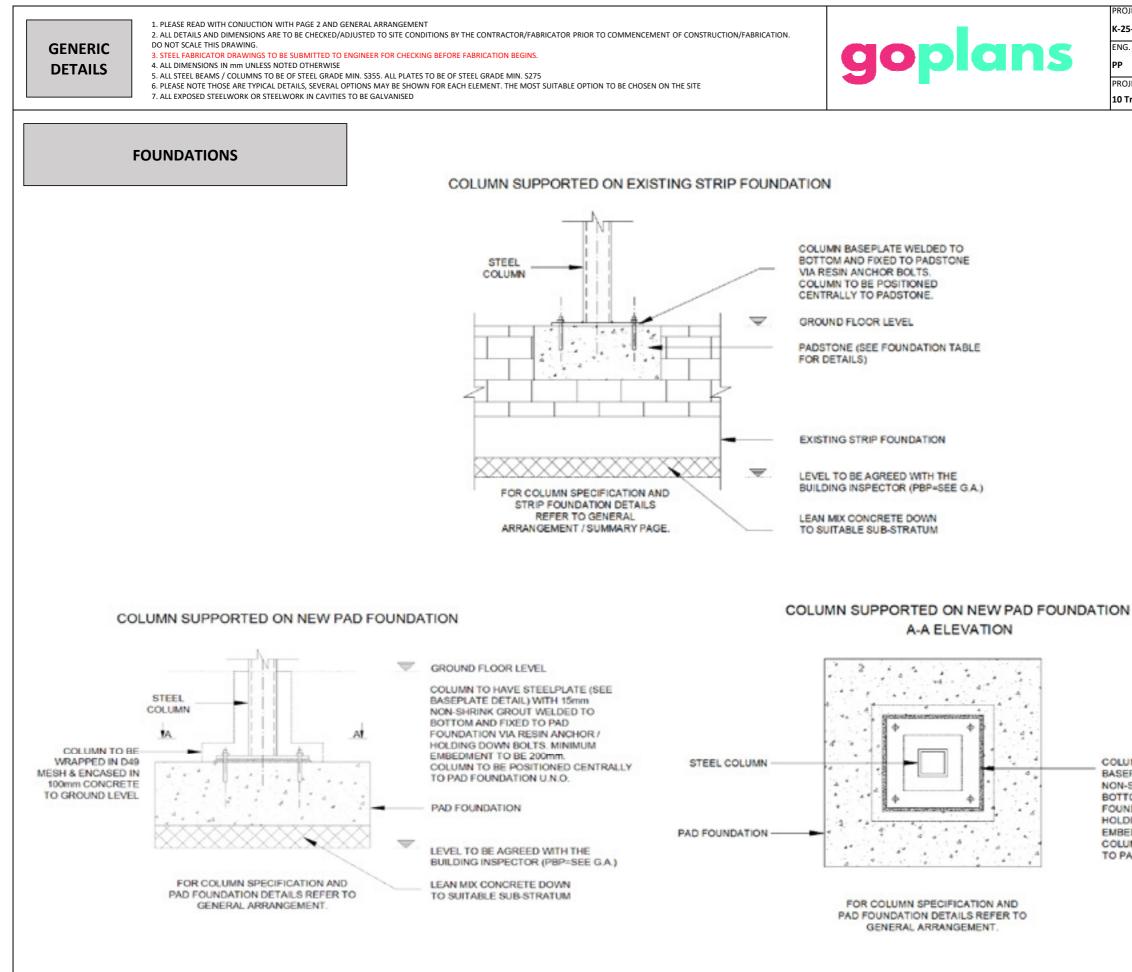


	TING ELEMENT MATCHES SPECIFICATION OF NEW STRUCTURAL MENT, RE-USE IS OK SUBJECT TO BUILDER CONFIRMATION / CHECKING QUALITY OF ELEMENT.	goplar	PROJECT No.         DATE         REV           K-25-02-80-C01         24.02.25         0           ENG.         CHD.         CHD.           PP         KJ         KJ           PROJECT         10 Trelawn, London E10 5QD         E10 5QD
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COLUMN TO HAVE STEELPLATE (SEE BASEPLATE DETAIL) WITH 15mm NON-SHRINK GROUT WELDED TO BOTTOM AND FIXED TO PAD FOUNDATION VIA RESIN ANCHOR / HOLDING DOWN BOLTS, MINIMUM EMBEDMENT TO BE 200mm. COLUMN TO BE POSITIONED CENTRALLY TO PAD FOUNDATION U.N.O.

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# LOAD SUMMARY

LOAD SUMMARY		
Beam & Block Floor		
Finishes	0.20 kN/m2	
75mm Screed	1.80 kN/m2	
Insulation	0.10 kN/m2	
150mm B&B Floor	2.20 kN/m2	
Total Dead load	4.30 kN/m2	
Imposed load	1.50 kN/m2	
Balcony		
Finishes & Boarding	1.00 kN/m2	
Insulation	0.10 kN/m2	
Joists	0.10 kN/m2	
Ceiling / Plasterboard	0.20 kN/m2	
Total Dead load Imposed load	1.40 kN/m2 1.50 kN/m2	
inposed load	1.50 KN/112	
Timber Floor		
Finishes & Boarding	0.20 kN/m2	
Insulation	0.10 kN/m2	
Joists	0.10 kN/m2	
Ceiling / Plasterboard	0.20 kN/m2	
Partition Walls Total Dead load	0.50 kN/m2 1.10 kN/m2	
Imposed load	1.50 kN/m2	
imposed load	1.00 KN/112	
<u>Ceiling</u>		
Finishes	0.05 kN/m2	
Insulation	0.10 kN/m2	
Joists	0.10 kN/m2	
Ceiling / Plasterboard Total Dead load	0.20 kN/m2 0.45 kN/m2	
Imposed load	0.45 kN/m2	
Imposed Ioad	0.25 KN/112	
Pitched Roof		
Finishes / Tiles	0.50 kN/m2	
Battens / Felt / Insulation	0.10 kN/m2	
Structure	0.20 kN/m2	
Ceiling / Plasterboard	0.20 kN/m2	
Ceiling / Plasterboard Total Dead load	0.20 kN/m2 1.00 kN/m2	
Ceiling / Plasterboard	0.20 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load <u>Flat Roof</u>	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load <u>Flat Roof</u> Finishes	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load Flat Roof Finishes Felt / Insulation	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.50 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load Flat Roof Finishes Felt / Insulation Joists	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2	
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead load Imposed load	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2 1.00 kN/m2	
Ceiling / Plasterboard Total Dead load Imposed load Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead load Imposed load WALLS	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2	4.00 141/2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2	1.00 kN/m2 0 35 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.75 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 1.00 kN/m2 0.75 kN/m2	0.35 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.75 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 ity Wall	0.35 kN/m2 4.20 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockw	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad MALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw 100mm Lightweight Blockwork W	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad MALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw 100mm Lightweight Blockwork W	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw 100mm Lightweight Blockwork W New Cavity Wall	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork //Dense Blockw 100mm Lightweight Blockwork W New Cavity Wall OTHERS	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork //Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Lightweight Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 0.50 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork //Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Caw 100mm Brickwork /Dense Blockw 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 0.50 kN/m2 2.10 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork /Dense Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.50 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 iall ity Wall vork Wall	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Brickwork //Dense Blockw 100mm Lightweight Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels Balustrade	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.75 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 0.75 kN/m2 1.00 kN/m2 0.75 kN/m2 ity Wall vork Wall all	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Fiet / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Lightweight Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels Balustrade Site altitude Δs =	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.75 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 all ity Wall vork Wall all 13 m	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2
Ceiling / Plasterboard Total Dead Ioad Imposed Ioad Flat Roof Finishes Felt / Insulation Joists Ceiling / Plasterboard Total Dead Ioad Imposed Ioad WALLS Dormer Wall / External Timber W Timber Partition Wall Solid 215mm Masonry Wall / Cav 100mm Erickwork //Dense Blockw 100mm Lightweight Blockwork W New Cavity Wall OTHERS Bi-folds Doors Glazing Chimney PV Panels Balustrade	0.20 kN/m2 1.00 kN/m2 0.75 kN/m2 0.75 kN/m2 0.10 kN/m2 0.20 kN/m2 0.20 kN/m2 0.20 kN/m2 0.75 kN/m2 1.00 kN/m2 0.75 kN/m2 ity Wall vork Wall all	0.35 kN/m2 4.20 kN/m2 2.10 kN/m2 0.90 kN/m2 4.20 kN/m2 0.50 kN/m2 2.10 kN/m2 0.30 kN/m2



## ALLOWABLE JOISTS SPAN DUE TO TRADA

Flat Roof Joists For Dead Load more than 0.75kN/m2 but not more than 1.00 kN/m2 ; For Imposed Load 0.75 kN/m2 Section (RJ): 150 x 50 C24 @400mm c/c

PROJECT 10 Trelawn, Lond	PROJECT					
РР	кл	кј				
ENG.	CHD.	CHD.				
K-25-02-80-C01	24.02.25	0				
PROJECT No.	DATE	REV				

Span 2.70 m

<= Allowable Span 3.11 m

ОК

PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	o
ENG.	CHD.	CHD.
РР	кј	кл
PROJECT		

# <u>TIMBER BEAM T1</u> Beam Span L =

1.75 m

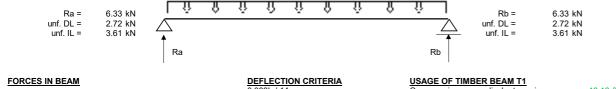
	Load Posit	ioned	Element	nt		Element			
Load	from (m)	to (m)	Span/Height						
Timber floor (1st)	0.00	1.75	5.50 m	/	2.00	=	2.75 m		
-	0.00	1.75	0.00 m	/	1.00	=	0.00 m		
-	0.00	1.75	0.00 m	/	1.00	=	0.00 m		
-	0.00	1.75	0.00 m	/	1.00	=	0.00 m		
-	0.00	1.75	0.00 m	/	1.00	=	0.00 m		
-	0.00	1.75	0.00 m						
_	0.00	1.75	0.00 m						

## UDL LOADING UDL Dead Loading Beam Self Weight

Beam Self Weight					0.08 kN/m	х	1.00	=	0.08 kN/m
Timber floor (1st)	1.10 kN/m2	х	2.75 m	=	3.03 kN/m	x	1.00	=	3.03 kN/m
- ( )	0.00 kN/m2	х	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
-	0.00 kN/m2	х	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
-	0.00 kN/m2	х	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
-	0.00 kN/m2	х	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
	0.00 kN	/	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
UDL Imposed Loadin	na			_	3.11 kN/m				3.11 kN/m
				_					
	1.50 kN/m2	x	2.75 m	=	4.13 kN/m	x	1.00	=	3.11 kN/m 4.13 kN/m
	1.50 kN/m2 0.00 kN/m2	X X	0.00 m	=	<b>4.13 kN/m</b> 0.00 kN/m	x ×	1.00	=	<b>4.13 kN/m</b> 0.00 kN/m
	1.50 kN/m2				4.13 kN/m				<b>4.13 kN/m</b> 0.00 kN/m
	1.50 kN/m2 0.00 kN/m2	Х	0.00 m	=	<b>4.13 kN/m</b> 0.00 kN/m	Х	1.00	=	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m
<b>UDL Imposed Loadir</b> Timber floor (1st) - - -	1.50 kN/m2 0.00 kN/m2 0.00 kN/m2	X X	0.00 m 0.00 m	=	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m	X X	1.00 1.00	=	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m
	1.50 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m	= = =	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m	X X X	1.00 1.00 1.00	= = =	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m
	1.50 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m 0.00 m	= = =	<b>4.13 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m	x x x x	1.00 1.00 1.00 1.00	= = =	4.13 kN/m

Point Load P1 @	0.00 m	Point Load P2 @	0.00 m	
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x (MAX)	
DL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	DL =	0.00 kN x 1.00 =	0.00 kN
IL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	IL =	0.00 kN x 1.00 =	0.00 kN
Point Load P3 @	0.00  m			

From Beam	=	1.00 X (MAX)	+	1.00 X (N	ЛАХ)	) + 1.00 X (IV	IAX
DL	=	0.00 kN	Х	1.00	=	0.00	kΝ
IL	=	0.00 kN	Х	1.00	=	0.00	kΝ



FORCES IN BEAM			DEFLECTION CRITERIA	USAGE OF TIMBER BEAM 11	
			0.003L / 14mm	Compression perpendicular to grain	18.16 %
Moment	=	2.77 kNm		Shear parallel to grain	63.49 %
Shear Force	=	6.33 kN	DURATION OF LOADING	Bending parallel to grain	66.96 %
Axial Force	=	0.00 kN	Long-term	Vertical deflection	63.76 %

## TIMBER BEAM T1 = 3No 150x50mm C24

## BEARING CHECK

	Total			Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
Beam	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
No	Load		Support	Strength	γb*fk/γm			Bearing				Padstone	
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
					1.25xfk/3.5								
T1 (LHS):	T1	9.58	Ex. Historic Brick	2.25	0.80	100	132	0.73	-	-	-	-	Satisfactory
					1.25xfk/3.5								
T1 (RHS):	T1	9.58	Ex. Historic Brick	2.25	0.80	100	132	0.73	-	-	-	-	Satisfactory

 Beam Support Summary:

 T1 (LHS):
 Provide Minimum 100mm End Bearing Length

 T1 (RHS):
 Provide Minimum 100mm End Bearing Length

 Refer To G.A. for more details.

# goplans

## TIMBER BEAM T1 - DESIGN DUE TO BS 5268

		Pr	operties of	3No 150x50mm		
Depth h = Overall breadth of r Length of bearing It Length of bearing It Area of beam A = Min modulus of elas Modified min modul Modulus of rigidity ( Moment of inertia Iy Section modulus Zy Root radius ry =	o_I = o_r = us of elasticit G = v =		145 mm 132 mm 100 mm 19140 mm 7.20 GP 8.71 GP 0.54 Gpi 3353 cm 463 cm 4.19 cm	n n n^2 'a a ^4 ^3	Timbe Servic Load I Loads Depth K2 = K3 = K4 = K5 = K7 = K8 =	e Clas Duratio haring
Forces in beam					K9 =	
Moment Shear Force Axial Force	= = =	2.77 kN 6.33 kN 0.00 kN	1			
Lateral support						
Ends held in positio				ct connection of s	sheathing	g, dec
Permissible depth-t Actual depth-to-bre		io =	5.000 1.098			ок
Compression perp	endicular to	arain				
Permissible bearing			2.640 N/n	nm^2		
Applied bearing stre	ess σc_a =		0.479 N/n	nm^2		ок
Shear parallel to g	rain					
Permissible shear s			0.781 N/n	nm^2		
Applied shear stres	s та =		0.496 N/n	nm^2		ок
Bending parallel to	o grain					
Permissible bending		idm =	8.937 N/n			
Applied bending str	ess σm_a =		5.984 N/n	nm^2		ок
Vertical deflection						
Total dead and imp			12.65 kN			
Shear area for bear			15950 mm	n		
Beam effective spa			1.85 m			
Shear deflection δv			0.319 mm	-		
Bending deflection Total deflection δa=			3.028 mm 3.347 mm			
Limiting deflection of =				n n (0.003L / 14mm	1)	ок
TIMBER BEAM T1	TO BE 3No	150x50mm (	224			

PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
РР	кл	кј
PROJECT		
10 Trelawn, Lond	on E10 5QD	

- grade: Class: uration: aring system: Breadth Ratio:
- C24 1 . Long-term No 5
- 1.00 (Service class 1)
- 1.00 (Long-term) 1.00 (Conservative approach)
- 1.00 (Beam without notch)
- 1.08 (72mm < h ≤ 300mm)
- 1.10 (3No element) 1.21 (3No softwoods element)

K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	кл	кл

# <u>TIMBER BEAM T2</u> Beam Span L =

1.50 m

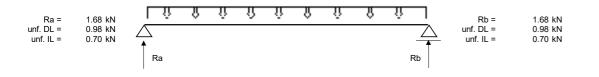
	Load Posi	tioned	Element	1			
Load	from (m)	to (m)	Span/Height				
Roof (flat)	0.00	1.50	2.50 m	/	2.00	=	1.25 m
-	0.00	1.50	0.00 m	/	1.00	=	0.00 m
-	0.00	1.50	0.00 m	/	1.00	=	0.00 m
-	0.00	1.50	0.00 m	/	1.00	=	0.00 m
-	0.00	1.50	0.00 m	/	1.00	=	0.00 m
-	0.00	1.50	0.00 m				
-	0.00	1.50	0.00 m				

# UDL LOADING UDL Dead Loading

Beam Self Weight					0.05 kN/m	х	1.00	=	0.05 kN/m
Roof (flat)	1.00 kN/m2	х	1.25 m	=	1.25 kN/m	х	1.00	=	1.25 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
					4 00 1 11/				4 00 1-11/
UDL Imposed Loading					1.30 kN/m				1.30 KN/M
		x	1 25 m	=		x	1.00	=	1.30 kN/m
	0.75 kN/m2	x	1.25 m	=	0.94 kN/m	×	<b>1.00</b>	=	0.94 kN/m
		X X X	<b>1.25 m</b> 0.00 m 0.00 m			<b>x</b> ×	<b>1.00</b> 1.00 1.00		
	0.75 kN/m2 0.00 kN/m2	Х	0.00 m	=	<b>0.94 kN/m</b> 0.00 kN/m	Х	1.00	=	<b>0.94 kN/m</b> 0.00 kN/m
UDL Imposed Loading - - - - -	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2	x x	0.00 m 0.00 m	=	<b>0.94 kN/m</b> 0.00 kN/m 0.00 kN/m	X X	1.00 1.00	=	<b>0.94 kN/m</b> 0.00 kN/m 0.00 kN/m
Roof (flat) - -	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m	= = =	<b>0.94 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m	X X X	1.00 1.00 1.00	= = =	<b>0.94 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m
Roof (flat) - -	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m 0.00 m	= = =	<b>0.94 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m	x x x x	1.00 1.00 1.00 1.00	= = =	0.94 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m

Point Load P1 @	0.00 m	Point Load P2 @	0.00 m		
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x (MAX)		
DL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	DL =	0.00 kN x 1	1.00 =	0.00 kN
IL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	IL =	0.00 kN x 1	1.00 =	0.00 kN
Point Load P3 @	0.00 m				

I OIIIC LOUG I V		0.00 111				
From Beam	=	1.00 x (MAX)	+ 1.	N) x 00.	/IAX) +	1.00 x (MAX)
DL	=	0.00 kN	Х	1.00	=	0.00 kN
IL	=	0.00 kN	Х	1.00	=	0.00 kN



FORCES IN BEAM			DEFLECTION CRITERIA	USAGE OF TIMBER BEAM T2	
			0.003L	Compression perpendicular to grain	5.79 %
Moment	=	0.63 kNm		Shear parallel to grain	20.24 %
Shear Force	=	1.68 kN	DURATION OF LOADING	Bending parallel to grain	18.30 %
Axial Force	=	0.00 kN	Medium-term (K3 = 1.25)	Vertical deflection	20.50 %

## TIMBER BEAM T2 = 2No 150x50mm C24

## BEARING CHECK

Beam	Total Vertical		Type of	Charact. Compr.	Local Strength	Bearing Length	Bearing Width	Stress Below	Padstone Length	Padstone Width	Ecc	Stress Below	Summary
No	Load		Support	Strength	γb*fk/γm	-		Bearing	Ŭ			Padstone	,
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
T2 (LHS):	T2	2.49	Beam Connection										
T2 (RHS):	Т2	2.49	Beam Connection										

Provide Steel Beam/Column/Timber Post Connection Refer To G.A. for more details. T2 (RHS):

# goplans

## TIMBER BEAM T2 - DESIGN DUE TO BS 5268

		Pr	opertie	s of 2No 150	x50mm	
Depth h = Overall breadth of merr Length of bearing lb_1 = Length of bearing lb_r = Area of beam A = Min modulus of elasticit Modified min modulus of Modulus of rigidity G = Moment of inertia ly = Section modulus Zy = Root radius ry =	: = ty Emin =	=	88 100 12760 7.20 8.21 0.51 2236	mm mm mm^2 GPa GPa GPa Gpa cm^4 cm^3 cm		Timber grad Service Clas Load Duratic Loadsharing Depth to Bre K3 = K4 = K5 = K7 = K8 =
Forces in beam						K9 =
Moment Shear Force Axial Force	= = =	0.63 kN 1.68 kN 0.00 kN				
Lateral support Ends held in position ar	nd members	held in line	e, as by	direct connec	tion of sh	eathing, dec
Permissible depth-to-br Actual depth-to-breadth			5.000 1.648			ок
Compression perpend Permissible bearing str Applied bearing stress	ess σc_adm			N/mm^2 N/mm^2		ок
Shear parallel to grain Permissible shear stres Applied shear stress ta	s τadm =			N/mm^2 N/mm^2		ок
Bending parallel to gr Permissible bending str Applied bending stress	ress om_adm	=		N/mm^2 N/mm^2		ок
Vertical deflection Total dead and impose Shear area for beam A Beam effective span le Shear deflection öv=	y =		3.36 10633 1.60 0.116	mm m		
Bending deflection δb= Total deflection δa= Limiting deflection =		-	0.807 0.922 4.500	mm	)	ок
TIMBER BEAM T2 TO	BE 2No 150	x50mm C	24			

10 Trelawn, London E10 5QD						
PROJECT						
РР	кл	кј				
ENG.	CHD.	CHD.				
K-25-02-80-C01	24.02.25	0				
PROJECT No.	DATE	REV				

grade: Class: uration: aring system: o Breadth Ratio:

C24 1 Medium-term No 5

- 1.00 (Service class 1)
- 1.25 (Medium-term) 1.00 (Conservative approach)
- 1.00 (Beam without notch)
- 1.08 (72mm < h ≤ 300mm)
- 1.10 (2No element) 1.14 (2No softwoods element)

K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	кл	кл

## <u>TIMBER BEAM T3</u> Beam Span L = 2.70 m

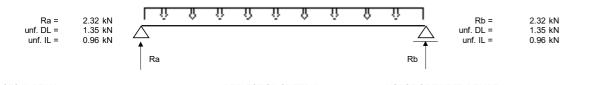
	Load Posi	tioned	Element	1			
Load	from (m)	to (m)	Span/Height				
Roof (flat)	0.00	2.70	1.90 m	/	2.00	=	0.95 m
-	0.00	2.70	0.00 m	/	1.00	=	0.00 m
-	0.00	2.70	0.00 m	/	1.00	=	0.00 m
-	0.00	2.70	0.00 m	/	1.00	=	0.00 m
-	0.00	2.70	0.00 m	/	1.00	=	0.00 m
-	0.00	2.70	0.00 m				
_	0.00	2 70	0.00 m				

# UDL LOADING UDL Dead Loading

Beam Self Weight					0.05 kN/m	х	1.00	=	0.05 kN/m
Roof (flat)	1.00 kN/m2	х	0.95 m	=	0.95 kN/m	х	1.00	=	0.95 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
						-			4 66 1 11/
UDL Imposed Loading					1.00 kN/m				1.00 kN/m
	0.75 kN/m2	x	0.95 m	=	0.71 kN/m	x	1.00	=	0.71 kN/m
	0.75 kN/m2 0.00 kN/m2	<b>x</b> ×	0.00 m	=	<b>0.71 kN/m</b> 0.00 kN/m	x ×	1.00	=	<b>0.71 kN/m</b> 0.00 kN/m
	0.75 kN/m2				0.71 kN/m				0.71 kN/m
	0.75 kN/m2 0.00 kN/m2	Х	0.00 m	=	<b>0.71 kN/m</b> 0.00 kN/m	Х	1.00	=	<b>0.71 kN/m</b> 0.00 kN/m
	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2	X X	0.00 m 0.00 m	=	<b>0.71 kN/m</b> 0.00 kN/m 0.00 kN/m	X X	1.00	=	<b>0.71 kN/m</b> 0.00 kN/m 0.00 kN/m
	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m	= = =	<b>0.71 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m	X X X	1.00 1.00 1.00	= = =	<b>0.71 kN/m</b> 0.00 kN/m 0.00 kN/m 0.00 kN/m
UDL Imposed Loading Roof (flat) - - - - - -	0.75 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m 0.00 m	= = =	0.71 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m	x x x x	1.00 1.00 1.00 1.00	= = =	0.71 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m

Point Load P1 @	0.00 m	Point Load P2 @	0.00 m	
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x (MAX)	
DL =	0.00 kN x 1.00 = 0.00 kN	DL =	0.00 kN x 1.00 =	0.00 kN
IL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	IL =	0.00 kN x 1.00 =	0.00 kN
Point Load P3 @	0.00 m			

	0.00 111	
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	
DL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	
IL =	0.00 kN x 1.00 = 0.00 kN	



USAGE OF TIMBER BEAM T3
Compression perpendicular to grain 7.98 %
Shear parallel to grain 27.90 %
Bending parallel to grain 45.40 %
Vertical deflection 83.60 %

## TIMBER BEAM T3 = 2No 150x50mm C24

## BEARING CHECK

	Total			Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
Beam	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
No	Load		Support	Strength	yb*fk/ym			Bearing	-			Padstone	-
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
					1.25xfk/3.5								
T3 (LHS):	Т3	3.44	3.6N Blocks	3.5	1.25	100	88	0.39	-	-	-	-	Satisfacto
T3 (RHS):	Т3	3.44	Beam Connection										

Provide Minimum 100mm End Bearing Length Provide Steel Beam/Column/Timber Post Connection Refer To G.A. for more details. T3 (LHS): T3 (RHS):

# goplans

## TIMBER BEAM T3 - DESIGN DUE TO BS 5268

			Pr	opertie	s of 2No 150	0x50mm		
	Depth h = Depth h = Depth of bearing lb_l = Length of bearing lb_r = Area of beam A = Min modulus of elasticity Vodified min modulus of Modulus of rigidity G = Moment of inertia ly = Section modulus Zy = Root radius ry =	Emin =	=	88 100 12760 7.20 8.21 0.51 2236	mm mm mm mm <sup>2</sup> GPa GPa GPa cm <sup>4</sup> cm <sup>3</sup> cm		Timbe Servic Loads Depth K2 = K3 = K4 = K5 = K7 =	e Clas Duratio haring
I	Forces in beam						K8 = K9 =	
5	Moment Shear Force Axial Force	= = =	1.56 kN 2.32 kN 0.00 kN					
E	Lateral support Ends held in position and Permissible depth-to-bre Actual depth-to-breadth	adth ratio =	eld in line	e, as by 5.000 1.648		ction of sł	neathin	g, dec <mark>OK</mark>
F	Compression perpendi Permissible bearing stre Applied bearing stress σ	ss σc_adm :			N/mm^2 N/mm^2			ок
F	<b>Shear parallel to grain</b> Permissible shear stress Applied shear stress τa =				N/mm^2 N/mm^2			ок
F	Bending parallel to gra Permissible bending stress Applied bending stress	ess σm_adm =	:		N/mm^2 N/mm^2			ок
E	Vertical deflection Total dead and imposed Shear area for beam Ay Beam effective span leff Shear deflection $\delta v$ = Bending deflection $\delta b$ = Total deflection $\delta a$ =	=		4.63 10633 2.80 0.287 6.484 6.771	mm m mm mm			
l	Limiting deflection =	BE 2No 150	c50mm 0	8.100	mm (0.003l	_)		ок

10 Trelawn, Lond	on E10 5QD	
PROJECT	•	
РР	кл	кј
ENG.	CHD.	CHD.
K-25-02-80-C01	24.02.25	0
PROJECT No.	DATE	REV

grade: Class: uration: aring system: Breadth Ratio: C24 1 Medium-term No 5

- 1.00 (Service class 1)
- 1.25 (Medium-term)1.00 (Conservative approach)1.00 (Beam without notch)
- 1.08 (72mm < h ≤ 300mm)
- 1.10 (2No element) 1.14 (2No softwoods element)

PROJECT No.	DATE	REV
К-25-02-80-С01	24.02.25	o
ENG.	CHD.	CHD.
PP	кл	кл

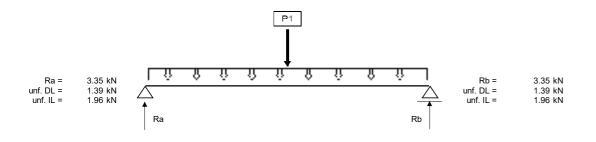
# <u>TIMBER BEAM T4</u> Beam Span L =

2.70 m

	Load Posit	ioned	Elemen	t							
Load	from (m)	to (m)	Span/Hei	ight							
Roof (flat)	0.00	2.70	1.20 m	1	/	2.00	=	0.60 m			
Roof (flat)	0.00	2.70	0.70 m	1	/	2.00	=	0.35 m	а	s Glazing	
	0.00	2.70	0.00 m	1	/	1.00	=	0.00 m		-	
-	0.00	2.70	0.00 m	1	/	1.00	_	0.00 m			
-	0.00	2.70	0.00 m	1	/	1.00	_	0.00 m			
-	0.00	2.70	0.00 m	1							
-	0.00	2.70	0.00 m	1							
UDL LOADING UDL Dead Load Beam Self Weig Roof (flat) Roof (flat)	ding ght 1.00   1.00   0.00   0.00		<b>x</b> × × / /	0.60 n 0.35 n 0.00 n 0.00 n 0.00 n 0.00 n 0.00 n	n = 1 = 1 = 1 = 1 =	0.08 kN/n 0.60 kN/n 0.35 kN/n 0.00 kN/n 0.00 kN/n 0.00 kN/n 0.00 kN/n 1.03 kN/n	1 1 1 1 1 1	x x x x x x	1.00 1.00 1.00 1.00 1.00 1.00 1.00	= = = = = =	0.08 kN/m 0.60 kN/m 0.35 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 1.03 kN/m
<b>UDL Imposed L</b> Roof (flat) Roof (flat)	0.75	kN/m2 kN/m2	x x	0.60 n 0.35 n		0.45 kN/n 0.26 kN/n		x x	1.00 1.00	= =	0.45 kN/m 0.26 kN/m
,	0.00	kN/m2	Х	0.00 n	n =	0.00 kN/n	1 :	X	1.00	=	0.00 kN/m
-	0.00	kN/m2	Х	0.00 n	n =	0.00 kN/n	1 :	X	1.00	=	0.00 kN/m
-	0.00	kN/m2	х	0.00 m	1 =	0.00 kN/n	1 :	Х	1.00	=	0.00 kN/m
-	0.00	kN	/	0.00 m	n =	0.00 kN/n	1 3	X	1.00	=	0.00 kN/m
_	0.00	kN	/	0.00 n	n =	0.00 kN/n	1 :	X	1.00	=	0.00 kN/m
						0.71 kN/n					0.71 kN/m

Point Load P1 @ From Beam = DL = IL =	1.35 m         (CONSERVATIVE APPROACH)           1.00 x AIR SOURCE HEAT PUMP(MAX) + 1.00 x (MAX) + 0.00 kN         x           0.00 kN         x         1.00 =         0.00 kN           2.00 kN         x         1.00 =         2.00 kN	+ 1.0 From Beam = DL =	1.00 x (MAX)	 0.00 kN 0.00 kN
Point Load P3 @	0.00 m			

From Beam = DL = IL = 1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX) 0.00 kN x 1.00 = 0.00 kN x 1.00 = 0.00 kN 0.00 kN



FORCES IN BEAM			DEFLECTION CRITERIA	USAGE OF TIMBER BEAM T4	
			0.003L	Compression perpendicular to grain	9.63 %
Moment	=	2.94 kNm		Shear parallel to grain	33.65 %
Shear Force	=	3.35 kN	DURATION OF LOADING	Bending parallel to grain	71.08 %
Axial Force	=	0.00 kN	Long-term	Vertical deflection	90.08 %

## TIMBER BEAM T4 = 3No 150x50mm C24

## BEARING CHECK

	Total			Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
Beam	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
No	Load		Support	Strength	γb*fk/γm			Bearing				Padstone	
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
					1.25xfk/3.5								
T4 (LHS):	T4	5.09	3.6N Blocks	3.5	1.25	100	132	0.39	-	-	-	-	Satisfactor
T4 (RHS):	T4	5.09	Beam Connection										

Provide Minimum 100mm End Bearing Length Provide Steel Beam/Column/Timber Post Connection T4 (LHS): T4 (RHS): Refer To G.A. for more details.



### TIMBER BEAM T4 - DESIGN DUE TO BS 5268

		Pro	opertie	s of 3No 150	0x50mm		
Depth h = Overall breadth of memil Length of bearing lb_l = Length of bearing lb_r = Area of beam A = Min modulus of elasticity Modified min modulus of Modulus of rigidity G = Moment of inertia ly = Section modulus Zy = Root radius ry =	/ Emin =	=	132 100 190 19140 7.20 8.71 0.54 3353	mm mm mm <sup>2</sup> GPa GPa Gpa cm <sup>4</sup> cm <sup>3</sup> cm		Timbe Servic Loads Depth K2 = K3 = K4 = K5 = K7 = K8 =	e Clas Duratio haring
Forces in beam						K9 =	
Moment Shear Force Axial Force	= = =	2.94 kN 3.35 kN 0.00 kN					
Lateral support Ends held in position and	d members h	neld in line	, as by	direct conne	ction of s	heathin	g, decl
Permissible depth-to-bre Actual depth-to-breadth			5.000 1.098				ок
Compression perpend Permissible bearing stree Applied bearing stress of	ess σc_adm =			N/mm^2 N/mm^2			ок
Shear parallel to grain							
Permissible shear stress Applied shear stress τa				N/mm^2 N/mm^2			ок
Bending parallel to gra	ain						
Permissible bending stre Applied bending stress		=		N/mm^2 N/mm^2			ок
Vertical deflection							
Total dead and imposed			6.71				
Shear area for beam Ay			15950				
Beam effective span left	=		2.80				
Shear deflection δv=			0.338				
Bending deflection δb= Total deflection δa=			0.958				
Limiting deflection =				mm (0.003L	_)		ок
TIMBER BEAM T4 TO	BE 3No 150	x50mm C	24				

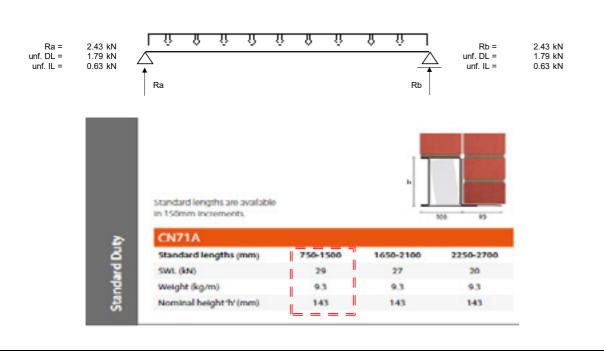
PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
РР	кл	кј
PROJECT		
10 Trelawn, Lond	on E10 5QD	

- grade: Class: uration: aring system: Breadth Ratio:
- C24 1 . Long-term No 5
- 1.00 (Service class 1)
- 1.00 (Long-term) 1.00 (Conservative approach)
- 1.00 (Beam without notch)
- 1.08 (72mm < h ≤ 300mm)
- 1.10 (3No element) 1.21 (3No softwoods element)

# ans go

PROJECT No.	DATE	REV
К-25-02-80-С01	24.02.25	0
ENG.	CHD.	CHD.
PP	кј	кл
PROJECT		
10 Trelawn, Lond	on E10 50D	

### <u>LINTEL L1</u> Clear Span L = Total Span = 1.00 m 1.30 m 1.15 m Effective Span = Load Positioned Element Load Ceiling Roof (sloping) 215mm/Cavity Wall from (m) to (m) 0.00 1.00 Span/Height 2.00 2.00 1.00 1.00 1.00 1.85 m 3.70 m = 1.00 1.00 1.00 1.00 1.00 0.00 0.00 1.08 m 0.40 m 2.15 m | | | = = 0.40 m 0.00 m 0.00 m 0.00 m 0.00 m 0.00 m 0.00 = = 00 r UDL LOADING UDL Dead Loading Ceiling Roof (sloping) 0.45 kN/m2 1.00 kN/m2 1.85 m 1.08 m 0.83 kN/m 1.08 kN/m х = = х 215mm/Cavity Wall 4.20 kN/m2 0.40 m 1.68 kN/m 0.00 kN/m2 0.00 kN/m2 0.00 m 0.00 m 0.00 kN/m 0.00 kN/m 0.00 kN 0.00 m 0.00 kN/m 0.00 kN 0.00 m 3.59 kN/m UDL Imposed Loading Ceiling Roof (sloping) 215mm/Cavity Wall 0.25 kN/m2 1.85 m 0.46 kN/m х 1.08 m 0.40 m 0.81 kN/m 0.00 kN/m 0.75 kN/m2 = 0.00 kN/m2 х = 0.00 kN/m2 0.00 kN/m2 0.00 m 0.00 m 0.00 kN/m 0.00 kN/m 0.00 kN 0.00 kN 0.00 m 0.00 kN/m 0.00 m 1.27 kN/m Total Loads = 4.86 kN/m 5.58 kN Total Loads acting on Lintel = 1.15 m 4.86 kN/m < 29.00 kN х =

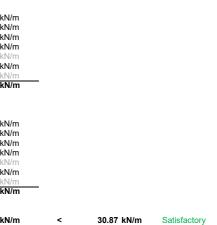


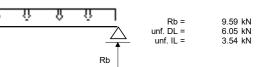
	PROJECT No.	DATE	REV
	K-25-02-80-C01	24.02.25	0
	ENG.	CHD.	CHD.
	РР	кл	кј
	PROJECT	•	
	10 Trelawn, Lond	on E10 5QD	

$ \frac{1000}{1000} \frac{1000}{1000}$	Load         from           Timber floor (1st)         0.0           Ceiling         0.0           Roof (sloping)         0.0           100mm Thick Wall         0.0           -         0.0           T1         0.0           -         0.0           UDL LOADING         0.0	(m)         to (m)           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90           10         0.90	Span/Height 3.60 m 5.50 m 5.50 m 2.70 m 0.00 m						
UDL LOADING UDL Dead Loading         0.00         0.00 m           Timber floor (1st) Ceiling         1.10 kN/m2         x         1.80 m         =         1.98 kN/m           Roof (sloping)         0.45 kN/m2         x         2.75 m         =         1.24 kN/m           Roof (sloping)         1.00 kN/m2         x         2.75 m         =         2.75 kN/m           100mm Thick Wall         2.10 kN/m2         x         2.70 m         =         0.00 kN/m           -         0.00 kN/m2         x         2.70 m         =         0.00 kN/m           T1         2.72 kN         /         1.50 m         =         1.81 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m           -         0.00 kN/m2         x         2.75 m         =         2.06 kN/m           100mm Thick Wall         0.00 kN/m2         x         2.70 m         =         0.00 kN/m           -         0.00 kN/m2         x         0.00 m         =         0.00 kN/m	- 0.0 UDL LOADING				/ /	2.00 = 2.00 = 1.00 =	2. 2. 2.	75 m 75 m 70 m	
UDL Dead Loading           Timber floor (1st)         1.10 kN/m2         x         1.80 m         =         1.98 kN/m           Ceiling         0.45 kN/m2         x         2.75 m         =         1.24 kN/m           Roof (sloping)         1.00 kN/m2         x         2.75 m         =         2.75 kN/m           100mm Thick Wall         2.10 kN/m2         x         2.70 m         =         5.67 kN/m           -         0.00 kN/m2         x         2.70 m         =         5.67 kN/m           -         0.00 kN/m2         x         0.00 m         =         0.00 kN/m           -         0.00 kN         /         1.50 m         =         1.81 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m           -         0.00 kN/m2         x         2.75 m         =         2.06 kN/m           100mm Thick Wall         0.00 kN/m2         x         2.70 m         =         0.00 kN/m           100mm Thick Wall         0.00 kN/m2         x         0.00 m         =         0.00 kN/m           -         0.00 k		· · · ·						(RH	S)
Ceiling $0.45 \text{ kN/m2}$ x $2.75 \text{ m}$ = $1.24 \text{ kN/m}$ Roof (sloping) $1.00 \text{ kN/m2}$ x $2.75 \text{ m}$ = $2.75 \text{ kN/m}$ 100mm Thick Wall $2.10 \text{ kN/m2}$ x $2.70 \text{ m}$ = $5.67 \text{ kN/m}$ - $0.00 \text{ kN/m2}$ x $0.00 \text{ m}$ = $0.00 \text{ kN/m}$ T1 $2.72 \text{ kN}$ / $1.50 \text{ m}$ = $1.81 \text{ kN/m}$ - $0.00 \text{ kN}$ / $0.00 \text{ m}$ = $0.00 \text{ kN/m}$ - $0.00 \text{ kN}$ / $0.00 \text{ m}$ = $0.00 \text{ kN/m}$ - $0.00 \text{ kN}$ / $0.00 \text{ m}$ = $0.00 \text{ kN/m}$ - $0.00 \text{ kN}$ / $0.00 \text{ kN/m}$ = $0.00 \text{ kN/m}$ - $0.25 \text{ kN/m2}$ $2.75 \text{ m}$ = $2.06 \text{ kN/m}$ 100mm Thick Wall $0.00 \text{ kN/m2}$ $2.70 \text{ m}$ $0.00 \text{ kN/m}$ - $0.00 \text{ kN/m2}$ $2.70 \text{ m}$ $0.00 \text{ kN/m}$ - $0.00 \text{ kN/m2}$ $2.70 \text{ m}$ $0.00 \text{ kN/m}$ -<									
100mm Thick Wall       2.10 kN/m2       x       2.70 m       =       5.67 kN/m         -       0.00 kN/m2       x       0.00 m       =       0.00 kN/m         T1       2.72 kN       /       1.50 m       =       1.81 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         Ceiling       0.25 kN/m2       x       2.75 m       =       0.69 kN/m         Roof (sloping)       0.75 kN/m2       x       2.75 m       =       0.00 kN/m         100mm Thick Wall       0.00 kN/m2       x       0.00 m       =       0.00 kN/m         -       0.00 kN/m2       x       0.00 m       =       0.00 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m	Ceiling	0.45 kN/m2	x	2.75 m	= -	1.24 kN/m			
T1       2.72 kN       /       1.50 m       =       1.81 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m         UDL Imposed Loading         Timber floor (1st)       1.50 kN/m2 x       1.80 m       =       2.70 kN/m         Ceiling       0.25 kN/m2 x       2.75 m       =       0.69 kN/m         Roof (sloping)       0.75 kN/m2 x       2.75 m       =       0.69 kN/m         100mm Thick Wall       0.00 kN/m2 x       2.70 m       =       0.00 kN/m         -       0.00 kN/m2 x       0.00 m       =       0.00 kN/m         -       0.00 kN       /       1.50 m       =       2.41 kN/m         -       0.00 kN       /       0.00 m       =       0.00 kN/m									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$									
UDL Imposed Loading         1.50 kN/m2         x         1.80 m         =         2.70 kN/m           Ceiling         0.25 kN/m2         x         2.75 m         =         0.69 kN/m           Roof (sloping)         0.75 kN/m2         x         2.75 m         =         2.06 kN/m           100mm Thick Wall         0.00 kN/m2         x         2.70 m         =         0.00 kN/m           -         0.00 kN/m2         x         0.00 m         =         0.00 kN/m           T1         3.61 kN         /         1.50 m         =         2.41 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m					=	0.00 kN/m			
Timber floor (1st)1.50 kN/m2x1.80 m=2.70 kN/mCeiling0.25 kN/m2x2.75 m=0.69 kN/mRoof (sloping)0.75 kN/m2x2.75 m=2.06 kN/m100mm Thick Wall0.00 kN/m2x2.70 m=0.00 kN/m-0.00 kN/m2x0.00 m=0.00 kN/mT13.61 kN/1.50 m=2.41 kN/m-0.00 kN/0.00 m=0.00 kN/m					1	3.45 kN/m			
Timber floor (1st)1.50 kN/m2x1.80 m=2.70 kN/mCeiling0.25 kN/m2x2.75 m=0.69 kN/mRoof (sloping)0.75 kN/m2x2.75 m=2.06 kN/m100mm Thick Wall0.00 kN/m2x2.70 m=0.00 kN/m-0.00 kN/m2x0.00 m=0.00 kN/mT13.61 kN/1.50 m=2.41 kN/m-0.00 kN/0.00 m=0.00 kN/m	UDL Imposed Loading								
Roof (sloping)         0.75 kN/m2         x         2.75 m         =         2.06 kN/m           100mm Thick Wall         0.00 kN/m2         x         2.70 m         =         0.00 kN/m           -         0.00 kN/m2         x         0.00 m         =         0.00 kN/m           -         0.00 kN/m2         x         0.00 m         =         0.00 kN/m           -         0.00 kN         /         1.50 m         =         2.41 kN/m           -         0.00 kN         /         0.00 m         =         0.00 kN/m									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Roof (sloping) (	0.75 kN/m2	x	2.75 m	= :	2.06 kN/m			
T1 3.61 kN / 1.50 m = 2.41 kN/m - 0.00 kN / 0.00 m = 0.00 kN/m <b>7.86 kN/m</b>									
7.86 kN/m	T1 3	3.61 kN	1	1.50 m	= :	2.41 kN/m			
Total Loads acting on Lintel = 21.31 kN/m < 30.87 kN/m Satisfacto	- (	0.00 KN	/	0.00 m					
Ra = 9.59 kN unf. DL = 6.05 kN unf. IL = 3.54 kN	unf. DL =	9.59 kN	-						Rb = unf. DL =
		MI Soco Pr						I	
Ra Rb		and appendix the						_	
Hi-Spec Range 64 R6 R9 R12		Lond Table						. 25	• 290
Hi-Spec Range 54 R6 R9 R12		Units suitat	ole		100		8	100	
Hi-Spec Range 54 R6 R9 R12		Units suitat for 100mm	vide walls	30	100	30	3 10 10 10 10 10	1000	30
Hi-Spec Rango     54     R6     R9     R12       Load Table Units suitable for 100mm wide walls     Image: 100 Image: 100 Ima		Units suitet for 100mm Fire Resistance Suitable For Fox	Available (mina) undation Use	Yes	10	Yes	W	0 09	Yes
HI-Spec Range     64     R6     R9     R12       Load Table Units suitable for 100mm wide walls     Image walls<		Units suitet for 100mm Fire Resistance Suitable For Fox	Available (mina) undation Use	Yes	wn	Yes	W	0 00 000mm	Yes 3600mm
Hi-Spec Rango     54     R6     R9     R12       Load Table Units suitable for 100mm wide walls     Image: 100 Image: 100 Ima		Units suitab for 100mm Fire Resistance Suitable For Fou Maximum Stock	Available (mins) Available (mins) undation Use Length Available	Yes 3000m		Yes 3000mm	3	0 55 500mm Enrger langths a 1 up to	Yes 3600mm setable on sequent 4800mm
Hi-Spec Range       54       R6       R9       R12         Load Table Units autable for 100mm wide walls       Image autable Image autable for 100mm wide walls       Image autable Image		Units suiteb for 100mm	Available (mina) Available (mina) undation Use Longth Available Pinisth	Ves 9 3000m Faced	UNF	Yes 3000mm Faced	ED LOA	togen biodomen Longer lengths a aced	Yes 3600mm addition on segand 600mm Faced
Hi-Spec Range     54     R6     R9     R12       Load Table Units suitable for 100mm wide walls     Image of the suitable (mine)     Image of the		Units suiteb for 100mm	Available (mina) Available (mina) undation Use Length Available Pinish Clear Span	Vite           3000m           Faced           100m1	UNF	Yes 3000mm Faced ACTOR 100x140	ED LOA	5 500mm Longer lengths a op to acced DIS IN kN/m 00x215	Yes 3600mm dd00mm Faced 100x290
Hi-Spec Range       54       R6       R9       R12         Load Table Units autable for 100mm wide walls       Image autable Image autable for 100mm wide walls       Image autable Image		Units suiteb for 100mm Fire Resistance Suitable For Fox Maximum Stock Available Range Length 900mm	Available (mins) undation Use Longth Available Pinists Clear Span 700mm	Ves 9 3000m Faced 100x1 15.77	U N F	Yes 3000mm Faced ACTOR 100x140 38.73	11 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	Yes 3600mm 4600mm Faced 100x200 127.77

Satisfactory

=	1.80 m
=	2.75 m
=	2.75 m
=	2.70 m
=	0.00 m

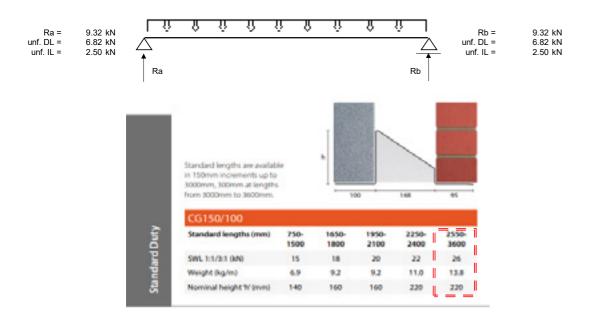




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PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	кл	кл

LINTEL L3 Clear Span L = Total Span = Effective Span =	3.00 m 3.30 m 3.15 m									
	Load Positioned	Element								
Load	from (m) to (m) 0.00 3.00	Span/Heigl	nt	,	2.00 =	1.35 m				
Roof (flat)	0.00 3.00 0.00 3.00	2.70 m 0.00 m		1	<b>2.00 =</b> 1.00 =					
-				1	1.00 =	0.00 m				
215mm/Cavity Wall	0.00 3.00 0.00 3.00	0.65 m 0.00 m		1		0.65 m				
-				1	1100	0.00 m				
-	0.00 3.00	0.00 m		/	1.00 =	0.00 m				
T4	0.00 3.00	3.00 m					(MAX)			
-	0.00 3.00	0.00 m								
UDL LOADING UDL Dead Loading										
Roof (flat)	1.00 kN/m2	x	1.35 m	=	1.35 kN/m					
	0.00 kN/m2	X	0.00 m	=	0.00 kN/m					
215mm/Cavity Wall	4.20 kN/m2	x	0.65 m	=	2.73 kN/m					
2 I JIIIII/Gavity Wall	0.00 kN/m2	x	0.00 m	_	0.00 kN/m					
	0.00 kN/m2	x	0.00 m	_	0.00 kN/m					
- T4	1.39 kN	î	3.00 m	=	0.46 kN/m					
14	0.00 kN	/	0.00 m	_	0.00 kN/m					
-	0.00 KN	/	0.00 111	-	4.54 kN/m	-				
UDL Imposed Load	ing									
Roof (flat)	0.75 kN/m2	х	1.35 m	=	1.01 kN/m					
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m					
215mm/Cavity Wall	0.00 kN/m2	х	0.65 m	=	0.00 kN/m					
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m					
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m					
T4	1.96 kN	1	3.00 m	=	0.65 kN/m					
-	0.00 kN	/	0.00 m	=	0.00 kN/m					
				-	1.67 kN/m	-				
		Total	Loads	=	6.21 kN/m					
Total Loads acting	on Lintel =	3.15 m		x	6.21 kN/m	=	19.56 kN	<	26.00 kN	Satisfactory

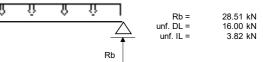


<u>BEAM EB1</u> Beam Span L =	3.70	m			(0
	Load Posi		Element		1
Load	from (m)		Span/Heigh	nt	
100mm Thick Wall	0.00	3.70	2.70 m		
Roof (sloping)	0.00	3.70	5.50 m		
-	0.00	3.70 3.70	0.00 m 0.00 m		
-	0.00	3.70	0.00 m		
-	0.00	3.70	0.00 m		
_	0.00	3.70	0.00 m		
JDL LOADING JDL Dead Loading Beam Self Weight 100mm Thick Wall Roof (sloping)	2.10 1.00 0.00 0.00		<b>x</b> × × / /	2.70 2.75 0.00 0.00 0.00 0.00 0.00	m m m m

C	JO			าร		PROJECT No. K-25-02-80-C01 ENG. PP	DATE 24.02.25 CHD. KJ	REV O CHD. KJ
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~						PROJECT 10 Trelawn, Lon	idon E10 5QD	
BEAM EB1 Beam Span L =	3.70 m		(Calculate	ed For Loading Purpo	ses Only)			
.oad 00mm Thick Wall Roof (sloping)	Load Positioned           from (m)         to (m)           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70           0.00         3.70	Element Span/Height 2.70 m 5.50 m 0.00 m 0.00 m 0.00 m 0.00 m 0.00 m	/ / / /	1.00       =         2.00       =         1.00       =         1.00       =         1.00       =	2.70 2.75 0.00 0.00 0.00	<b>m</b> m		
JDL LOADING JDL Dead Loading Beam Self Weight OOmm Thick Wall Roof (sloping)	2.10 kN/m2 1.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN 0.00 kN	<b>x</b> <b>x</b> × × / /	2.70 m = 2.75 m = 0.00 m = 0.00 m = 0.00 m = 0.00 m =	0.23 kN/m 5.67 kN/m 2.75 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 8.65 kN/m	<b>x</b> <b>x</b> <b>x</b> × × × ×	1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =         1.40       =	0.32 kN/m 7.94 kN/m 3.85 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 12.11 kN/m	
JDL Imposed Load 00mm Thick Wall Roof (sloping)	ling 0.00 kN/m2 0.75 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN 0.00 kN	<b>x</b> x x x / /	2.70 m = 2.75 m = 0.00 m = 0.00 m = 0.00 m = 0.00 m =	0.00 kN/m 2.06 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 2.06 kN/m	<b>x</b> x x x x x	1.60       =         1.60       =         1.60       =         1.60       =         1.60       =         1.60       =         1.60       =         1.60       =	0.00 kN/m 3.30 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m 3.30 kN/m	
Point Load P1 @           From Beam         =           DL         =           L         =           Point Load P3 @           From Beam         =           DL         =	0.00 m 1.00 x (MAX) + 1.0 0.00 kN x	1.40 = 1.60 =	0.00 kN 0.00 kN	Point Load From Bear DL IL				0.00 kN 0.00 kN

1 1 1 1 1 1 1 1 1 1 Ra = 28.51 kN unf. DL = 16.00 kN unf. IL = 3.82 kN  $\bigtriangleup$ . Ra

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24.02.25	o
CHD.	CHD.
кј	кл

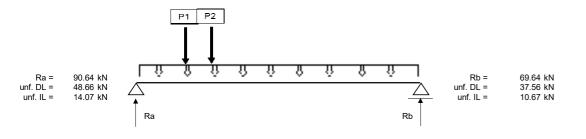
# <u>BEAM B1</u> Beam Span L =

3.75 m

Element Span/Height 2.70 m 3.70 m Load Positioned Load Roof (flat) Timber floor (1st) from (m) to (m) 0.00 3.75 2.00 2.00 2.00 2.00 1.35 m 1.85 m = 0.00 3.75 = Ceiling Roof (sloping) 215mm/Cavity Wall 0.00 0.00 3.75 3.75 3.70 m = = 1.85 m 2.15 m 1 1 08 m 0.00 3.75 3.00 m 1.00 3.00 m Avg. - due to window openings UDL LOADING UDL Dead Loading Beam Self Weight 1.40 1.40 1.40 1.40 1.40 1.40 0.46 kN/m 0.65 kN/m х 1.35 m 1.85 m 1.00 kN/m2 1.35 kN/m 2.04 kN/m Roof (flat) 1.89 kN/m х = 1.10 kN/m2 2.85 kN/m Timber floor (1st) = х = х Ceiling Roof (sloping) 0.45 kN/m2 1.85 m 0.83 kN/m = 1.17 kN/m 1.51 kN/m 1.00 kN/m2 1.08 m 1.08 kN/m = х 215mm/Cavity Wall 4.20 kN/m2 3.00 m 12.60 kN/m 17.64 kN/m Х 0.00 kN 0.00 kN 0.00 m 0.00 m 1.40 1.40 0.00 kN/m 18.35 kN/m \_ 25.69 kN/m UDL Imposed Loading Roof (flat) 1.60 1.60 1.60 1.60 1.60 0.75 kN/m2 1.35 m 1.01 kN/m 1.62 kN/m Х х Timber floor (1st) 1.85 m 1.85 m 1.50 kN/m2 = 2.78 kN/m = 4.44 kN/m Ceiling 0.25 kN/m2 0.46 kN/m 0.74 kN/m = х х Roof (sloping) 215mm/Cavity Wall 0.75 kN/m2 1.08 m = 0.81 kN/m = 1.29 kN/m х 0.00 kN/m2 0.00 kN/m 3.00 m 0.00 kN/m = х = x 0.00 kN 0.00 kN 1.60 1.60 0.00 m 0.00 kN/r 0.00 kN/n 0.00 m 5.06 kN/m 8.09 kN/m

Point Load P1 @	0.65 m	Point Load P2 @	1.00 m		
From Beam =	1.00 x EB1(MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x T4(RHS)		
DL =	16.00 kN x 1.40 = 22.40 kN	DL =	1.39 kN x	1.40 =	1.95 kN
IL =	$3.82 \text{ kN} \times 1.60 = 6.11 \text{ kN}$	IL =	1.96 kN x	1.60 =	3.14 kN

Point Load P3 @ 0.00 m 1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX) 0.00 kN x 1.40 = 0.00 kN 0.00 kN x 1.60 = 0.00 kN From Beam = DL = =



FORCES IN BEAM			DEFLECTION CRITERIA	USAGE OF STEEL BEAM B1	
Moment Shear Force Axial Force	= = =	71.78 kNm 90.64 kN 0.00 kN	L/300; Brittle finishes (all loads) L/360 (imposed loads only)	Shear capacity Moment capacity Buckling resistance moment Vertical deflection	29.09 % 44.94 % 57.91 % 63.15 %

BEAM WITH PLATE, SEE DETAILS ON SUMMARY PAGE

## STEEL BEAM B1 = 203 x 203 x 46 UKC S355

BEARING CHECK

	Total			Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
Beam	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
No	Load		Support	Strength	yb*fk/ym			Bearing				Padstone	
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
	B1												
B1 (LHS):		90.64	Beam Connection										
	B1												
B1 (RHS):		69.64	Beam Connection										1
Beam Support B1 (LHS): B1 (RHS):	Provide St	el Beam	/Column/Timber Post ( /Column/Timber Post (						Restraint (	aring design Condition Co Condition Co	oef. Suppo		1.0 + 2 x 1.0 + 2 x

# goplans

## STEEL BEAM B1 - DESIGN DUE TO BS 5950-1

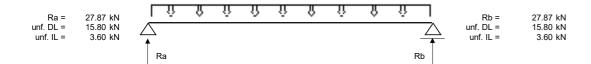
	Properties of 203 x 203 x	46 UKC Section	
Design strength of steel py = Half of flange b = Flange thickness T = Area of cross-section A = Rad of gyration (minor axis) r = Modulus of elasticity E = Elastic modulus Zx =	355.00 N/mm <sup>2</sup> 101.80 mm 11.0 mm 58.7 cm <sup>2</sup> 5.13 cm 205.00 GPa 450 cm <sup>3</sup>	Total beam span L = Web depth d = Web thickness t = Overall depth D = Overall breadth B = Moment of inertia Ix = Plastic modulus Sx = Root radius r =	3.75 m 160.80 mm 7.2 mm 203.2 mm 203.6 mm 4570 cm <sup>4</sup> 497 cm <sup>3</sup> 10.20 mm
Forces in beam		Beam bearing design details	5
	71.78 kNm 90.64 kN 0.00 kN	Restraint Condition Coef. Sup Restraint Condition Coef. Sup	
Classification of cross-section			
Parameter ε =	0.880		
Web d/t = Web (d/t)/ $\epsilon$ =	22.33 25.37 ≤ 80	Class 1 plastic	
Flanges b/t = Flanges (b/t)/ε =	9.25 10.51 ≤ 15	Class 3 semi-compact	
	Section is class 3 semi-	compact	
Shear capacity			
Shear area Av = Web (d/t)/ε = Shear capacity Pv =	311.63 kN	es not need to be checked for shear b	uckling)
Design shear force =	90.64 kN	OK	
Moment capacity Design bending moment M= Moment capacity low shear Mc =	71.78 kNm 159.75 kNm (Mc = py	*Z) <b>OK</b>	
Effective length for lateral-torsion	-		
Total Beam Span = Effective length Le =	3750 mm 4156 mm		
Slenderness ratio $\lambda$ =	81.02		
Equivalent slenderness			
Buckling parameter u =	0.847		
Torsional index x = Slenderness factor v =	17.7 0.836		
Ratio βw =	0.836 0.905 (Z/S)		
Equivalent slenderness $\lambda LT =$	54.59		
Limiting slenderness λL0 =	30.20		
$\lambda LT > \lambda L0$ (Allowance should be r	nade for lateral-torsional buck	ling)	
Bending strenght Bending strenght ρb =	275.48 N/mm^2 (With	Table 16)	
Buckling resistance moment	T = 1.00 (Canaan with a	approach)	
Equivalent uniform moment factor ml Buckling resistance moment Mb =	LT = 1.00 (Conservative a 123.97 kNm	арргоаст)	
Design bending moment	71.78 kNm	ОК	
Vertical dead & imposed load defle		ttla finiahaa)	
Limiting deflection = Maximum deflection =	12.500 mm (L/300; Bri 7.893 mm	OK	
Vertical imposed load deflection			
Limiting deflection =	10.417 mm (L/360)		
Maximum deflection =	1.783 mm	ОК	
STEEL BEAM B1 = 203 x 203 x 46	<u>UKC</u>		

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PROJECT No.	DATE	REV			
K-25-02-80-C01	24.02.25	o			
ENG.	CHD.	CHD.			
PP	кл	кј			
PROJECT					
10 Trelawn, Lond	on E10 5QD				

10 Trelawn, London E10 5QD						
PROJECT		I				
РР	кј	кј				
ENG.	CHD.	CHD.				
К-25-02-80-С01	24.02.25	o				
PROJECT No.	DATE	REV				

<b>BEAM B1.</b> Beam Span L =	1.70 m		(Cal	culated	For Loading Purpos	ses Only)			
Load Roof (flat) Timber floor (1st) Ceiling Roof (sloping) 215mm/Cavity Wall	Load Positioned           from (m)         to (m)           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70           0.00         1.70	Element Span/Heigh 2.70 m 2.60 m 3.70 m 2.15 m 3.20 m 0.00 m 0.00 m		     	2.00 = 2.00 = 2.00 = 2.00 = 1.00 =	1.35 m 1.30 m 1.85 m 1.08 m 3.20 m	Þ	Avg, due	e to window opening
UDL LOADING UDL Dead Loading Beam Self Weight Roof (flat) Timber floor (1st) Ceiling Roof (sloping) 215mm/Cavity Wall	1.00 kN/m2 1.10 kN/m2 0.45 kN/m2 1.00 kN/m2 4.20 kN/m2 0.00 kN	x x x x / /	1.35 m 1.30 m 1.85 m 1.08 m 3.20 m 0.00 m 0.00 m		0.46 kN/m 1.43 kN/m 1.43 kN/m 0.83 kN/m 1.08 kN/m 13.44 kN/m 0.00 kN/m <b>18.59 kN/m</b>	x x x x x x x x x	1.40 1.40 1.40 1.40 1.40 1.40 1.40		0.65 kN/m 1.89 kN/m 2.00 kN/m 1.17 kN/m 1.51 kN/m 18.82 kN/m 0.00 kN/m 26.02 kN/m
UDL Imposed Load Roof (flat) Timber floor (1st) Ceiling Roof (sloping) 215mm/Cavity Wall	ing 0.75 kN/m2 1.50 kN/m2 0.25 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN 0.00 kN	x x x x x / /	1.35 m 1.30 m 1.85 m 1.08 m 3.20 m 0.00 m	= = = = =	1.01 kN/m 1.95 kN/m 0.46 kN/m 0.81 kN/m 0.00 kN/m 0.00 kN/m 4.23 kN/m	x x x x x x x x	1.60 1.60 1.60 1.60 1.60 1.60 1.60	= = = =	1.62 kN/m 3.12 kN/m 0.74 kN/m 1.29 kN/m 0.00 kN/m 0.00 kN/m 6.77 kN/m
Point Load P1 @ From Beam = DL = L = Point Load P3 @ From Beam =		1.40 = 1.60 =	0.00 kN 0.00 kN		Point Load From Beam DL IL		0.00 m 1.00 x (M 0.00 kl 0.00 kl	IAX) N x	1.40 = 0.00 1.60 = 0.00



## BEARING CHECK

	Total			Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
Beam	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
No	Load		Support	Strength	yb*fk/ym			Bearing	-			Padstone	
	From	kN		fk, N/mm2	N/mm2	mm	mm	N/mm2	mm	mm	mm	N/mm2	
	B1.												
B1. (LHS):		27.87	Beam Connection										
	B1.												
B1. (RHS):		27.87	Beam Connection										

Beam Support So B1. (LHS): B1. (RHS): Summary: Provide Steel Beam/Column/Timber Post Connection Provide Steel Beam/Column/Timber Post Connection Refer To G.A. for more details.

g	C	p	la	ns		PROJECT No. <b>K-25-02-80-C01</b> ENG. <b>PP</b> PROJECT	DATE 24.02.25 CHD. KJ		REV <b>0</b> CHD. KJ
						10 Trelawn, Londo	on E10 5QD		
<u>MN C2</u> n Height, L =	3.35 n	n				DESIGN	DUE TO BS (	5950-1:2000	
	2 x 152 x .2mm ; rx		S355 '0cm ; Ag = 29.20	E = 205.00 kN/ cm2 ; lx = 1250cm4 ;		: 164cm3 ; Zy = 52.6	6cm3 ; u = 0.84	42 ; x = 20.6	
Axis x-x: Le> Axix y-y: Ley		I.5 * L = 5.0 I.5 * L = 5.0	3 m 3 m	Slenderness: Slenderness: Slenderness fa	λy =	Lex / rx = 76.8 Ley / ry = 135.8 1/ [1 + 0.05 (λy /x)^	1 (	ЭК ЭК = 0.75	
CAL LOAD				Equiv. Slender		υνλγ√βw ΄΄΄		= 85.68	
			DL =	= 0.00 kN	(MAX) + 1.00 x (M 76.10 mm	IAX)			
eam = 1.00 x B1	.(RHS) +	• 1.00 x (MAX) + 1.0	0 x (MAX)	×		From Beam = 1.00 ;	x B1(LHS) + 1	.00 x (MAX) + 1.00 x	(MAX)
= = icity =	15.80 k 3.60 k D/2 =		у		У	DL = IL = Eccentricity =	48.66 k 14.07 k D/2 =		
				× .00 x (MAX) + 1.00 x	(MAX) + 1.00 x (M	IAX)			
				= 0.00 kN	-76.10 mm				
ONTAL LOAD bad orizontal Load uction bad Applied in		= = = =	0.00 kN/r 0.00 m2 0.00 kN Simply Su Major Axis	oported					
N LOADING ANI	D MOME	NT BS 595	0 2.4.1.2						
ombination 1 + 1.6 IL			Load Co 1.4 DL +	mbination 2 1.4 WL		Load Combin 1.2 DL + 1.2			
orce force t x-x t y-y	= = = =	118.52 kN 0.00 kN 4.78 kNm 0.00 kNm	Axial For Shear Fo Moment Moment	x-x =	90.25 kN 0.00 kN 3.51 kNm 0.00 kNm	Axial Force Shear Force Moment x-x Moment y-y	= = =	98.56 kN 0.00 kN 3.96 kNm 0.00 kNm	
e <b>d Forces</b> xial Force, Fc hear Force ajor Moment x-x, inor Moment y-y,		= = = =	118.52 kN 0.00 kN 4.78 kNm 0.00 kNm	Max Max Max Max	actored Forces (. Axial Force DL (. Axial Force IL (. Shear Force (. Moment x-x (. Moment y-y		= = = =	64.46 kN 17.67 kN 0.00 kN 3.30 kNm 0.00 kNm	
ABLE STRESS Strength of Stee essive Strength Strength	l p p	by = bcy = bb =	355.00 N/m 87.00 N/m 175.00 N/m	m2 m2 (tab	le 24, curve c)	s, pb = py for SHS se		0.00 KINIII	
L ession Resistance t Capacity (Major t Capacity (Minor g Resistance Mo	rAxis) M rAxis) M	Pcy = Ag * pcy Mc,x = py * Zx Mc,y = py * Zy Mb= pb * Zx	= =	54.04 kN 58.22 kNm 18.67 kNm 28.70 kNm (Fo	SHS Sections Mb	o = Mc,x)			
ARY Pcy 「*Mx/Mb ; n *My/Mc,y ; n		)	= = =	0.47 0.17 0.00	OK OK OK				
<b>CTIONS</b> le Deflection t from vertical loa loads max defle	ads: x-x	1] + [2] + [3] = L/300 M M*L^2 / 16E	= =	< 1.00 11.17 mm 3.30 kNm 0.90 mm	ок				
nt from vertical loa I loads max defle oad Horizontal for	ads: y-y ction: y-y ce	M M*L^2 / 16E H	= = =	0.00 kNm 0.00 mm 0.00 kN					
oads maximum de eflection	eflection	H * L^3 / 48E	=	0.00 mm 0.90 mm	ОК	STEEL (	COLUMN C2 =	= 152 x 152 x 23 UK	C (S355)

C	0		a	n	5	PROJECT No. K-25-02-80-C01 ENG. PP	DATE 24.02.25 CHD. KJ		REV <b>0</b> CHD. <b>KJ</b>
3						PROJECT 10 Trelawn, Londo	on E10 5QD		
COLUMN C2 Column Height, L =	3.35 m					DESIGN	DUE TO BS 5	5950-1:2000	
	52 x 152 x 23 2.2mm ; rx =				kN/mm2 n4 ; ly = 400cm4 ; Zx	= 164cm3 ; Zy = 52.6	cm3 ; u = 0.84	42 ; x = 20.6	
,		* L = 5.03 * L = 5.03		Slendernes Slendernes	ss: λy =	Lex / rx = 76.8 Ley / ry = 135.8	1 C	OK OK	
/ERTICAL LOAD				Slendernes Equiv. Sler		1/[1 + 0.05 (λy/x)^2 uvλy √βw	2]^0.25	= 0.75 = 85.68	
			From Beam = 1.00 DL = IL = Eccentricity =	0.00		MAX)			
From Beam = 1.00 x B	1.(RHS) + 1. 15.80 kN	00 x (MAX) + 1.00	. ,	×		From Beam = 1.00 x	c B1(LHS) + 1. 48.66 k		(MAX)
ccentricity =	3.60 kN D/2 =	76.20 mm	<u> </u>		У	IL = Eccentricity =	14.07 k		
			From Beam = 1.00 DL = IL =	× (MAX) + 1.0 0.00 0.00		MAX)			
IORIZONTAL LOAD Vind Load vrea otal Horizontal Load Construction Vind Load Applied in		= = = =	Eccentricity = 0.00 kN/m2 0.00 m2 0.00 kN Simply Suppor Major Axis (x-)	ted	-76.10 mm				
ESIGN LOADING AN									
oad Combination 1 .4 DL + 1.6 IL			Load Combir 1.4 DL + 1.4			Load Combin 1.2 DL + 1.2 I			
ixial Force Shear Force Moment x-x Moment y-y	= · ·	118.52 kN 0.00 kN 4.78 kNm 0.00 kNm	Axial Force Shear Force Moment x-x Moment y-y	= = = =	90.25 kN 0.00 kN 3.51 kNm 0.00 kNm	Axial Force Shear Force Moment x-x Moment y-y	= = = =	98.56 kN 0.00 kN 3.96 kNm 0.00 kNm	
actored Forces Max. Axial Force, Fc Max. Shear Force Max. Major Moment x-: Max. Minor Moment y-y		= = = =	118.52 kN 0.00 kN 4.78 kNm 0.00 kNm		Unfactored Forces Max. Axial Force DL Max. Axial Force IL Max. Shear Force Max Moment x-x Max Moment y-y		= = = =	64.46 kN 17.67 kN 0.00 kN 3.30 kNm 0.00 kNm	
ALLOWABLE STRES Design Strength of Ste Compressive Strength Bending Strength	el py	= = =	355.00 N/mm2 87.00 N/mm2 175.00 N/mm2		(table 24, curve c) (table 16 for I-section	ns, pb = py for SHS se	ections)		
CTUAL compression Resistan loment Capacity (Maj loment Capacity (Min luckling Resistance M	or Axis) Mc, or Axis) Mc,	y = Ag * pcy x = py * Zx y = py * Zy = pb * Zx	= 18.6	2 kNm 7 kNm	(For SHS Sections M	/lb = Mc,x)			
<b>SUMMARY</b> 1] Fc / Pcy 2] mLT * Mx / Mb ; 3] my * My / Mc,y ;			= 0.4 = 0.1 = 0.0	7	ок ок ок				
EFLECTIONS llowable Deflection loment from vertical k ertical loads max defl loment from vertical loads max defl /ind loads max defl	bads: x-x ection: x-x bads: y-y ection: y-y prce	+ [2] + [3] = L/300 M M*L^2 / 16EI M M*L^2 / 16EI H	= 3.3 = 0.9 = 0.0 = 0.0 = 0.0	1.00 7 mm 80 kNm 90 mm 90 kNm 90 mm 90 kN	ОК				
	deflection	H * L^3 / 48EI	= 0.0	00 mm					

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10 Trelawn, London E10 5QD						
PROJECT						
PP	кл	кл				
ENG.	CHD.	CHD.				
K-25-02-80-C01	24.02.25	o				
PROJECT No.	DATE	REV				

## LOADS ACTING ON THE FOOTING (BELOW COLUMN C1)

Load Positioned		ioned	Element				
Load	from (m)	to (m)	Span/Height				
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m				
-	0.00	1.00	0.00 m				

# UDL LOADING UDL Dead Loading

Selfweight	24.00 kN/m3	х	0.10 m2	=	2.43 kN/m	х	1.00	=	2.43 kN/m
-	0.00 kN/m2	X	0.00 m	=	0.00 kN/m	X	1.00	=	0.00 kN/m
	0.00 kN/m2	X	0.00 m	_	0.00 kN/m	X	1.00	_	0.00 kN/m
-	0.00 kN/m2	X	0.00 m	=	0.00 kN/m	X	1.00	_	0.00 kN/m
-	0.00 kN/m2	X	0.00 m	_	0.00 kN/m	X	1.00	_	0.00 kN/m
-	0.00 kN/m2	X	0.00 m	_	0.00 kN/m	X	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	X	1.00	=	0.00 kN/m
-	0.00 kN	,	0.00 m	-	0.00 kN/m	X	1.00	=	0.00 kN/m
				-	2.43 kN/m	-		-	2.43 kN/m
UDL Imposed Lo									
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
				_	0.00 kN/m	-		-	0.00 kN/m

Point Load P1	
From Beam =	

From Beam = DL = IL =	1.00 x B1.(LHS) + 1.00 x (MAX) + 1.00 x (MAX) 15.80 kN x 1.00 = 15.80 kN 3.60 kN x 1.00 = 3.60 kN	SUM:	19.40 kN
Point Load P2			
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)		
DL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$		
IL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	SUM:	0.00 kN

### DESIGN FORCES

STRIP FOOTING OPTION Vertical Force	Ν	=	20.85 kN	1*B1. (LHS)+UDL*Load Dispersion Length
PAD FOUNDATION OPTION				
Vertical Force	Pz	=	19.40 kN	1*B1. (LHS)+UDL*Pad Dimension
Horizontal Force in x direction	Fx	=	0.00 kN	
Horizontal Force in y direction	Fy	=	0.00 kN	
Major axis moment x-x	Mxx	=	0.00 kNm	
Major axis moment y-y	Муу	=	0.00 kNm	
Eccentricity x-x	ex	=	225.00 mm	
Eccentricity y-y	ey	=	0.00 mm	

Allowable Bearing Capacity of Soil

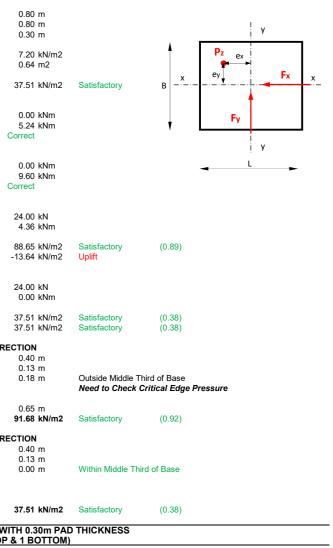
= 100.00 kN/m2

# goplans

LOCATION: COLUMN STRIP FOOTING OPT													
Plan Area Required		N/Allowable	Bearing Capacity o	of Soil	=	0.21 n	n2						
			bearing capacity o	0.001									
Minimum Footing Widt Minimum Footing Dept		W D			=	0.45 n 0.60 n							
Plan Area Provided		W*(D)			=	0.27 n	n2						
Plan Area Required	<	Plan Area F	Provided	Satisfactor	v	(0.77)							
BEARING CHECK BE													
	Total		ADSTONE	Charact.	Local	Bearing	Bearing	Stress	Padstone	Padstone	Ecc	Stress	
	Vertical		Type of	Compr.	Strength	Length	Width	Below	Length	Width		Below	Summary
	Load From	kN	Support	Strength fk, N/mm2	γb*fk/γm N/mm2	mm	mm	Bearing N/mm2	mm	mm	mm	Padstone N/mm2	
c		27.87	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	-	-	-	300	215	0	0.43	Satisfactor
COLUMN C1 Padste						<b>I</b>						1	1
Р	rovide M	IN 300x(Wal	I Width)x215 Concre	ete Padstone	•								
- DIS	TANCE		OOTINGS ARE S D FROM BASEP							THAN 0.	60m		
		S NOT LES	S THAN 0.45m; I	FOOTING	HICKNES	SS IS NOT	LESS T	HAN 0.22	5m FOR N	IEW STRI	P FOOTI	NG	
PAD FOUNDATION C													
FOUNDATION DIMEN Length of Pad Footing		L			=	0.80 n	n						
Width of Pad Footing		B			=	0.80 n						1	
Depth of Pad Footing		Н			=	0.30 n	n					У	
Pad Foundation Selfwe	aight	Sf			_	7 00 1	NI/m 0			4	Pz		
Area of Pad Foundation	5	A=L*B			=	7.20 k 0.64 n					ey	ex	Fx v
Bearing Pressure		(Pz+Sf)/A			=	37.51 k	N/m2	Satisfactor	У	в	¥	··-·	<b>FX</b> X
CHECK STABILITY A				ON	_	0.00 k	N Inn					1	
Total Overturning Mon Total Restoring Mome		Mox=Myy+F Mrx=Pz*(1/2	-х^н 2-ex)+Sf*A*L/2		=	0.00 k 5.24 k				•	F	y I	
Overturning Safety Fac		FOS=Mrx/N			=	Correct							
CHECK STABILITY A Total Overturning More		OVERTURN Moy=Mxx+F		ON	=	0.00 k	Nm					įΥ L	
Total Restoring Mome			2-ey)+Sf*A*B/2		=	9.60 k					4		-
Overturning Safety Fac		FOS=Mry/N			=	Correct							
PAD FOUNDATION B				IRES IN X-D	IRECTION								
Total Pad Base Reacti Total Pad Base Mome		T=Pz+Sf*A Mbx=Myy+F			=	24.00 k 4.36 k							
										(0.00)			
Maximum Base Presso Minimum Base Presso			+6*Mbx/(B*L*L) 6*Mbx/(B*L*L)		=	88.65 k -13.64 k		Satisfactor Uplift	У	(0.89)			
PAD FOUNDATION B			ND BASE PRESSU	IRES IN Y-D	IRECTION								
Total Pad Base Reacti Total Pad Base Mome		T=Pz+Sf*A Mby=Mxx+F	Pz*ey+Fy*H		=	24.00 k 0.00 k							
Maximum Base Press	ure	gvmax=T/A	+6*Mby/(L*B*B)		=	37.51 k	N/m2	Satisfactor	v	(0.38)			
Minimum Base Pressu			6*Mby/(L*B*B)		=	37.51 k		Satisfactor		(0.38)			
CHECK PAD BASE R	EACTIO		RICITY AND BEARI	NG PRESSI									
Half of base Middle Third of Base		I=L/2 tx=L/6			=	0.40 n 0.13 n							
Eccentricity of Base Re	eaction				=	0.13 n 0.18 n		Outside M					
CRITICAL EDGE PRE	SSURE	IN X-DIREC	TION					weed to C	neck Criti	cal Edge P	essure		
Length of Base in Con		Le=3*(I-ebx			=	0.65 n							
Critical Bearing Pres	sure	Qx=2*T/(B*	Le)		=	91.68 k	N/m2	Satisfactor	У	(0.92)			
CHECK PAD BASE R	EACTIO		RICITY AND BEARI	NG PRESSI	JRE IN Y-D								
		b=B/2			=	0.40 n							
Half of base		ty=B/6 eby=Mby/T			=	0.13 n 0.00 n		Within Mid	dle Third o	f Base			
	eaction	oby mby/1											
Half of base Middle Third of Base	eaction	oby mby r											
Half of base Middle Third of Base	eaction	Qy=qymax			=	37.51 k	N/m2	Satisfactor	у	(0.38)			

10 Trelawn, Lond	on E10 5QD	
PROJECT	•	•
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PROJECT No.	DATE	REV

0.21	m2
0.45	m
0.60	m



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ENG.	CHD.	CHD.
PP	кл	кл

# LOADS ACTING ON THE FOOTING (BELOW COLUMN C2)

	Load Posit	ioned	Element				
Load	from (m)	to (m)	Span/Height				
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m				
-	0.00	1.00	0.00 m				

# UDL LOADING UDL Dead Loading

Selfweight	24.00 kN/m3	х	0.10 m2	=	2.43 kN/m	х	1.00	=	2.43 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
				_	2.43 kN/m	-		-	2.43 kN/m
UDL Imposed Lo		х	0.00 m	=	0.00 kN/m	х	1.00	=	0.00 kN/m
UDL Imposed Lo	0.00 kN/m2 0.00 kN/m2	x x	0.00 m 0.00 m	=	0.00 kN/m 0.00 kN/m	X X	1.00 1.00	=	0.00 kN/m 0.00 kN/m
UDL Imposed Lo - -	0.00 kN/m2								
UDL Imposed Lo - - -	0.00 kN/m2 0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
UDL Imposed Lo - - - - -	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X	0.00 m 0.00 m	=	0.00 kN/m 0.00 kN/m	x x	1.00 1.00	=	0.00 kN/m 0.00 kN/m
UDL Imposed Lo - - - - -	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m	X X X	1.00 1.00 1.00	= =	0.00 kN/m 0.00 kN/m 0.00 kN/m
UDL Imposed Lo - - - - - -	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m 0.00 m	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m	x x x x	1.00 1.00 1.00 1.00	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m

Point Load	P1
E	_

From Bea DL IL	am = = =	64.46 kN	x́	+ 1.00 x B1( 1.00 = 1.00 =	LHS) + 1.00 x (MAX) 64.46 kN 17.67 kN	SUM:	82.13 kN
		17.07 KN	^	1.00 -	17.07 KN	00111.	02.10 KN
Point Lo	ad P2						
From Bea	am =	1.00 x (MAX	) + 1	.00 x (MAX)	+ 1.00 x (MAX)		
DL	=	0.00 kN	Х	1.00 =	0.00 kN		
IL	=	0.00 kN	Х	1.00 =	0.00 kN	SUM:	0.00 kN

## DESIGN FORCES

Ν	=	86.99 kN	1*B1. (RHS) +1*B1 (LHS)+UDL*Load Dispersion Length
<b>D</b> -		00.40 (N)	
			1*B1. (RHS) +1*B1 (LHS)+UDL*Pad Dimension
	=		
Fy	=	0.00 kN	
Mxx	=	0.00 kNm	
Муу	=	0.00 kNm	
ex	=	0.00 mm	
ey	=	0.00 mm	
	Pz Fx Fy Mxx Myy ex	Pz = Fx = Fy = Mxx = Myy = ex =	Pz = 82.13 kN Fx = 0.00 kN Fy = 0.00 kN Mxx = 0.00 kNm Myy = 0.00 kNm ex = 0.00 mm

Allowable Bearing Capacity of Soil

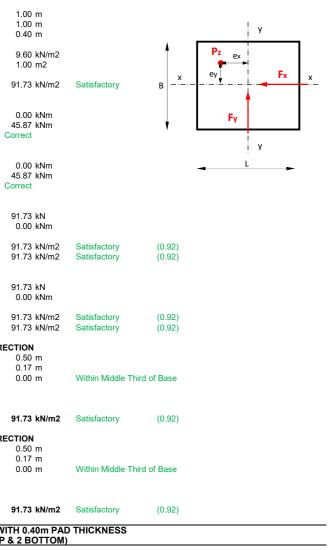
= 100.00 kN/m2

# goplans

STRIP FOOTING OPTIC		ble Bearing Capacity o	f Soil	=	0.87 r	~?						
		ble bearing Capacity o	1 301									
Minimum Footing Width Minimum Footing Depth	W D			=	0.45 r 1.00 r							
Plan Area Provided	W*(2*D)			=	0.90 r	n2						
Plan Area Required	< Plan Are	a Provided	Satisfactor	у	(0.97)							
BEARING CHECK BEL		2 PADSTONE @ GRO								-		
	Fotal ertical	Type of	Charact. Compr.	Local Strength	Bearing Length	Bearing Width	Stress Below	Padstone Length	Padstone Width	Ecc	Stress Below	Summary
	Load	Support	Strength	γb*fk/γm			Bearing	-			Padstone	
C2	From kN 118.52	Ex. Historia Briek	fk, N/mm2	N/mm2 1.25xfk/3.5 0.80	mm	mm	N/mm2	mm 700	 215	 0	N/mm2	Satisfactory
		Ex. Historic Brick	2.20	0.00	-	-	-	700	215	0	0.79	Salisfactory
	ovide MIN 700x(V STRIP	Vall Width)x300 Concre <b>FOOTINGS ARE S</b>	ATISFACT	ORY IF B								
		RED FROM BASEP ESS THAN 0.45m; F									NG	
PAD FOUNDATION OP	TION						_	_	_		_	
FOUNDATION DIMENS	IONS											
Length of Pad Footing	L			=	1.00 r							
Width of Pad Footing Depth of Pad Footing	B H			=	1.00 r 0.40 r						y	
				-	0.401				4			
Pad Foundation Selfweig Area of Pad Foundation	ght Sf A=L*B			= =	9.60 k 1.00 r				Ī	Pz ev	ex	Fx v
Bearing Pressure	(Pz+Sf)//	Ą		=	91.73 k	N/m2	Satisfactor	У	в	¥	<u>.</u>	<b>FX</b> X
CHECK STABILITY AG			ON								1 I	
Total Overturning Mome				=	0.00 k 45.87 k					F	y 🛛	
Total Restoring Moment Overturning Safety Factor		(L/2-ex)+Sf*A*L/2 x/Mox		=	45.87 F	unm			Y		y	
CHECK STABILITY AG			ON								! <b>'</b>	
Total Overturning Mome Total Restoring Moment		k+Fy*H (B/2-ey)+Sf*A*B/2		=	0.00 k 45.87 k					4	L	-
Overturning Safety Facto				=	Correct							
PAD FOUNDATION BA												
Total Pad Base Reaction			KES IN A-D	=	91.73 k	N						
Total Pad Base Moment	Mbx=My	y+Pz*ex+Fx*H		=	0.00	Nm						
Maximum Base Pressur	e axmax=T	/A+6*Mbx/(B*L*L)		=	91.73 k	N/m2	Satisfactor	v	(0.92)			
Minimum Base Pressure		/A-6*Mbx/(B*L*L)		=	91.73		Satisfactor	·	(0.92)			
PAD FOUNDATION BA	SE REACTIONS	AND BASE PRESSU	RES IN Y.D									
Total Pad Base Reaction				=	91.73 k	٨N						
Total Pad Base Moment	Mby=Mx	x+Pz*ey+Fy*H		=	0.00							
Maximum Base Pressur	e avmax=T	/A+6*Mby/(L*B*B)		=	91.73 k	N/m2	Satisfactor	v	(0.92)			
Minimum Base Pressure		/A-6*Mby/(L*B*B)		=	91.73		Satisfactor	·	(0.92)			
CHECK PAD BASE RE	ACTION ECCEN	ITRICITY AND BEARI	NG PRESSI	JRE IN X-D	IRECTION							
Half of base	I=L/2			=	0.50 r							
Middle Third of Base Eccentricity of Base Rea	tx=L/6 action ebx=Mbx	/T		=	0.17 r 0.00 r		Within Mid	dle Third o	fBase			
Eccentricity of Dase Nea				-	0.001				Dase			
Bearing Pressure	Qx=qxma	ax		=	91.73 I	kN/m2	Satisfactor	У	(0.92)			
CHECK PAD BASE RE	ACTION ECCEN	TRICITY AND BEARI	NG PRESSI	JRE IN Y-D	IRECTION							
Half of base	b=B/2			=	0.50 r							
Middle Third of Base Eccentricity of Base Rea	ty=B/6 action eby=Mby	//T		= =	0.17 r 0.00 r		Within Mid	dle Third o	f Base			
Bearing Pressure	Qy=qyma	ах		=	91.73 I	«N/m2	Satisfactor	У	(0.92)			
	Р	ROVIDE 1.00m x 1					THICKNE	SS				
					OP & 2 BO							

10 Trelawn, Lond	on E10 5QD	
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0.	87	m2
^	45	



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РР	кл	кл
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10 Trelawn, Lond	on E10 5QD	

# LOADS ACTING ON THE FOOTING (BELOW COLUMN C3)

	Load Posi	tioned	Element			
Load	from (m)	to (m)	Span/Height			
-	0.00	1.00	0.00 m	/	1.00	
-	0.00	1.00	0.00 m	/	1.00	-
-	0.00	1.00	0.00 m	/	1.00	=
-	0.00	1.00	0.00 m	/	1.00	=
-	0.00	1.00	0.00 m	/	1.00	=
-	0.00	1.00	0.00 m			
-	0.00	1.00	0.00 m			

# UDL LOADING UDL Dead Loading

Selfweight	24.00 kN/m3	х	0.10 m2	=	2.43 kN/m	х	1.00	=	2.43 kN/m
Ochweight	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-									
-	0.00 kN/m2	X	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
				_	2.43 kN/m	•		-	2.43 kN/m
UDL Imposed Lo	ading								
	0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
-		x x	0.00 m 0.00 m	=	0.00 kN/m 0.00 kN/m	x x	1.00 1.00	=	0.00 kN/m 0.00 kN/m
-	0.00 kN/m2								
- - -	0.00 kN/m2 0.00 kN/m2	Х	0.00 m	=	0.00 kN/m	Х	1.00	=	0.00 kN/m
- - -	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X	0.00 m 0.00 m	=	0.00 kN/m 0.00 kN/m	X X	1.00 1.00	=	0.00 kN/m 0.00 kN/m
	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m	X X X	1.00 1.00 1.00	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m
- · · · · · · · · · · · · · · · · · · ·	0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2 0.00 kN/m2	X X X	0.00 m 0.00 m 0.00 m 0.00 m	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m	x x x x	1.00 1.00 1.00 1.00	= = =	0.00 kN/m 0.00 kN/m 0.00 kN/m 0.00 kN/m

Point Load P1 From Beam = DL = IL =	1.00 x B1(RHS) + 1.00 x (MAX) + 1.00 x (MAX) 37.56 kN x 1.00 = 37.56 kN 10.67 kN x 1.00 = 10.67 kN	SUM:	48.22 kN
Point Load P2			
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)		
DL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$		
IL =	$0.00 \text{ kN} \times 1.00 = 0.00 \text{ kN}$	SUM:	0.00 kN

## DESIGN FORCES

STRIP FOOTING OPTION Vertical Force	Ν	=	51.14 kN	1*B1 (RHS)+UDL*Load Dispersion Length
PAD FOUNDATION OPTION				
Vertical Force	Pz	=	48.22 kN	1*B1 (RHS)+UDL*Pad Dimension
Horizontal Force in x direction	Fx	=	0.00 kN	
Horizontal Force in y direction	Fy	=	0.00 kN	
Major axis moment x-x	Mxx	=	0.00 kNm	
Major axis moment y-y	Муу	=	0.00 kNm	
Eccentricity x-x	ex	=	517.50 mm	
Eccentricity y-y	ey	=	0.00 mm	

Allowable Bearing Capacity of Soil

= 100.00 kN/m2

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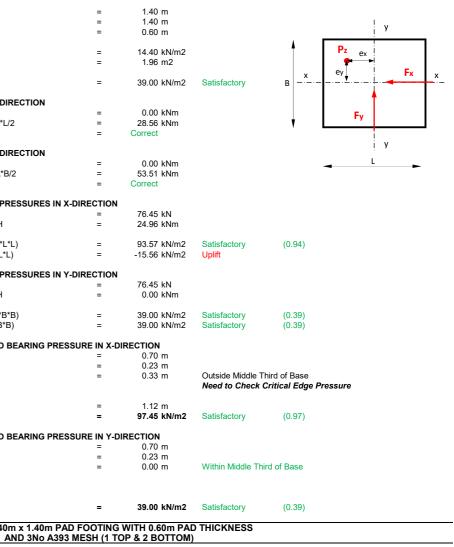
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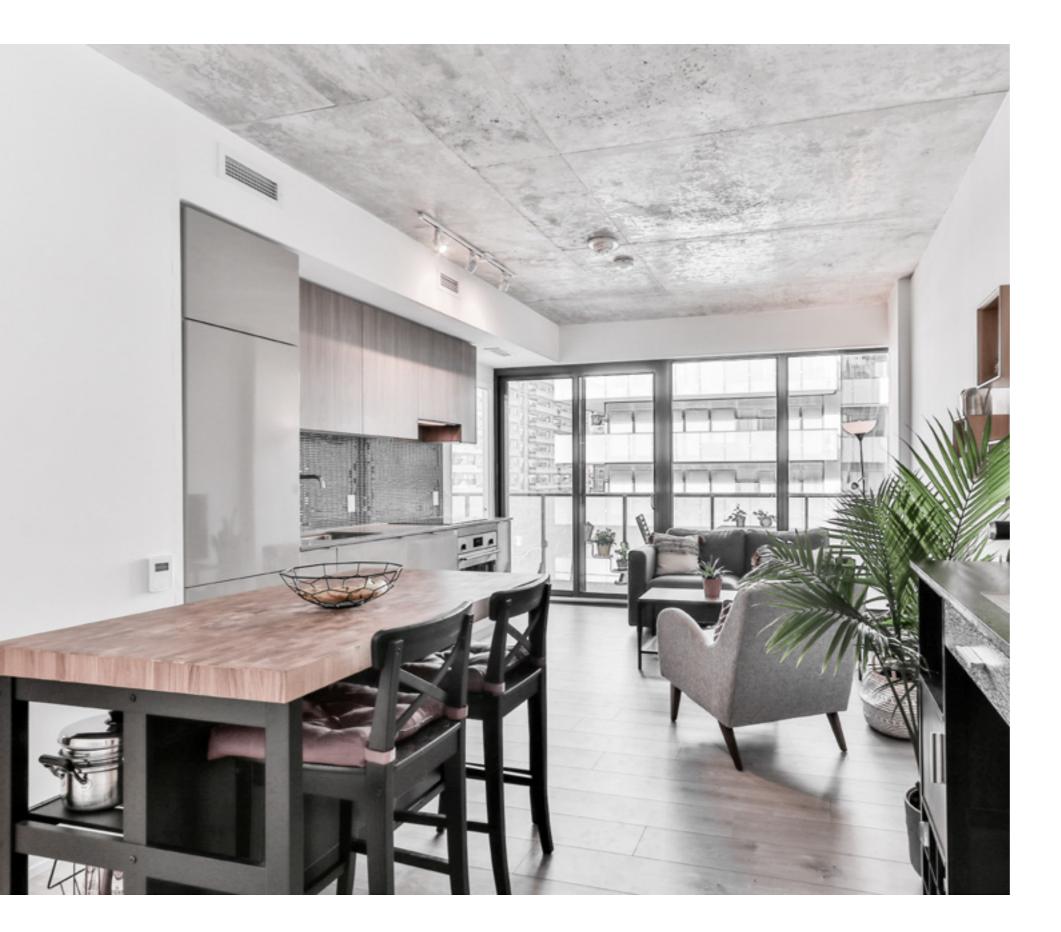
-same ressure		~1 ymax		-	55.00		Calibration	3	(0.00)				
Bearing Pressure		Qy=qymax		=	39.00	kN/m2	Satisfactor	v	(0.39)				
Eccentricity of Base	Reaction	eby=Mby/T		=	0.00	m	Within Mid	aie Third o	I Base				
Middle Third of Base		ty=B/6		=	0.23		10/04/2010 1 1 1	dia Thi 1	f Dec -				
Half of base		b=B/2		=	0.70	m							
CHECK PAD BASE	REACTIO	N ECCENTRICITY ANI			Y-DIRECTION								
Critical Bearing Pre		Qx=2*T/(B*Le)		=		kN/m2	Satisfactor	у	(0.97)				
Length of Base in Co		Le=3*(I-ebx)		=	1.12	m							
CRITICAL EDGE PR	FCCIDE						Need to C	heck Criti	cal Edge P	ressure			
Eccentricity of Base				=	0.33		Outside Mi						
Half of base Middle Third of Base	•	I=L/2 tx=L/6		=	0.70 0.23								
	REACTIO		D BEARING P										
VIII IIIIIIII DASE FIES	Suic	qymin=T/A-6*Mby/(L*E	, 0)	=	39.00	NIN/IIIZ	Jausidului	y	(0.39)				
Vaximum Base Pres Vinimum Base Pres		qymax=T/A+6*Mby/(L*		=		kN/m2 kN/m2	Satisfactor Satisfactor		(0.39)				
Fotal Pad Base Read Fotal Pad Base Morr		T=Pz+Sf*A Mby=Mxx+Pz*ey+Fy*h	ł	=	76.45 0.00	kN kNm							
			PRESSURES			LNI.							
Landin Dase i 163		4,41111 177-0 1000/(D1	)	-	-10.00		Obint						
Maximum Base Pres Minimum Base Press		qxmax=T/A+6*Mbx/(B qxmin=T/A-6*Mbx/(B*I		=		kN/m2 kN/m2	Satisfactor Uplift	у	(0.94)				
							0-11 (		(0.04)				
Total Pad Base Rea		Mbx=Myy+Pz*ex+Fx*H	1	=	24.96								
PAD FOUNDATION Total Pad Base Rea		ACTIONS AND BASE T=Pz+Sf*A	PRESSURES	IN X-DIRECT	ION 76.45	kN							
Total Restoring Mom Overturning Safety F		Mry=Pz*(B/2-ey)+Sf*A FOS=Mry/Moy	D/Z	=	53.51 Correct								
Total Overturning Mo		Moy=Mxx+Fy*H	*D/0	=		kNm				-	L	►	
		OVERTURNING IN Y-	DIRECTION										
Overturning Safety F	acior			=	Correct						i y		
Total Restoring Mom		Mrx=Pz*(L/2-ex)+Sf*A FOS=Mrx/Mox	*L/2	=	28.56				Y				
Total Overturning Mo	oment	Mox=Myy+Fx*H		=		kNm			Ţ	F	y		
CHECK STABILITY	AGAINST	OVERTURNING IN X-	DIRECTION								1		
Bearing Pressure		(Pz+Sf)/A		=	39.00	kN/m2	Satisfactor	у	в	-·-· <u>*</u> ·-	···		
niea ul Pad Foundat	uUII	A=L*B		=	1.96	1112			x	ey		Fx	x
Pad Foundation Self		Sf		=		kN/m2			T	Pz	ex		
				-						_	!		
Width of Pad Footing Depth of Pad Footing		В		=	1.40 0.60						y		
Length of Pad Footin		L		=	1.40								
FOUNDATION DIME													
PAD FOUNDATION	OPTION												
		MEASURED FROM									NG		
		STRIP FOOTINGS											
	Provide M	IN 440x(Wall Width)x21	15 Concrete Pa	adstone									
COLUMN C3 Pade													
	C3	69.64 Ex. Historic	Brick	2.25 0.8		-	-	440	215	0	0.74	Satisf	acto
	From	kN	fk,	N/mm2 N/mr 1.25xfk/		mm	N/mm2	mm	mm	mm	N/mm2		
	Load	Supp	ort St	rength γb*fk/	γm		Bearing	-			Padstone		
	Total Vertical	Туре	-	naract. Loca ompr. Stren		Bearing Width	Stress Below	Padstone Length	Padstone Width	Ecc	Stress Below	Sum	mar
BEARING CHECK E		DLUMN C3 PADSTON							1			-	
Plan Area Required	<	Plan Area Provided	Sat	tisfactory	(0.95)								
Plan Area Provided		W*(D)		=	0.54	m2							
						_							
Minimum Footing Wi Minimum Footing De		D		=	1.20								
	-141-	w		=	0.45								
ann a ca r toquirou		N/Allowable Bearing C	apacity of Soil	=	0.51	m2							
Plan Area Required													

PROJECT No.	DATE	REV
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10 Trelawn, London E10 5QD

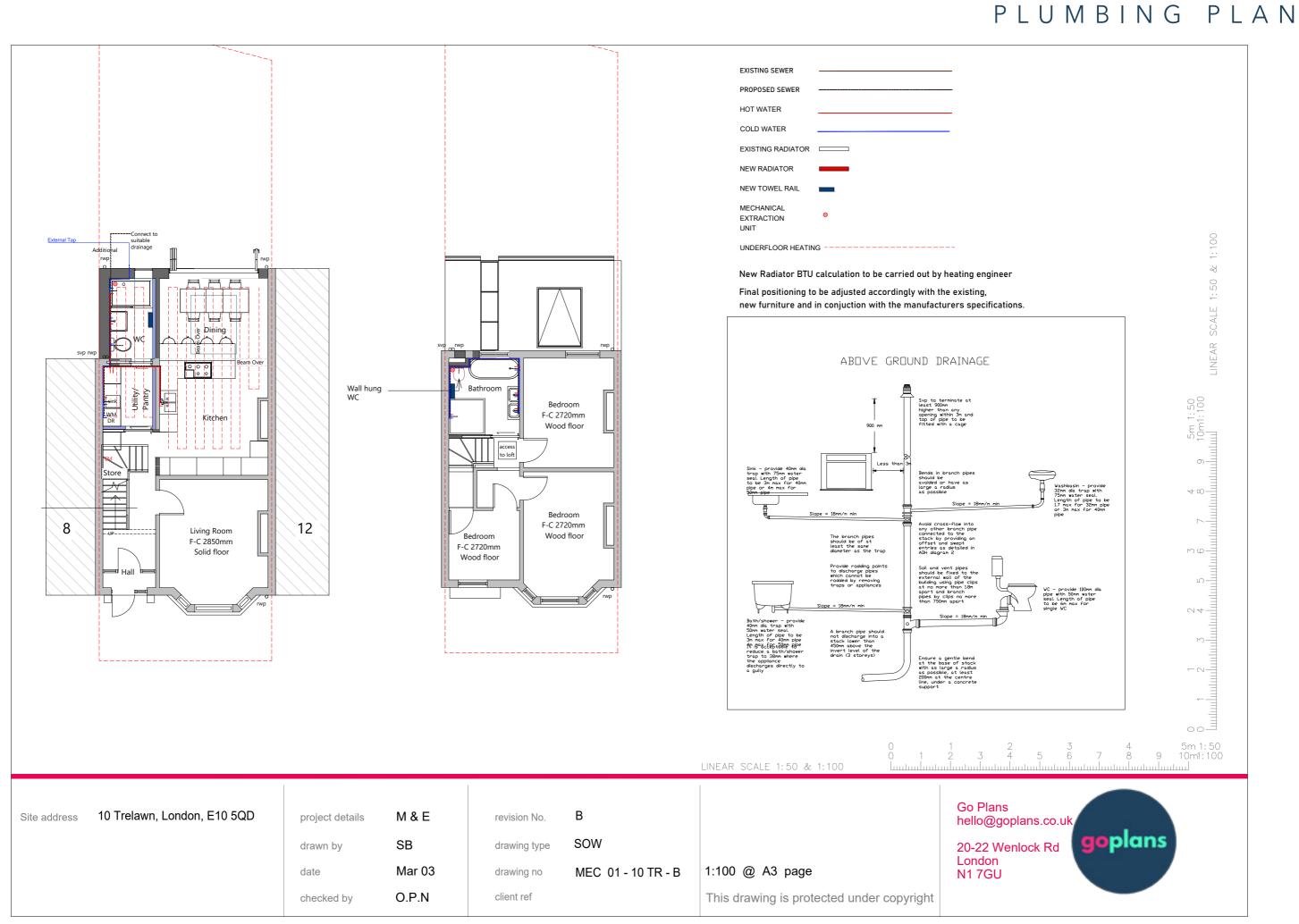


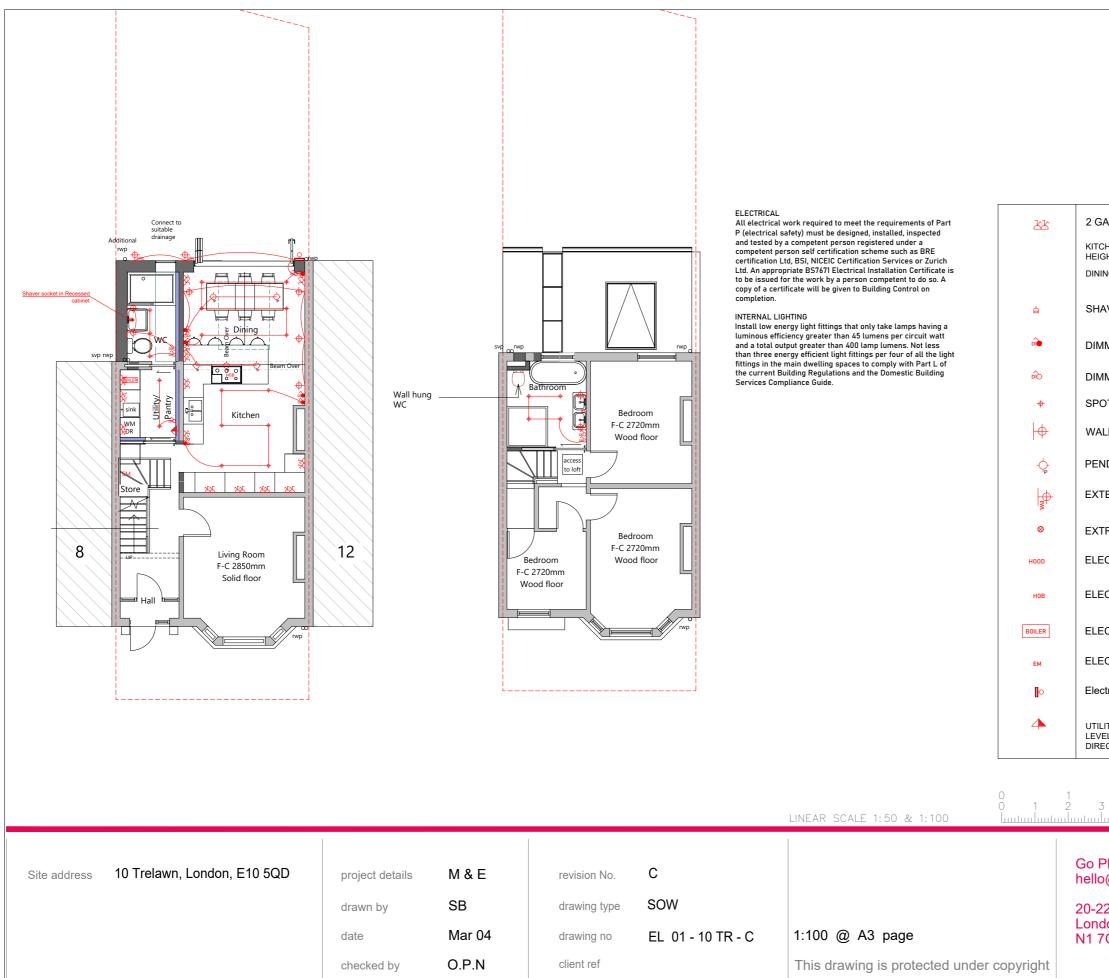






M&E PLANS



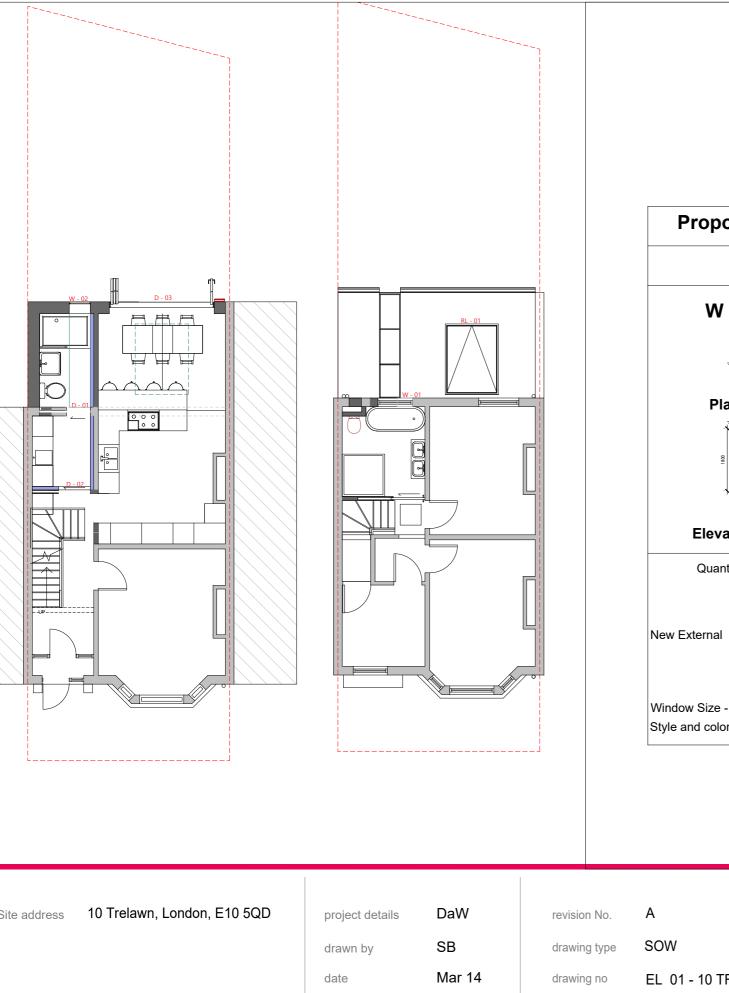


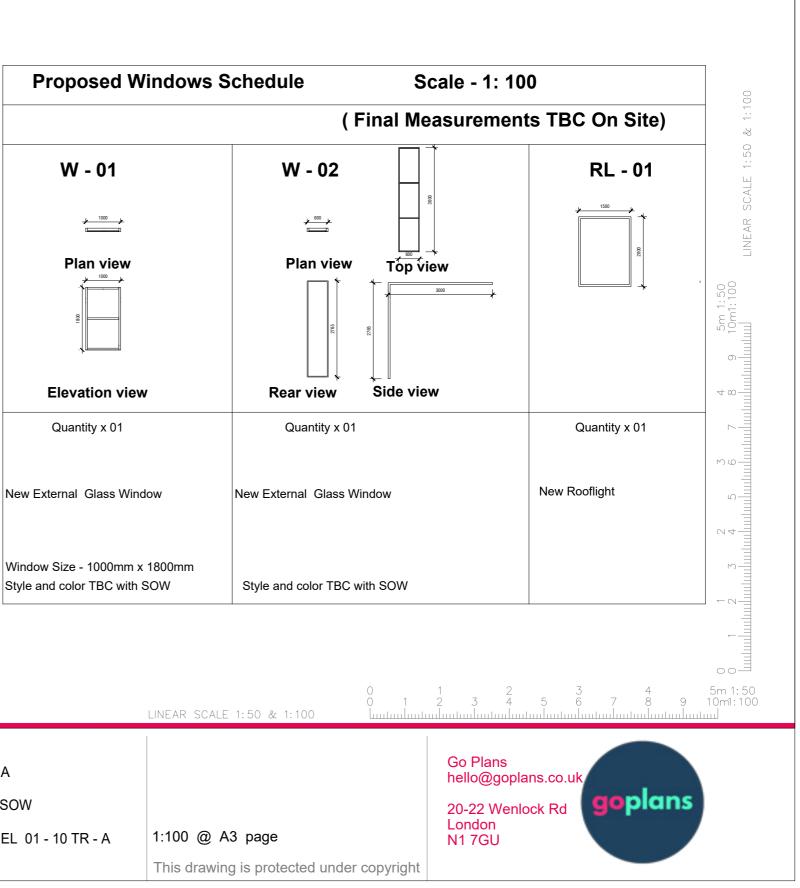
ELECTRICAL PLAN

ANG SWITCHED-SOCKET OUTLETS	0
CHEN - SOCKET/SWITCH IN WALL AT NORMAL GHT	1:100
NG - SOCKET/SWITCH IN WALL AT BENCH HEIGHT	1:50 &
AVER ONLY SOCKET	SCALE 1:
IMABLE MULTIPLE WAY SWITCH	LINEAR S
IMABLE 1 WAY SWITCH	
DTLIGHT	00
LL SCONCE LIGHT	5m 1:5 10m1:15
NDANT LIGHT	5 10 110
FERNAL WALL LIGHT	6
	4 00
IRACTOR FAN	7
ECTRIC HOOD	6
ECTRIC HOB	
	1
ECTRIC BOILER	4
ECTRIC METER	
ctrical Circuit Box - for future use. EWL above	
ITY - SOCKET/SWITCH IN WALL ABOVE SKIRTING EL. DIMMABLE 1 WAY SWITCH TO BE PLACED	
ECTLY ABOVE, AT NORMAL HEIGHT.	
	Ē.oo
2 3 4 3 4 5 6 7 8 9 Inntanlantanlantanlantanlantanlant	5m 1:50 10m1:100 hund
Plans o@goplans.co.uk 22 Wenlock Rd don 'GU	

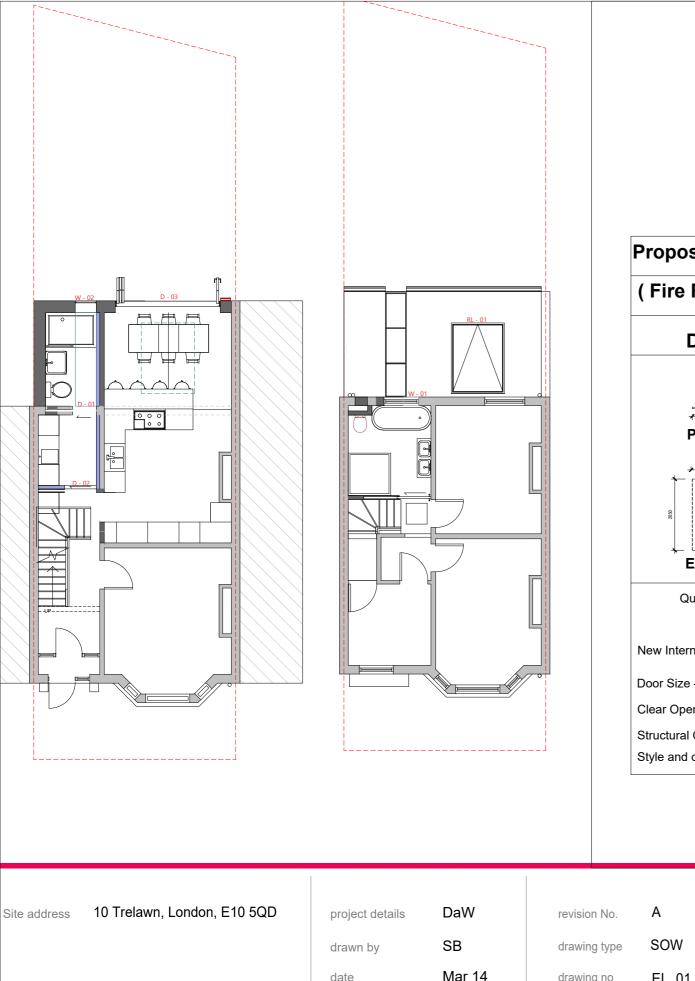


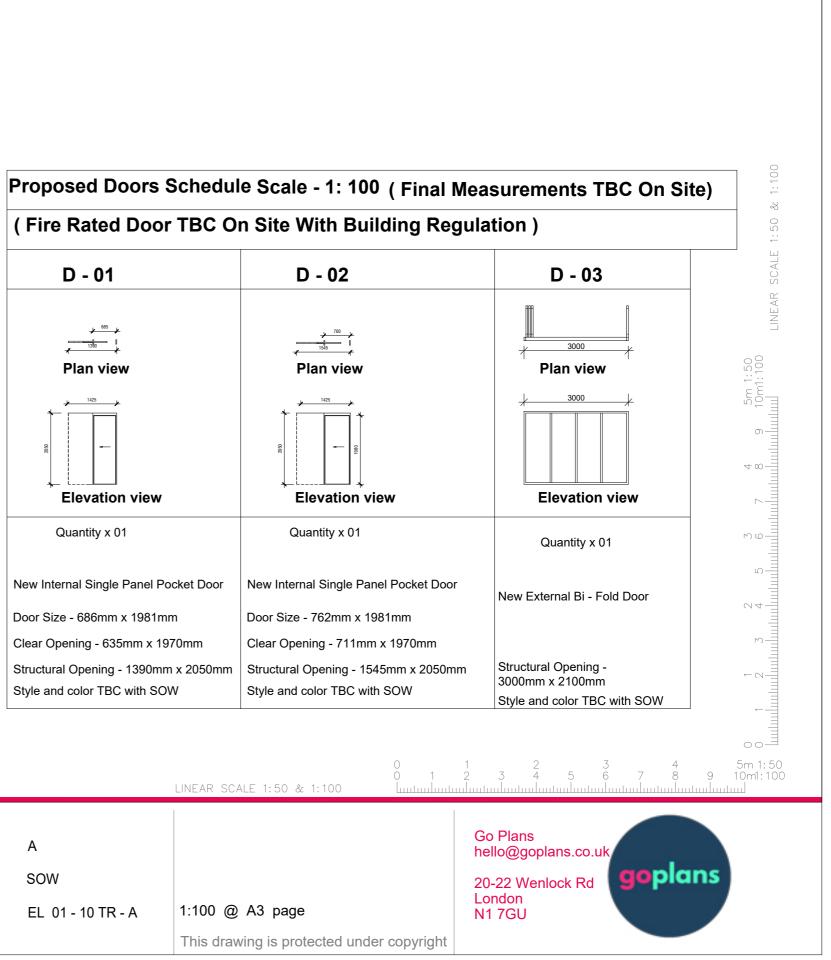






						0 LINEAR SCALE 1:50 & 1:100	
Site address	10 Trelawn, London, E10 5QD	project details drawn by date	DaW SB Mar 14	revision No. drawing type drawing no	A SOW EL 01 - 10 TR - A	1:100 @ A3 page	Go Pla hello@ 20-22 Londo N1 7G
		checked by	O.P.N	client ref		This drawing is protected under copyr	right









# FIXTURES, FITTINGS & FINISHES

## PROJECT ADDRESS

# GROUND FLOOR

GF Kitchen/Dining Room GF Utility Room GF Bathroom

# KITCHEN/DINING ROOM

PRODUCT	PRODUCT NAME	PRODUCT LINK	BUILDER SUPPLY?
	InfiniGlide6 Sliding Doors	https://www.finepoint.glass/aluminium-sliding-doors-london/#infiniglide-6	YES
	COR Vision Plus Sliding(alternative door option)	https://www.cortizo.com/en/sistemas/quenecesitas/grandes_dimensiones/93/cor-vi- sion-plus-sliding.html	YES
	Double Socket with USB-C Fast Charge	https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique- brass-white	NO
	Antique Brass triple dimmer switch	https://www.dowsingandreynolds.com/shop/antique-brass-triple-dimmer-switch/	NO
LIGHTING	LED downlights (white), task lighting (pendants) over kitchen peninsula & dining table and wall sconces		NO
HEATING	Underfloor Heating		N/A
	Victorian 1 MDF Skirting Board	https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/	YES
	Victorian 1 MDF Architrave	https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/	YES

## KITCHEN/DINING ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK
	Sandbank Engineered Wooden Floor (Plank Style)	https://www.tedtodd.co.uk/product/sandbank/
WALLS	Plasterboard & skimmed	
CEILING	Plasterboard & skimmed	
CABINETRY	No cabinets (we will source via family)	

BUILDER SUPPLY?
NO
YES
YES
N/A

# UTILITY ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
DOORS	Pocket Door		YES
	Regent Recessed Small Pull	https://www.corston.com/products/regent-recessed-small-pull-antique-brass	NO
	Double Socket with USB-C Fast Charge	https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique- brass-white	NO
	Antique Brass double dimmer switch	https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch/	NO
	Calla - 2 light Calacatta marble and aged brass wall light	https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass- wall-light	NO
LIGHTING	LED Downlights		YES
HEATING	Underfloor Heating		N/A
FLOORING	ТВС		

# UTILITY ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
	Victorian 1 MDF Skirting Board	https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/	YES
	Victorian 1 MDF Architrave	https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/	YES
FLOORING	Calacatta Amber Honed Marble	https://www.mandarinstone.com/product/calacatta-amber-honed-marble/	NO
WALLS	Plasterboard & skimmed		YES
CEILING	Plasterboard & skimmed		YES
CABINETRY	No cabinets		N/A

## BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY
DOORS	Pocket door with lock		YES
	Regent Recessed Small Pull	https://www.corston.com/products/regent-recessed-small-pull-antique-brass	NO
0	Regent Recessed Thumbturn	https://www.corston.com/products/regent-recessed-thumbturn-antique-brass	NO
M. M.	50mm Hook Lock	https://www.corston.com/products/50mm-hook-lock-antique-brass	NO
	Shaver Socket	https://www.corston.com/products/shaver-socket-antique-brass-white	NO
	Antique Brass double dimmer switch	https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch	NO
	Calla - 2 light Calacatta marble and aged brass wall light	https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass- wall-light	NO
LIGHTING	LED Downlights		YES

## BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
HEATING	Underfloor Heating		N/A
	Victorian 1 MDF Skirting Board	https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/	YES
	Victorian 1 MDF Architrave	https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/	YES
E be att	Arezzo Brushed Brass Concealed Individual Diverter + Ther- mostatic Control Valve with Handset + Wall Mounted Shower Head	https://www.victorianplumbing.co.uk/arezzo-brushed-brass-concealed-individual-di- verter-thermostatic-control-valve-with-handset-wall-mounted-shower-head	YES
	Arezzo Round Brushed Brass Wall Mounted (2TH) Basin Mixer Tap		YES
WALL HUNG WC	твс		YES
WALL HUNG VANITY	твс		YES
CEILING	Plasterboard & skimmed		YES

## BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
FLOORING	Calacatta Amber Honed Marble	https://www.mandarinstone.com/product/calacatta-amber-honed-marble/	NO
WALLS	Calacatta Amber Honed Marble	https://www.mandarinstone.com/product/calacatta-amber-honed-marble/	NO

#### ADDITIONAL INFORMATION

• The client is only proceeding with the ground floor works at this stage, please exclude the first floor bathroom renovation.

• Garden works: External Tap (plumbing) and Lights, along with electrical box for future landscaping lighting (these lights have not been incorporatred on M&E drawings).

#### SITE INFORMATION

PRE-CONSTRUCTION	
Can the contractor use site utilities (water/electric)?	YES
Builder to provide welfare facilities (inc. toilet)?	YES
Do you require a temporary kitchen setting up?	NO
Does the site require hoarding?	NO

EXTERNAL FINISHES	
Garden works?	YES
Make good around extension?	YES
Tarmac?	NO
Grass?	NO
Artificial grass?	NO

WALLS	
Brick finish?	YES
Render?	NO
Does the extension match?	YES

#### ROOFING

Pitched roof tile type?

Flat roof type?

#### FASCIA AND GUTTER

Would you like to match the existing fascia and If no, please specify desired finish

#### SKYLIGHTS

Does the project have skylights?

#### EXTERNAL DOORS

Which type of door would you like? Please spe

Would you prefer to supply the doors?

#### WINDOWS

Which type of windows would you like? Please

Would you prefer to supply the windows?

N/A
FELT

d guttering?	YES

YES

W&D PLANS
YES

e specify	W&D PLANS
	YES

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