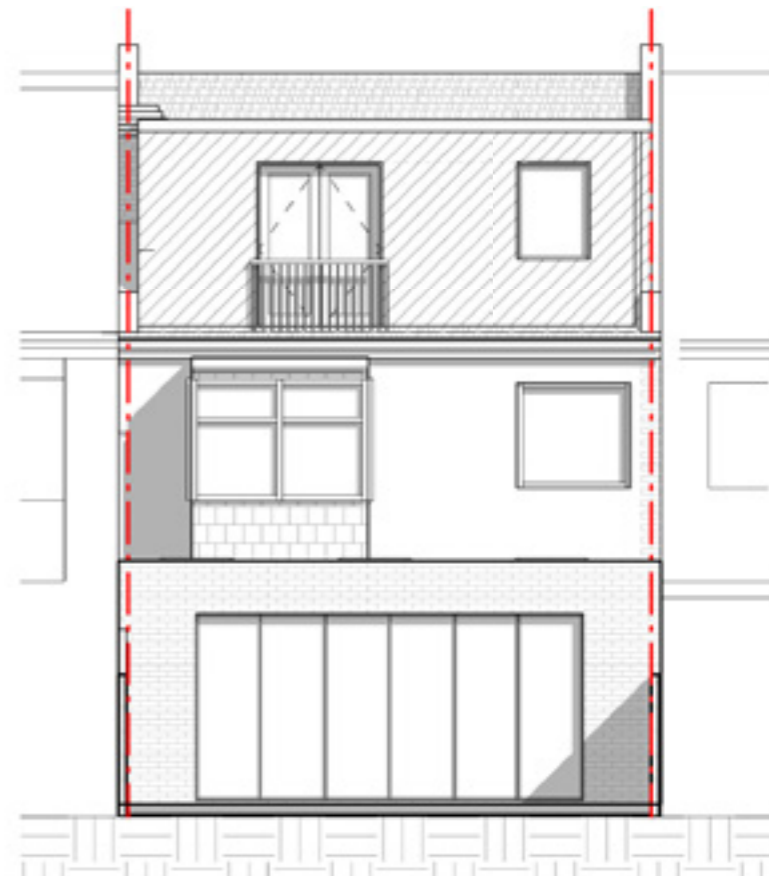


# gop plans

PROJECT ADDRESS



SCOPE OF WORK



# PROJECT INFORMATION



Company	<b>Go Plans</b>
Project Manager	<b>Oliver Newell</b>
Building Regulations	<b>Joe Mooney</b>
Structural Engineer	<b>Patrycja Perlińska</b>
Architectural Designer	<b>Ahmed Afzal</b>
Client	<b>Client Name</b>

## JOB DESCRIPTION

Single storey rear extension  
New kitchen, shower room & utility and all associated works

This package contains the scope of works and mechanical and electrical  
design documents required for construction pricing.  
For any further questions, please refer to Go Plans immediately.

## PLANNING PROPOSAL

Existing Plan

Proposed Plan

## BUILDING REGULATIONS

Building Regulations Drawing

## STRUCTURAL ENGINEERING

Structural Engineering Plan

## W & D PLANS

Window & Door Plan

## M & E PLANS

Plumbing Plan

Electrical Plan

## FIXTURES, FITTINGS & FINISHES

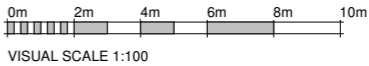
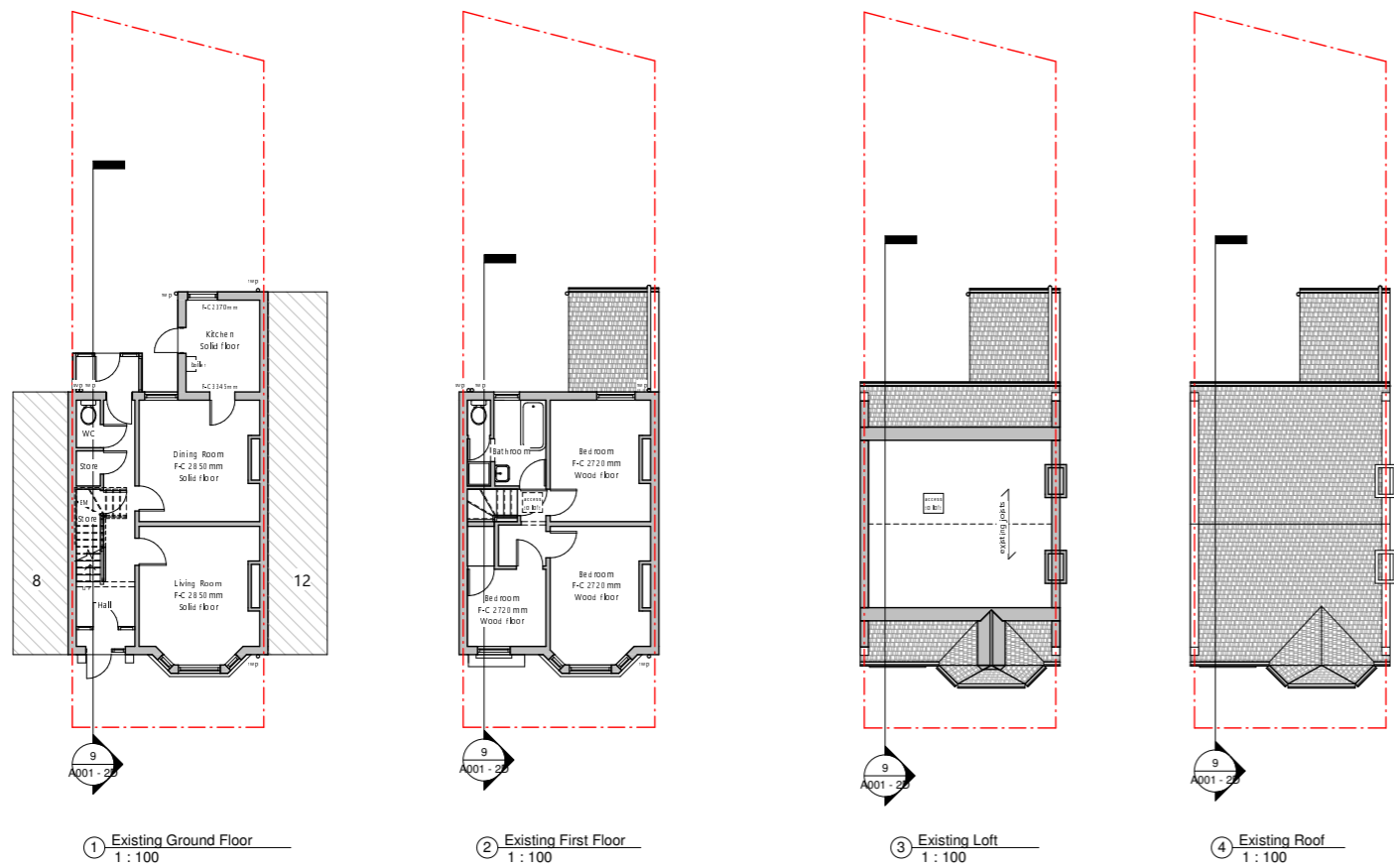
## SITE INFORMATION





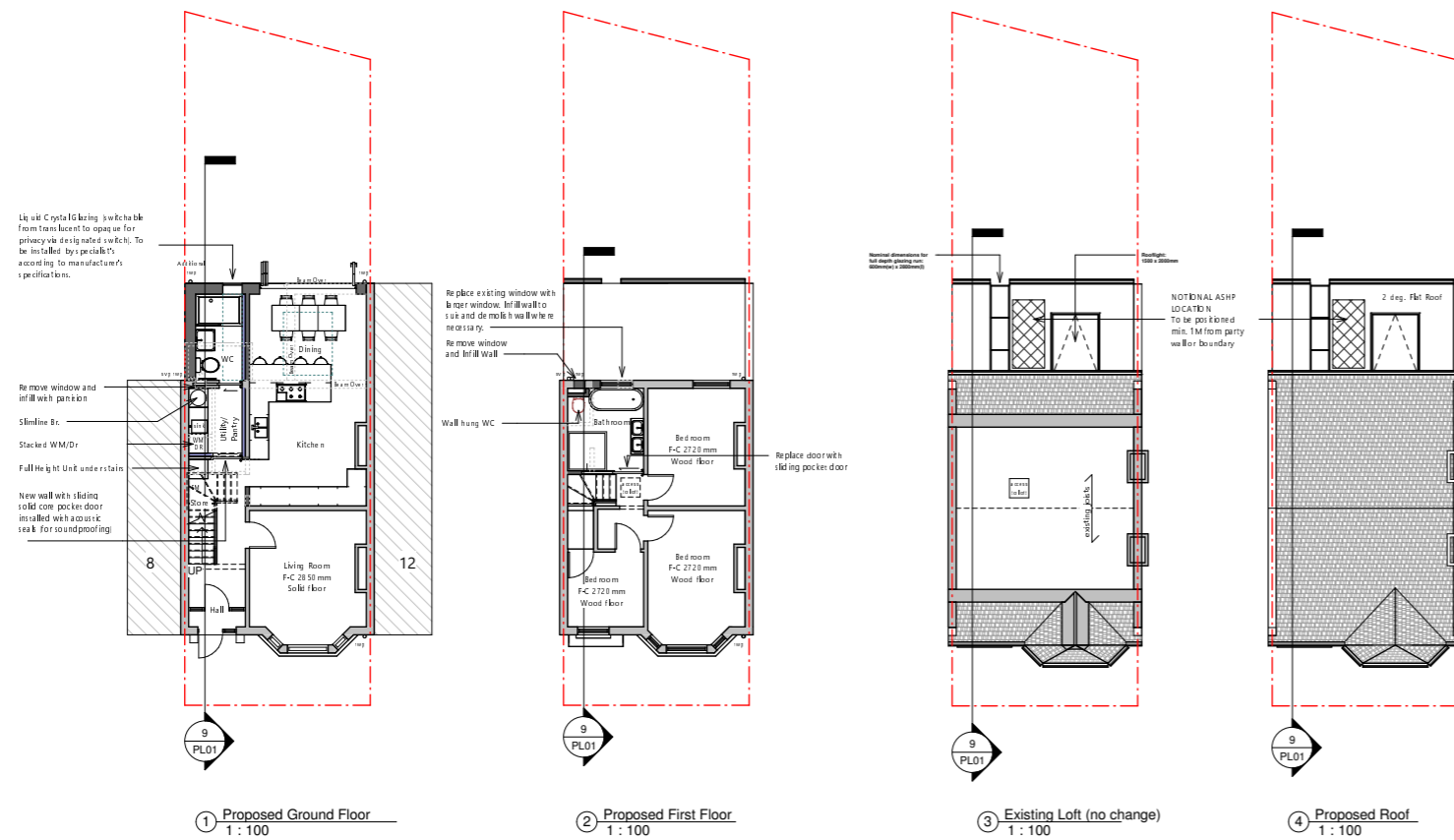
PROJECT ADDRESS

PLANNING PROPOSAL



PROJECT Rear Extension & Internal Reconfigurations			
ADDRESS 10 Trelawn Road, London E10 5QD			
CLIENT NAME D. Verrall			
PROJECT STATUS Project Status			
SHEET N. A001 - 2D	DRAWING TITLE Existing Drawings		
DESIGNED BY: Goplans	DRAWN BY: KC	CHECKED BY: Goplans	
DATE 05/11/2024	SCALE As Indicated @ A1		
<div>..... Detailed existing</div> <div>..... New above cut</div> <div>..... Headheight of 1.8m (estimated)</div> <div>..... Roof lights</div> <div>All dimensions to be cross checked on site prior to completing drawings for a party wall process, ordering and/or structural purposes</div>			
<div><div><div>goplans</div></div></div>			
<div><div>goplans.co.uk</div><div> </div><div>020 3633 0928</div></div>			

## PROPOSED PLAN



Rev.	Description:	Drawn by:	Date:
PL1	Externally lazing to GF bathroom incorporated. Previous proposed window removed. Bathroom reconfigured.	AA	22.01.25

PROJECT Single Storey Rear Extension and Internal Reconfiguration		
ADDRESS 10 Treleawn, London, E10 5QD		
CLIENT NAME D.Verrall		
PROJECT STATUS Planning		
SHEET N PL01	DRAWING TITLE Proposed Drawings	
DESIGNED BY Gopians	DRAWN BY AA	CHECKED BY Gopians
DATE 17/12/2024	SCALE As Indicated @ A1	

----- Demolished existing      Soundproofing  
 - - - - - Item above cut      - - - - - Units below  
 - - - - - Headheight of 1.8m (estimated)  
 Roof lights

All dimensions to be cross-checked on site prior to completing drawings for a party wall process, ordering and/or structural purposes

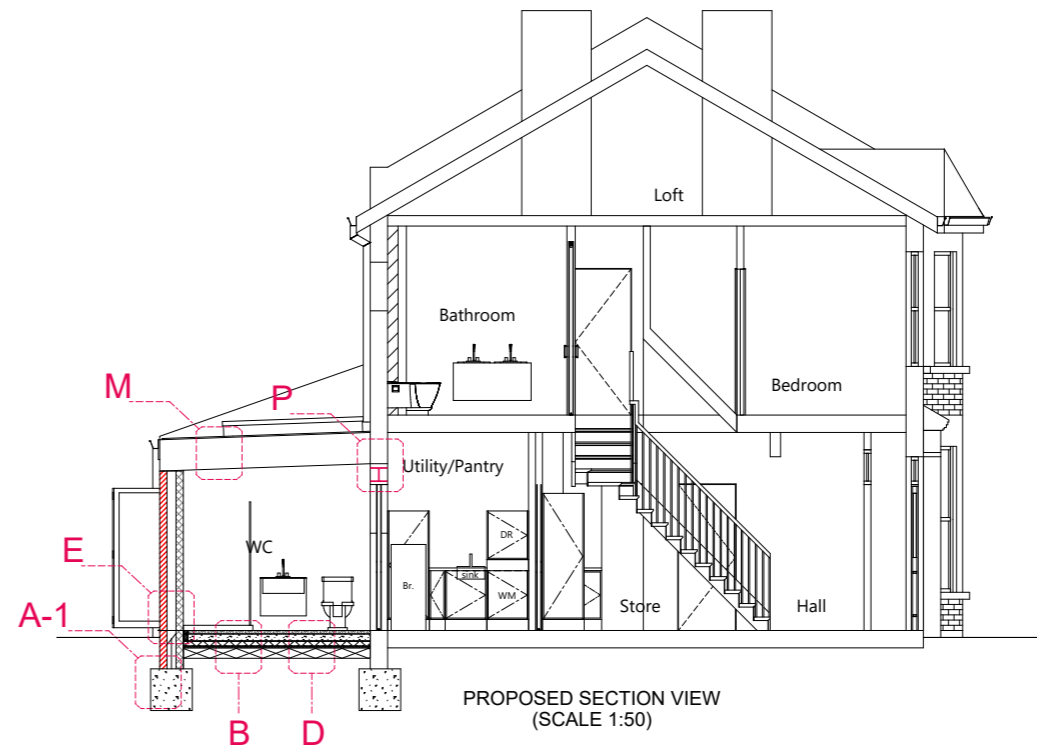
**goplans**

goplans.co.uk | 020 3633 0928

PROJECT ADDRESS

BUILDING REGULATIONS



[illegible]

- GENERAL NOTES
1. CHECK ALL DIMENSIONS ON SITE.
  2. ALL NOTES IN STRUCTURAL CALCULATIONS TO BE READ BEFORE ANY WORK DONE IN THE SITE. THIS IS MANDATORY.
  3. ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE STATED.
  4. ALL VERTICAL MEASUREMENTS ASSUME GROUND TO BE LEVEL UNLESS OTHERWISE STATED.
  5. THIS DRAWING SHOULD BE READ IN CONJUNCTION WITH THE GENERAL NOTES.
  6. WORKS TO BE CARRIED OUT WITH MATERIALS AND WORKMANSHIP IN COMPLIANCE WITH APPROVED DOCUMENT FOR REGULATION 7 (THE BUILDING REGULATIONS 2010).
  7. WORKS TO BE CARRIED OUT IN A SAFE MANNER IN ACCORDANCE WITH CDM REGULATIONS 2007.
  8. OPEN UP EXISTING STRUCTURE AS REQUIRED BY THE BUILDING INSPECTOR.
  9. THIRD PARTY SUPPLIER TO MEASURE ON SITE BEFORE MANUFACTURING.
  10. GENERAL CONTRACTOR TO VERIFY FEED CONDITIONS PRIOR TO COMMENCEMENT OF EACH PORTION OF THE WORK.
  11. ALL DIMENSIONS SHOULD BE NOTED PRIOR TO PROCEEDING ANY WORKS.
  12. UNLESS OTHERWISE INDICATED, PLAN DIMENSIONS ARE TO COLUMN GRID ON CENTERLINES, NOMINAL SURFACE OF MASONRY, FACE OF STUDIOS AND FACE OF CONCRETE.
  13. "FLOOR LINE" REFERS TO TOP OF CONCRETE SLABS. FINISH FLOORING IS INSTALLED ABOVE THE FLOOR LINE. FOR DERESSED FLOORS AND CURBS, SEE STRUCTURAL DRAWINGS.
  14. RELEVANT FEATURES ARE TO BE NOTED AND DRAWN IN THEIR ENTIRETY AND SHALL BE COMPLETELY PROVIDED AS DRAWN IN FULL. WHERE A DOOR IS LOCATED NEAR CORNER OF ROOM AND IS NOT LOCATED BY DIMENSION ON PLAN OR DETAILS, DIMENSION SHALL BE 100MM FROM FACE OF STUD WALL.
  15. LINE OF EXISTING FLOOR SLABS AS SHOWN ON THE BUILDING ELEVATIONS AND SECTIONS ARE APPROXIMATE.
  16. FLOOR LEVELS AND BOUNDARIES ASSUMED WHERE NOTED, DEPECTED BY LINE DASH LINES.
  17. REFER TO ARCHITECTURAL, STRUCTURAL, MECHANICAL, ELECTRICAL, GENERAL SPECIFICATION AND OTHER CATEGORIES OR DRAWINGS FOR ADDITIONAL NOTES.
  18. VERIFY RELOCATION/CONTAMINATION/INFESTING, ETC. AND PROVIDE COMPLETE REQUIRED OPENINGS THROUGH FLOORS AND WALLS, ACCESS DOORS, FLOORING, CURBS, ANCHORS IN STRUCTURE.
  19. CONTRACTOR TO CARRY OUT MOST LOGICAL SOLUTION BUT TO CHECK WITH ARCHITECT OR ENGINEER IF UNSURE, REQUESTING BY CLIENTS THAT OBTAIN FROM CLIENT THE DESIGN INTENT.
  20. SEE STRUCTURAL, GENERAL NOTES AND PLANS TO COMPLEMENT ARCHITECTURAL PLANS AT ALL TIMES. DO NOT ASSUME ANYTHING.

[illegible]

STEELWORK TO BE TEMPORARILY BRACED DURING CONSTRUCTION. A TEMPORARY WORKS DESIGN MAY BE REQUIRED.

- Protected fire route
- Insulation
- Brick work
- Block work

project details	As Per Planning
drawn by	J.W.M.
date	February 2025
checked by	K.E.S.

version	A
drawing type	Building Regulations
drawing no	BR 01 - 10 TR - A
client ref	-

0 1 2 3 4 5m

SCALE 1:100

1:100 1:50 @ A1 page

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Go Plans  
hello@goplans.co.uk

20-22 Wenlock Rd  
London  
N1 7GU







PROJECT ADDRESS

ENGINEERING PLANS



Project	10 Trelawn, London E10 5QD	
Subject	Structural Calculations	
Calc. No.	Rev	Date
K-25-02-80-C01	0	24.02.25

**Note to Contractor: PLEASE READ BEFORE COMMENCING ON SITE**

1. If you require any additional information before starting the works please email us.
2. Whilst carrying out the works, if you uncover any additional structural elements not noted within this calculation package please contact us as this may require a check and revised structural calculations
3. The contractor should carry out their own measured survey and investigations prior to starting works on site and ordering materials to confirm any critical assumptions noted in this document on page 3!
4. Please carefully read all notes on next two pages.
5. These calculations should be submitted for a full plans submission to building control prior to starting the works, a compliance report must be issued to the structural engineer prior to the works commencing on site. If you proceed with the works using a Building Notice, you are assuming the risk for the project and we will not accept responsibility or liability for any delays on site or associated costs or damages in connection with the delay or materials and labour cost associated with the re-design.

<div>IMPORTANT NOTES</div>		<div>goplans</div>		PROJECT No. K-25-02-80-C01	DATE 24.02.25	REV 0
				ENG. PP	CHD. KJ	CHD. KJ
				PROJECT 10 Trelawn, London E10 5QD		

General Notes

1. All works are to be in accordance with the current British Standard and Building Regulations.

2. This document to be read in conjunction with all relevant drawings issued by the Architect and specialist sub-contractors together with the specifications. Any discrepancies to be reported to Engineer.

3. Please note that the lengths of structural elements indicated in these calculations are not for fabrication purposes. The length of elements may differ slightly to allow for bearing, etc. The lengths of elements should always be based on onsite measurements. If the lengths of elements should differ from these calculations by more than 10%, please contact Engineer.

4. All setting out, levels, DPC, insulation, fire protection & waterproofing information is to be obtained from the Architect.

5. The Party Wall Act may apply.

6. Structural elements not shown in this document are out of scope and to be designed by others.

7. Balustrade and balustrade fixing details to be provided by manufacturer.

8. Off-the-shelf items to be installed as per manufacturer's details/recommendations.

9. All specified structural elements (i.e. steel beams & columns, timber beams&posts, etc.) are to be installed in a single continuous length unless stated otherwise.

10. No holes, chases, cut-outs, existing or proposed services or the like may be formed in or pass through any beam, column, or load bearing wall.

11. This document is intended to be printed in colour.

12. CALCULATIONS ARE SUBJECT TO BUILDING CONTROL APPROVAL. ANY WORKS CARRIED OUT PRIOR TO APPROVAL OF CALCULATIONS BY BUILDING CONTROL ARE AT OWN RISK. WE WILL NOT ACCEPT LIABILITY FOR ANY REQUIREMENTS, ALTERNATIONS, COSTS OR DELAYS RESULTING FROM THIS.

Construction Notes / Health & Safety Notes

1. We do not provide monitoring on site and the experience, diligence and management of the building contractor’s team must be relied on. The Contractor must provide permanent, experienced site managers capable of understanding the requirements of our specifications and design.

2. The Contractor shall ensure that stability of the building and adjacent premises is maintained at all stages of construction. The contractor is to design, install and maintain all necessary temporary works and programme the work accordingly.

3. In addition to the usual risks associated with building works and materials, of which competent builder should be aware, the following site and work specific health and safety risks have been identified: demolition, excavation, drilling and cutting into existing structure or materials should be carried out carefully in case there are any unknowns services hidden in the area.

4. The project requires the introduction of heavy structural elements such as steel beams or concrete lintels. Builder is to take into consideration the placement of all structural elements, ensuring that the method of lifting and placement is safely carried out. Responsibility for this element lies with the Contractor. As the existing walls need to be propped in order to introduce some of the lintels, this should also be considered in relationship to the risk assessment of the Contractor. Safe working procedures must be adopted. Responsibility for this element lies with the Contractor. Splice details for long-span beams can often be accommodated if required.

5. The design has been based on the assumption that the construction will be undertaken by a Competent Building Contractor used to undertaking this form of building works, of this type and complexity, and in accordance with Good Building Practice and general accepted standards and methods of construction.

Steelwork Notes

1. All steel beams / columns to be of steel grade min. S355. All plates to be of steel grade min. S275.

2. All bolts to be grade 8.8 unless noted otherwise.

3. All welds to be min 6mm fillet welds unless noted otherwise.

4. Steel elements end bearing to be equal to full width of any spreader or post / min. 100mm end bearing unless noted otherwise.

5. Corus “The Prevention of corrosion on structural steelwork” to be used as a guidance for steelwork finish/paint system.

6. Design of all connections is the responsibility of the steelwork sub-contractor unless noted otherwise.

7. Steel fabricator drawings to be submitted to engineer for checking before fabrication begins.

8. Padstones and steel beams to avoid clashes with chimney breast. Please contact Engineer if otherwise.

9. All padstones to be C35 grade.

10. As an alternative to padstones, 25mm thick steel spreader plates for padstones less than 440mm long can be used and 45mm thick steel spreader plates for padstones longer or equal than 440mm long but shorter than 700mm can be used. Steel plates plan dimensions to be the same as padstones plan dimensions.

11. Provide clearance to under-side of steelwork at intersecting wall locations where no bearing information is shown to prevent unintended load transfer.

12. Where pair of beams is presented, steel beams to be bolted together with M16 bolts @ spacer tubes @max 600mm centres.

13. Beams and columns to be placed centrally on bearings, ie beams/posts/padstones unless noted otherwise. Beams to be located centrally under walls, unless they are working as lintels on external cavity walls.

14. All steelwork below ground to have a minimum of 50mm concrete encasement unless noted otherwise.

15. All new columns to be tied to walls using shot fired wall ties or galvanized frame cramps at 450mm centres.

16. In places where beam is located parallel to padstone, beam must be centralized on the padstone. End bearing length of the beam to be equal to half padstone length. In places where beam is located perpendicular to padstone, end bearing length to be equal to padstone width. See drawings for details.

17. Site welding is not allowed unless noted otherwise.

18. Site modifications to structural steelwork shall not be carried out.

Timber Notes

1. All structural timber to be grade C24 unless noted otherwise.

2. All bolts to be grade 8.8 unless noted otherwise.

3. All timbers to be treated with an approved preservative to BS 5268 PT5

4. All cut ends to be retreated before fixing.

5. Timber elements end bearing length to be equal to full width of any spreader or post / min. 100mm end bearing unless noted otherwise.

6. All joist hangers are to be galvanised mild steel with minimum thickness of 2.5mm specified and designed by the specialist manufacturer. Timber joints between members are to be created using either traditional joinery techniques or proprietary fixings. Where input is required contact with engineer.

7. Floor and roof constructions, walls require lateral restraints by straps in accordance with the provisions in Building Regulation requirements.

8. Where two or more pieces of timber are specified in one element the timbers are to be fixed together to Building Control Officer approval.

9. New timber joists spanning more than 2.5m to be restrained by solid noggins in 1/3 of their length.

10. Provide clearance to under-side of timber joists at intersecting wall locations where no bearing information is shown to prevent unintended load transfer.

11. Double joists shall be provided under non-load bearing studwork partitions running parallel with joists spans, under baths and under airing cupboards.

12. Using notch for timber elements at support is not permitted. If it is required then contact engineer.

13. Timber post adjacent to existing masonry wall need to be resin anchored into the masonry using min M12 anchors @ max 450mm CTRS or angle brackets (if preferred).

14. Timber to timber/steel connections to be specified by others.

Masonry Notes

1. All proposed bricks to be standard format clay 20N/mm2 bricks unless noted otherwise.

2. All proposed blockwork to be 7.3N blocks unless noted otherwise.

3. Mortar below DPC to be designation M6 (ii), above designation M4 (iii).

4. Existing loadbearing masonry wall to be minimum 100mm thick wall.

5. 100mm wide blocks shall not be laid flat if load bearing.

6. Any disturbed and loose masonry should be removed and rebuilt.

7. Wall ties to be provided in accordance with the provisions in Building Regulation requirements.

8. Movement joints to be provided in accordance with masonry manufacturers recommendations.

Foundation Notes

1. For calculation purposes allowable bearing capacity of 100kN/m2 is assumed. Building Control Officer or other suitably qualified individual to ensure that formation level bearing stratum is valid.

2. Concrete to be grade C28/35, reinforcement to be high yield (fy = 500 N/mm2) unless noted otherwise.

3. All new foundations to be mass concrete strip footing - minimum width 0.6m, minimum depth 1.0m (final depth to building control officer) unless noted otherwise. These depths may need to be increased in order to transfer the loading onto satisfactory ground, or where there are trees nearby.

4. Minimum cover to reinforcement to be 50mm unless noted otherwise.

5. Existing foundations are assumed sufficient to carry the existing building.

6. Main contractor to check condition of existing walls and foundations prior to construction.

7. When additional load is added onto existing foundations , the existing foundations to be exposed and inspected by the Building Control Officer to checked/approved if adequate prior to commencement of works.

8. If soil is found to be shrinkable clays and trees are located nearby, foundations depth may need to be calculated in accordance with NHBC standard chapter 4.2. Spread foundations may not be suitable to use.

9. Pad footing to be placed centrally under columns/piers unless noted otherwise.

10. Pad footing near existing foundations should be at least equal in depth to existing foundation depth. Local underpinning may be required to prevent undermining if new pad footing proposed formation level is deeper than adjacent existing footing.

11. Footing near existing foundations should be at least equal in depth to existing foundation depth. Local underpinning may be required to prevent undermining if new footing proposed formation level is deeper than adjacent existing footing. New foundations to be excavated in 1.0m long bays; bays being excavated at the same time must not be adjacent to each other.

12. New foundations to be connected to existing foundations to Building Control Officer approval.

13. OBTAIN APPROVAL FROM LOCAL AUTHORITY BUILDING CONTROL BEFORE CASTING ANY FOUNDATIONS.

IMPORTANT NOTES

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PROJECT No.  
K-25-02-80-C01

DATE  
24.02.25

REV  
0

ENG.  
PP

CHD.  
KJ

CHD.  
KJ

PROJECT  
10 Trelawn, London E10 5QD

SYMBOL KEY

LOAD BEARING MASONRY WALL

LOAD BEARING STUD / DORMER WALL

APPROX LINE OF LOAD BEARING STUD / DORMER WALL OVER SHOWN DASHED

NON-LOADBEARING TIMBER PARTITION WALL SHEATHED IN PLYWOOD / OSB EITHER SIDE. WALL TO BE STRAPPED TO WALLS AND FLOORS. SEE SUMMARY PAGE FOR DETAILS.

OSB BOARDED JOISTS WITH ADDITIONAL LATERAL RESTRAINT BY STRAPS. SEE PLYBOARDING OF TIMBER JOISTS NOTE ON GENERAL ARRANGEMENT PAGE.

STEEL BEAM ON PLAN/ COLUMN ON SECTION / ELEVATION

STEEL UB / UC COLUMN ON PLAN / STEEL BEAM ON SECTION / ELEVATION

STEEL UB / UC COLUMN OVER SHOWN DASHED

STEEL SHS COLUMN

STEEL SHS COLUMN OVER SHOWN DASHED

TIMBER BEAM ON PLAN / TIMBER POST ON SECTION / ELEVATION

TIMBER POST / RAKING STRUT

APPROX BEARING OF TIMBER POST / RAKING STRUT OVER SHOWN DASHED

LINTEL

EXISTING BEAM / EXISTING LINTEL

EXISTING JOISTS SPAN DIRECTION UNLESS NOTED OTHERWISE

FLEXIBLE ENDPLATE CONNECTION. SEE DRAWING DETAILS

NEW RAFTERS SPAN DIRECTION

NEW FLAT ROOF JOISTS SPAN DIRECTION

NEW CEILING JOISTS SPAN DIRECTION

NEW FLOOR JOISTS SPAN DIRECTION

NEW GROUND FLOOR JOISTS SPAN DIRECTION

PADSTONE SHAPE

BEARING DETAIL NUMBER

1

1. WE DO NOT PROVIDE MONITORING ON SITE AND THE EXPERIENCE, DILIGENCE AND MANAGEMENT OF THE BUILDING CONTRACTOR'S TEAM MUST BE RELIED ON. THE CONTRACTOR MUST PROVIDE PERMANENT, EXPERIENCED SITE MANAGERS CAPABLE OF UNDERSTANDING THE REQUIREMENTS OF OUR SPECIFICATIONS AND DESIGN.

2. THE CONTRACTOR SHALL ENSURE THAT STABILITY OF THE BUILDING AND ADJACENT PREMISES IS MAINTAINED AT ALL STAGES OF CONSTRUCTION. THE CONTRACTOR IS TO DESIGN, INSTALL AND MAINTAIN ALL NECESSARY TEMPORARY WORKS AND PROGRAMME THE WORK ACCORDINGLY.

3. THE DESIGN HAS BEEN BASED ON THE ASSUMPTION THAT THE CONSTRUCTION WILL BE UNDERTAKEN BY A COMPETENT BUILDING CONTRACTOR USED TO UNDERTAKING THIS FORM OF BUILDING WORKS, OF THIS TYPE AND COMPLEXITY, AND IN ACCORDANCE WITH GOOD BUILDING PRACTICE AND GENERAL ACCEPTED STANDARDS AND METHODS OF CONSTRUCTION.

DESIGN APPROACH

BS 6399 P1/P2/P3

Loading for Building.  
Code of practice for dead and imposed loads.  
Code of practice for wind loads.  
Code of practice for imposed roof loads.

BS 8103 P3

Structural design of low-rise buildings.  
Code of practice for timber floors and roofs for housing.

BS 5950 P1

Structural use of steelwork in building.  
Code of practice for design – Rolled and welded sections

BS 8110 P1

Structural use of concrete.  
Code of practice for design and construction

BS 5628 P1

Code of practice for the use of masonry.  
Structural use of unreinforced masonry.

BS 5268 P2

Structural use of timber.

INPUT REQUIRED BY 3rd PARTIES / OTHER CONTRACTORS

- Liquid Crystal Glazing and trimmers design and specification

- Foundation design; verification of Presumed Allowable Bearing Pressure.

- Acceptability of ground bearing slab / foundations depth with local ground conditions.

- Steelwork connections (Steel fabricator drawings to be submitted to us for checking before fabrication begins).

- Timber connections to contractor (if any guidance required, please come back to us)

DESIGN ASSUMPTIONS

CRITICAL ASSUMPTIONS - THESE MUST BE CONFIRMED BY CONTRACTOR BEFORE COMMENCING THE WORK ON SITE AS DESIGN MAY NEED TO CHANGE:

1. Masonry load-bearing wall locations (hatched on general arrangement / steel beam bearing positions). Existing walls to be min. 100mm wide loadbearing masonry walls (and not 65mm "brick on edge" walls) with foundations underneath.

2. Existing floors above the ground floor are timber construction (with no concrete screed on top).

3. If ground is shrinkable clay and there are trees within 30m of the proposed development, then a tree survey to be forwarded to engineer, as foundations may need to be updated.

4. The existing ground floor is a ground-bearing slab.

5. Allowable bearing capacity of 100kN/m2. Building Control Officer or other suitably qualified individual to ensure that formation level bearing stratum is valid.

6. Air source heat pump total weight does not exceed 200kg.

CONSERVATIVE ASSUMPTIONS - THESE CAN BE CONFIRMED BY CONTRACTOR TO POTENTIALLY OPTIMISE DESIGN BUT ARE NOT CRUCIAL:

1. The existing masonry is assumed to be poor-quality brickwork/stonework for padstone design, where relevant.

2. The existing floor joists span direction is unknown (worst case assumed).

3. Existing walls marked below as W1 is 100mm wide masonry walls.

Bathroom

Bedroom F-C 2720mm Wood floor

Bedroom F-C 2720mm Wood floor

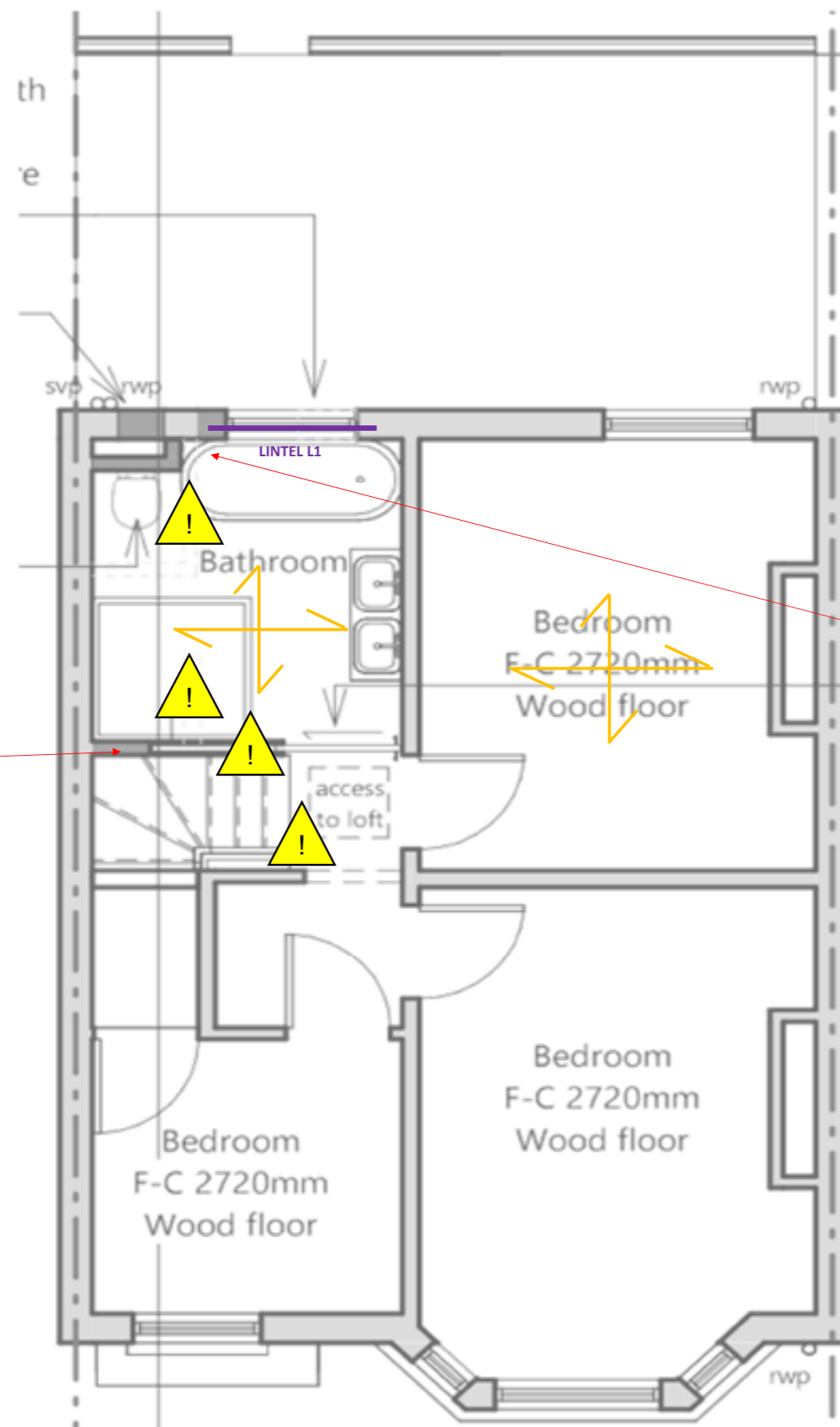
Bedroom F-C 2720mm Wood floor

W1

1st FLOOR PLAN

Page 3 / 34

13



WALL TO BE DEMOLISHED AND REBUILD AS  
TIMBER PARTITION WALL.

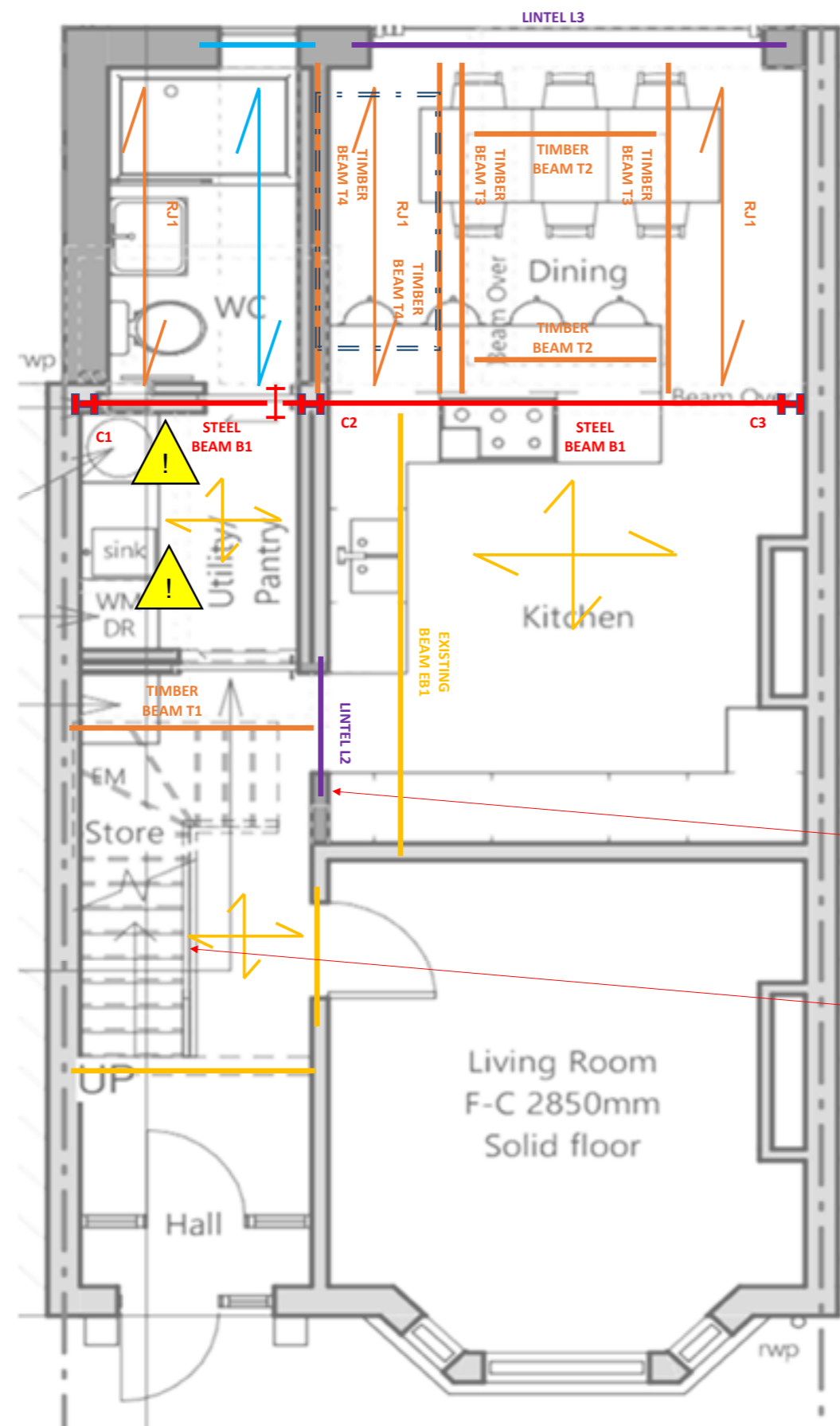
OPENING TO BE BRICKED UP WITH 20N/mm<sup>2</sup>  
BRICKWORK WITH MORTAR M4 (iii). NEW  
MASONRY TO BE KEYED INTO EXISTING  
MASONRY.

FOR ELEMENT SPECIFICATIONS REFER TO THE  
SUMMARY PAGE.  
FOR DESIGN ASSUMPTIONS  
REFER TO PAGE 3.

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10 Trelawn, London E10 5QD		

**1st FLOOR PLAN**  
**(SHOWING STRUCTURE ABOVE)**



**GROUND FLOOR PLAN  
(SHOWING STRUCTURE ABOVE)**

SYMBOL KEY

REMOVED WALL IS NON-LOADBEARING  
(TBC BY CONTRACTOR ON-SITE PRIOR TO REMOVAL)

AIR SOURCE HEAT PUMP ABOVE

LIQUID CRYSTAL GLAZING AND ITS TRIMMERS TO MANUFACTURER DESIGN AND SPECIFICATION

TIMBER BEAM T4 TO BE PROVIDED UNDER EACH LEG/SUPPORT LINE OF THE AIR SOURCE HEAT PUMP.

NO MASONRY WALL ABOVE TIMBER BEAM T1.

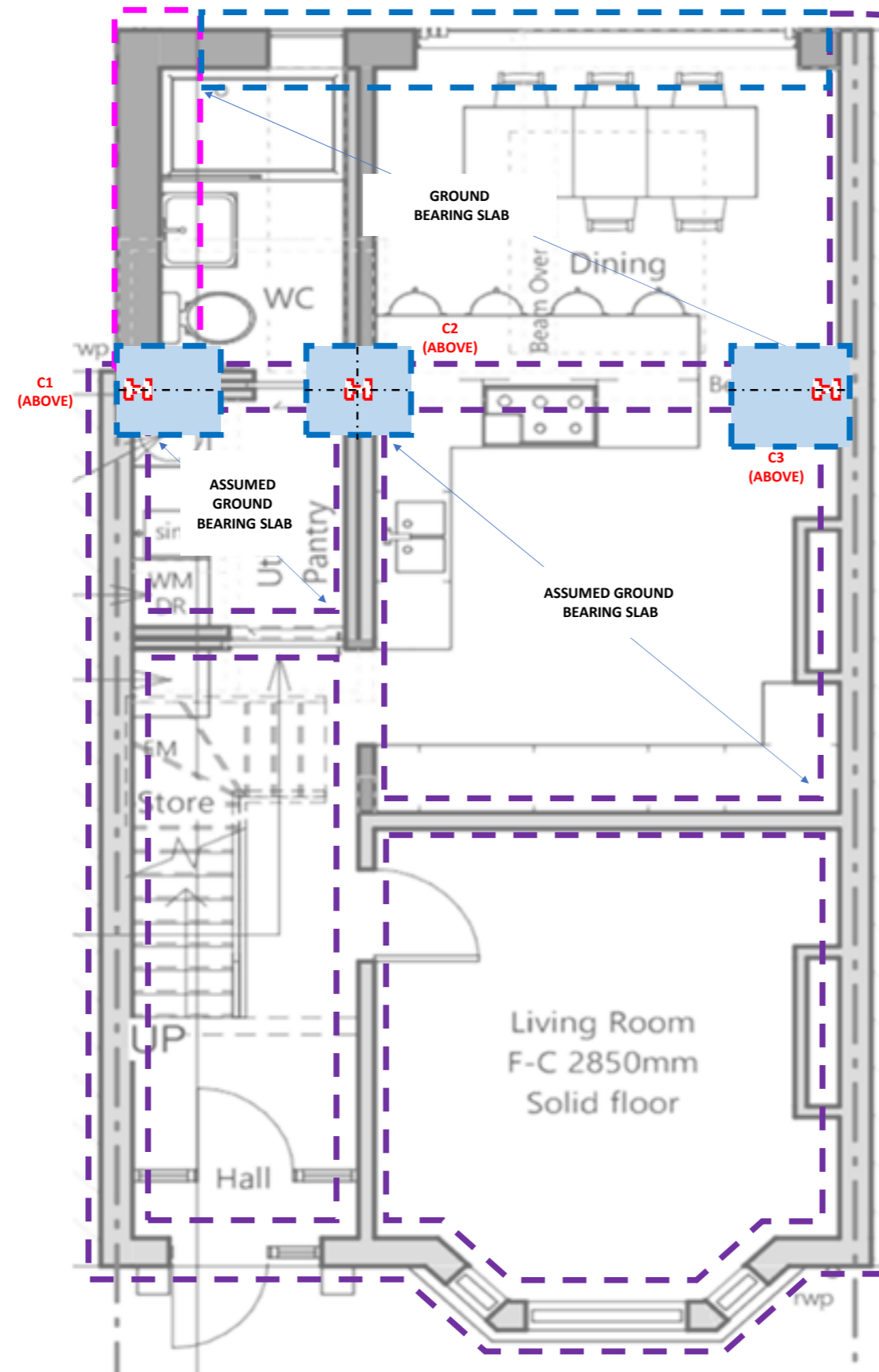
OPENING TO BE BLOCKED/BRICKED UP WITH 3.6N BLOCKWORK / 20N/mm2 BRICKWORK WITH MORTAR M4 (iii). NEW MASONRY TO BE KEYED INTO EXISTING MASONRY.

WALL BELOW STAIRS REMAIN UNCHANGED.

FOR ELEMENT SPECIFICATIONS REFER TO THE SUMMARY PAGE.  
FOR DESIGN ASSUMPTIONS REFER TO PAGE 3.





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**FOUNDATION PLAN**

**SYMBOL KEY**

-  EXISTING STRIP FOUNDATION (SEE TABLE FOUNDATIONS FOR DETAILS). IF FOUND TO BE DIFFERENT THAN STRIP/TRENCH COME BACK TO THE ENGINEER
-  PROPOSED CONCRETE TRENCH FILL FOUNDATION F1
-  PROPOSED ECCENTRIC CONCRETE TRENCH FILL FOUNDATION F2
-  PROPOSED PAD FOUNDATION (IF REQUIRED - SEE TABLE FOUNDATIONS FOR DETAILS)

**TREES IN SHRINKAGE CLAYS**

NO TREES/SHRINKABLE SOILS ARE ASSUMED (REFER TO THE ASSUMPTIONS ON PAGE 3)

**DRAIN**

PUBLIC SEWER AND DRAINAGE INFORMATION WAS NOT PROVIDED TO THE ENGINEER. IT IS ASSUMED THAT THERE IS NO PUBLIC SEWER IN CLOSE PROXIMITY TO OR CROSSING THE PROPOSED FOUNDATIONS.

FOR ELEMENT SPECIFICATIONS REFER TO THE SUMMARY PAGE.  
FOR DESIGN ASSUMPTIONS REFER TO PAGE 3.

**goplans**

PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

SUMMARY PAGE		IF EXISTING ELEMENT MATCHES SPECIFICATION OF NEW STRUCTURAL ELEMENT, RE-USE IS OK SUBJECT TO BUILDER CONFIRMATION / CHECKING QUALITY OF ELEMENT.		<div>goplans</div>		<table><tr><td>PROJECT No.</td><td>DATE</td><td>REV</td></tr><tr><td>K-25-02-80-C01</td><td>24.02.25</td><td>0</td></tr><tr><td>ENG.</td><td>CHD.</td><td>CHD.</td></tr><tr><td>PP</td><td>KJ</td><td>KJ</td></tr><tr><td colspan="3">PROJECT</td></tr><tr><td colspan="3">10 Trelawn, London E10 5QD</td></tr></table>		PROJECT No.	DATE	REV	K-25-02-80-C01	24.02.25	0	ENG.	CHD.	CHD.	PP	KJ	KJ	PROJECT			10 Trelawn, London E10 5QD		
PROJECT No.	DATE	REV																							
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PROJECT																									
10 Trelawn, London E10 5QD																									
<div>STEEL ELEMENTS</div> <p>B1 = 203 x 203 x 46 UKC (BEAM WITH PLATE, SEE DETAILS BELOW)</p> <p>C1 = 152 x 152 x 23 UKC (GROUND FLOOR TO 1st FLOOR LEVEL) (SATISFACTORY BY INSPECTION) C2 = 152 x 152 x 23 UKC (GROUND FLOOR TO 1st FLOOR LEVEL) C3 = 152 x 152 x 23 UKC (GROUND FLOOR TO 1st FLOOR LEVEL) (SATISFACTORY BY INSPECTION)</p> <p>STEELWORK GRADE: S355</p> <p>BEAMS WITH PLATE: - FOR BEAMS PLACED CENTRALLY UNDER 215mm THICK WALL / CAVITY WALL / CHIMNEY: PROVIDE 10mm THICK AND WALL WIDTH / CHIMNEY WIDTH PLATE 6mm FILLET WELDED TO TOP FLANGE OF BEAM.</p>		<div>TIMBER ELEMENTS</div> <p>RJ1 - FLAT ROOF JOIST = 150 x 50 C24 @ 400mm CTRS</p> <p>T1 = 3No 150x50 C24 T2 = 2No 150x50 C24 T3 = 2No 150x50 C24 T4 = 3No 150x50 C24</p> <p>WHERE TWO OR MORE PIECES OF TIMBER ARE SPECIFIED IN ONE ELEMENT THE TIMBERS TO BE FIXED TOGETHER TO BCO APPROVAL</p> <p>NON-LOADBEARING TIMBER PARTITION WALL (MARKED AS GREEN ON GENERAL ARRANGEMENT) TO BE 100x50 C24 @400mm C/C SHEATHED IN 9.5mm PLYWOOD / 9mm OSB EITHER SIDE. WALL TO BE STRAPPED TO WALLS AND FLOORS.</p> <div><p>OSB BOARDING OF TIMBER JOISTS - YELLOW SHADED AREA</p><p>ROOF JOISTS WITH 11mm OSB3 SHEATING REQUIRE LATERAL RESTRAINTS BY STRAPS IN ACCORDANCE WITH THE PROVISIONS IN BUILDING REGULATION REQUIREMENTS</p></div>		<div>WALLS</div> <p>ALL NEW EXTERNAL WALLS TO BE CAVITY MASONRY WALL CONSTRUCTION:</p> <p>- INNER SKIN TO BE CONSTRUCTED USING 3.6N BLOCKS WITH MORTAR M4 (iii).</p> <p>- OUTER SKIN TO BE CONSTRUCTED USING 20N/mm2 BRICKS WITH MORTAR M4 (iii).</p> <p>ALL NEW INTERNAL WALLS TO BE TIMBER PARTITION WALL CONSTRUCTION UNLESS NOTED OTHERWISE.</p>		<div>FOUNDATIONS</div> <p>ALLOWABLE BEARING CAPACITY OF 100kN/m2 ASSUMED.</p> <p>UNDER C1: - STRIP FOUNDATION: MIN DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL: 0.60m / MIN WIDTH: 0.45m / CONCRETE PADSTONE UNDER COLUMN: 300x(WALL WIDTH)x215mm OR - PAD FOUNDATION: 0.80mx0.80m MINIMUM 0.30m THICK WITH A393 MESH (TOP AND BOTTOM)</p> <p>UNDER C2: - STRIP FOUNDATION: MIN DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL: 1.00m / MIN WIDTH: 0.45m / CONCRETE PADSTONE UNDER COLUMN: 700x(WALL WIDTH)x300mm OR - PAD FOUNDATION: 1.00mx1.00m MINIMUM 0.40m THICK WITH A393 MESH (TOP AND 2 BOTTOM)</p> <p>UNDER C3: - STRIP FOUNDATION: MIN DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL: 1.20m / MIN WIDTH: 0.45m / CONCRETE PADSTONE UNDER COLUMN: 440x(WALL WIDTH)x215mm OR - PAD FOUNDATION: 1.40mx1.40m MINIMUM 0.60m THICK WITH A393 MESH (TOP AND 2 BOTTOM)</p> <p>PROPOSED CONCRETE TRENCH FILL FOUNDATION (F1): 600mm WIDE, MIN 600mm CONCRETE THICKNESS, MIN 1000mm DEPTH (SATISFACTORY BY INSPECTION)</p> <p>PROPOSED ECCENTRIC CONCRETE TRENCH FILL FOUNDATION (F2): 600mm WIDE, MIN 600mm CONCRETE THICKNESS, MIN 1000mm DEPTH (SATISFACTORY BY INSPECTION)</p> <p>PLEASE ALSO NOTE:</p> <p>- SEVERAL FOUNDATION OPTIONS ARE SHOWN FOR EACH ELEMENT. THE MOST SUITABLE OPTION TO BE CHOSEN ON THE SITE.</p> <p>- EXPOSE EXISTING FOUNDATIONS; IF THEY MEET THE SPECIFICATIONS, REUSE THEM WITH ON-SITE APPROVAL FROM THE BUILDING CONTROL INSPECTOR.</p> <p>- PAD FOUNDATION TO BE PLACED CENTRALLY UNDER COLUMN/PIER (EXCEPT FOR COLUMNS C1 AND C3). TO POUR PAD FOUNDATION, EXISTING FOUNDATIONS SHOULD BE REMOVED ENTIRELY IN PAD LOCATION.</p> <p>- DEPTH OF FOUNDATIONS TO BE MEASURED FROM GROUND LEVEL.</p> <p>- FINAL DEPTH TO BE AGREED WITH BUILDING CONTROL OFFICER ON SITE.</p>																			
<div>LINTELS</div> <p>L1 = CATNIC CN71A EXTERNAL SOLID WALL LINTEL L2 = 140x100 R6 HI-SPEC NAYLOR LINTEL OR SIMILAR L3 = CATNIC CG CAVITY WALL LINTEL</p>																									

GENERIC DETAILS

1. PLEASE READ WITH CONJUNCTION WITH PAGE 2 AND GENERAL ARRANGEMENT

2. ALL DETAILS AND DIMENSIONS ARE TO BE CHECKED/ADJUSTED TO SITE CONDITIONS BY THE CONTRACTOR/FABRICATOR PRIOR TO COMMENCEMENT OF CONSTRUCTION/FABRICATION. DO NOT SCALE THIS DRAWING.

3. STEEL FABRICATOR DRAWINGS TO BE SUBMITTED TO ENGINEER FOR CHECKING BEFORE FABRICATION BEGINS.

4. ALL DIMENSIONS IN mm UNLESS NOTED OTHERWISE

5. ALL STEEL BEAMS / COLUMNS TO BE OF STEEL GRADE MIN. S355. ALL PLATES TO BE OF STEEL GRADE MIN. S275

6. PLEASE NOTE THOSE ARE TYPICAL DETAILS, SEVERAL OPTIONS MAY BE SHOWN FOR EACH ELEMENT. THE MOST SUITABLE OPTION TO BE CHOSEN ON THE SITE

7. ALL EXPOSED STEELWORK OR STEELWORK IN CAVITIES TO BE GALVANISED

goplans

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24.02.25

REV  
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KJ

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KJ

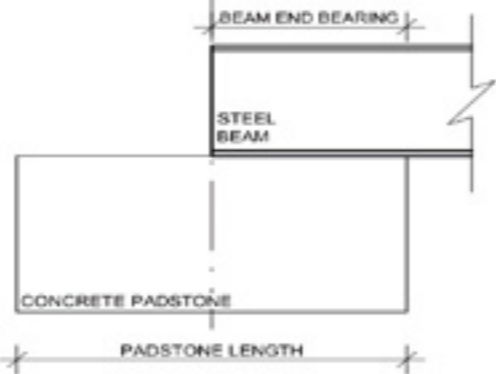
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10 Trelawn, London E10 5QD

PADSTONE DETAILS

IN PLACES WHERE BEAM IS LOCATED PARALLEL TO PADSTONE, BEAM MUST BE CENTRALIZED ON THE PADSTONE. END BEARING LENGTH OF THE BEAM TO BE EQUAL TO HALF PADSTONE LENGTH. IN PLACES WHERE BEAM IS LOCATED PERPENDICULAR TO PADSTONE, END BEARING LENGTH TO BE EQUAL TO PADSTONE WIDTH. SEE SKETCHES.

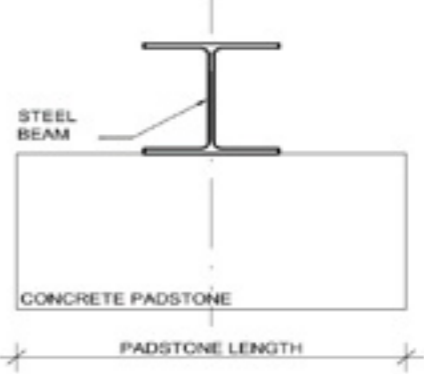
BEAM PARALLEL TO PADSTONE

BEAM END BEARING = HALF PADSTONE LENGTH



BEAM PERPENDICULAR TO PADSTONE

BEAM END BEARING = PADSTONE WIDTH



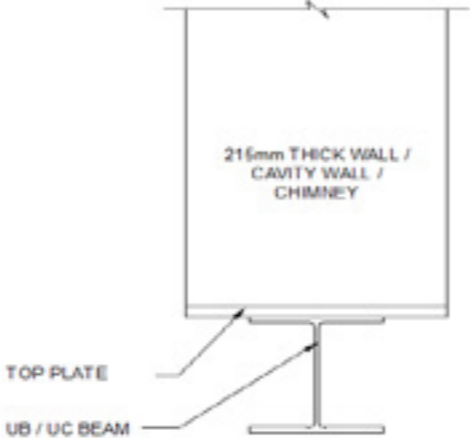
NOTE: SECTION INDICATIVE ONLY

PLATE DETAILS

BEAMS WITH PLATE:

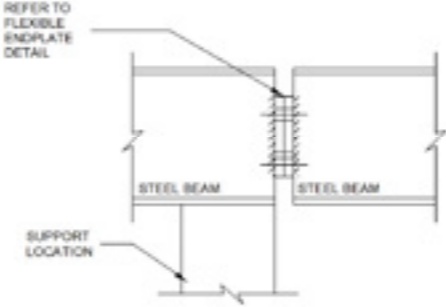
- FOR BEAMS PLACED CENTRALLY UNDER 215mm THICK WALL / CAVITY WALL / CHIMNEY: PROVIDE 10mm THICK AND WALL WIDTH / CHIMNEY WIDTH PLATE 6mm FILLET WELDED TO TOP FLANGE OF BEAM.

UB / UC STEEL BEAM WITH TOP PLATE  
DETAIL (FOR BEAMS PLACED  
CENTRALLY UNDER 215mm THICK WALL  
/ CAVITY WALL / CHIMNEY)



FLEXIBLE ENDPLATE CONNECTIONS  
(BEAM TO BEAM OVER SUPPORT)

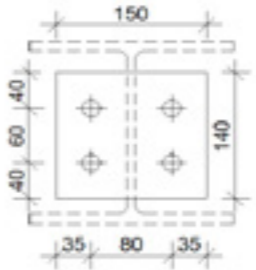
FLEXIBLE ENDPLATE CONNECTION DETAIL



SUITABLE FOR: B1 TO B1

203 UC BEAM FLEXIBLE  
ENDPLATE DETAIL

4No M16 8.8 BOLTS  
10mm THICK ENDPLATE (GRADE S275)  
WELDED TO 203 UC  
WITH 6mm FWFP



B1

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GENERIC  
DETAILS

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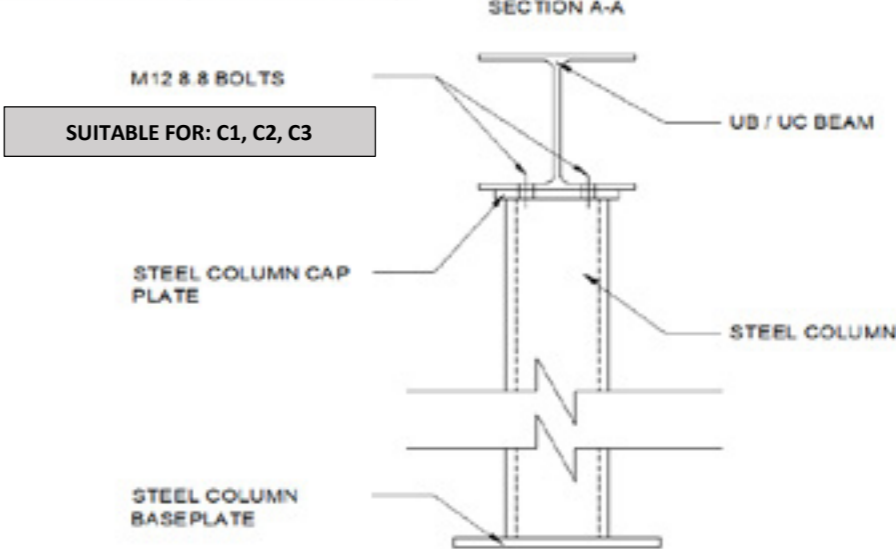
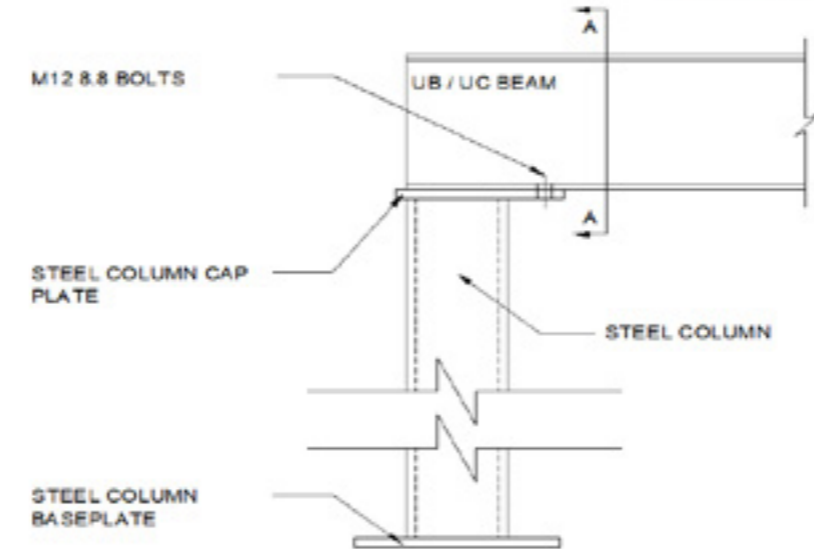
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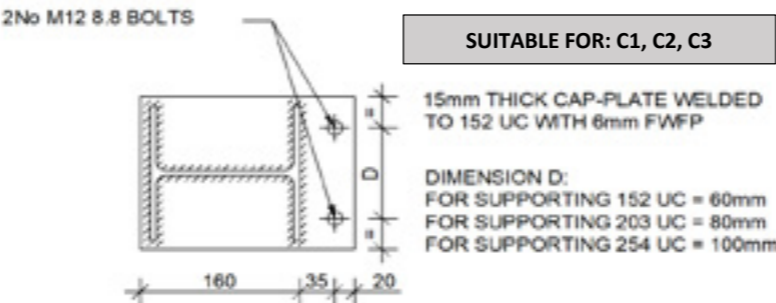
UB / UC COLUMNS CONNECTIONS

ALL NEW COLUMNS TO BE TIED TO WALLS  
USING SHOT FIRED WALL TIES OR  
GALVANIZED FRAME CRAMPS AT 450MM  
CENTRES.

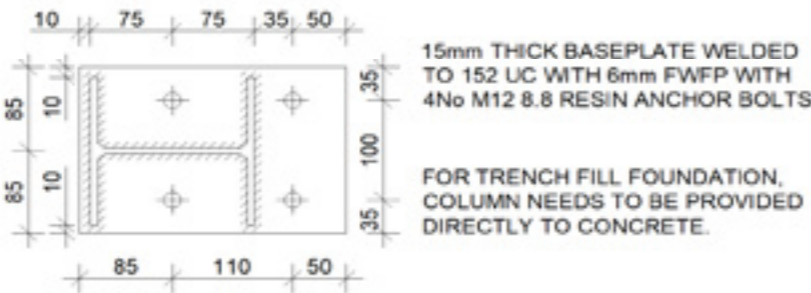
STEEL UB / UC BEAM SUPPORTED  
ON STEEL COLUMN (ELEVATION)



152 UC CAP PLATE DETAIL (SUPPORTING UC BEAM)

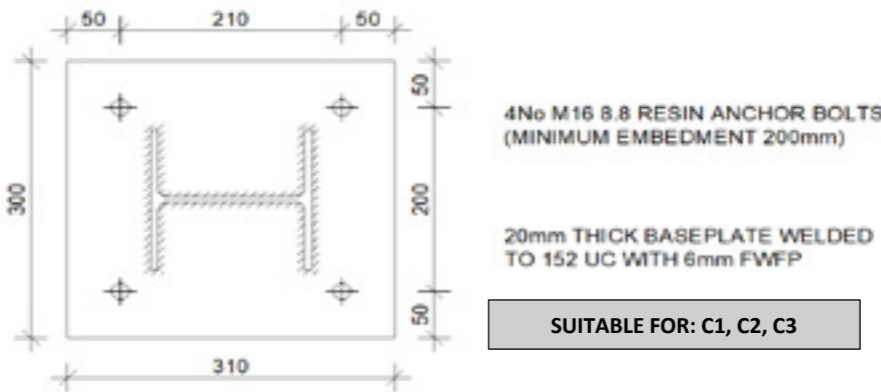


152 UC COLUMN BASEPLATE DETAIL  
(COLUMN SUPPORTED ON STRIP FOUNDATIONS OR  
TRENCH FILL FOUNDATIONS)



SUITABLE FOR: C1, C2, C3

152 UC COLUMN BASEPLATE DETAIL  
(COLUMN SUPPORTED ON PAD FOUNDATION)



SUITABLE FOR: C1, C2, C3

GENERIC  
DETAILS

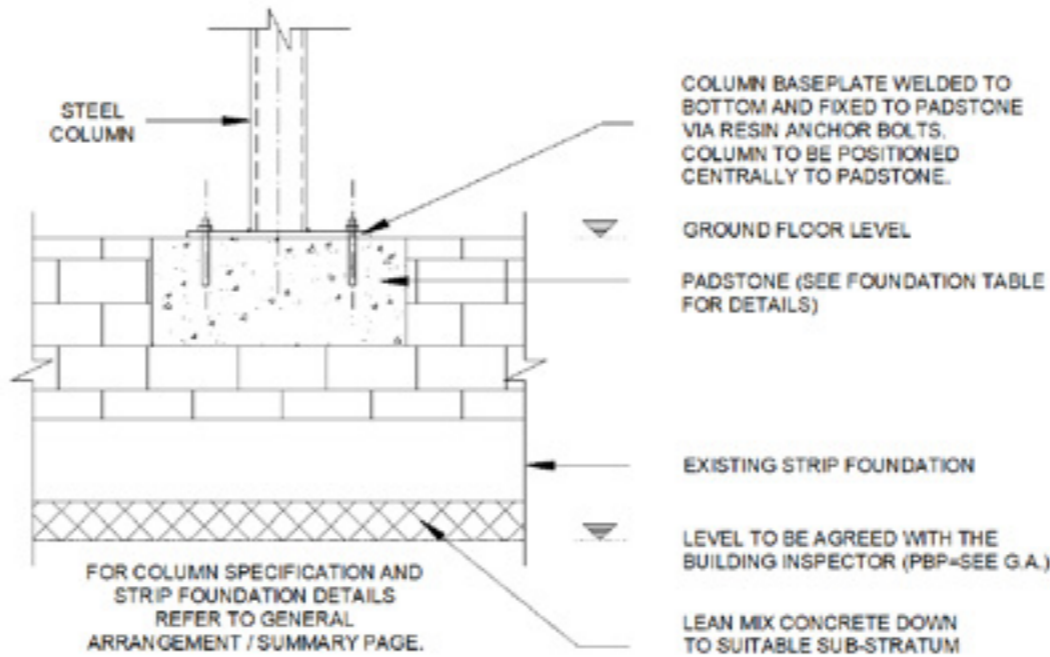
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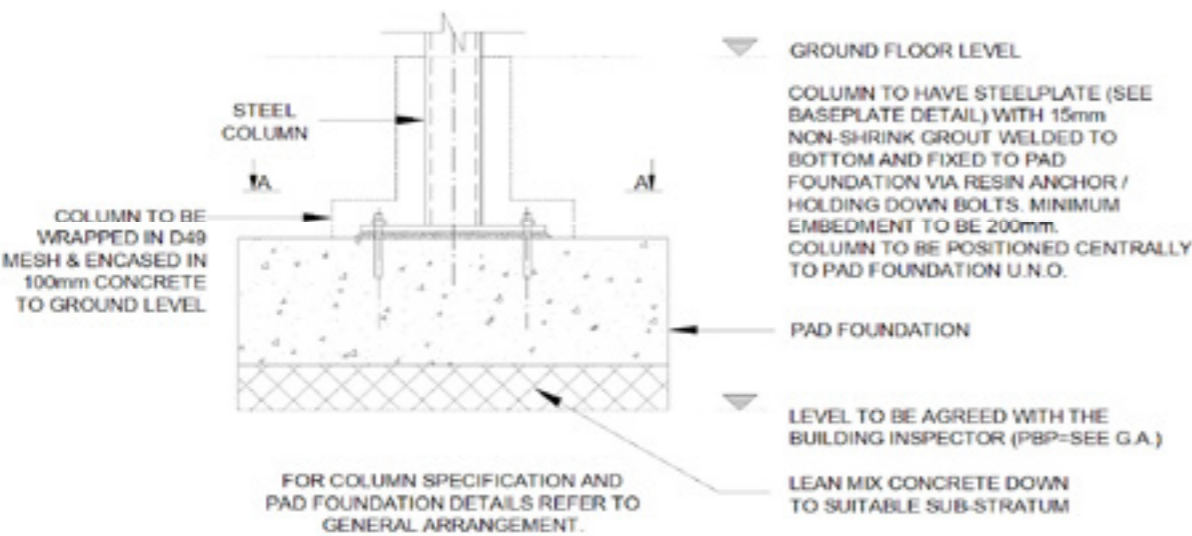
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FOUNDATIONS

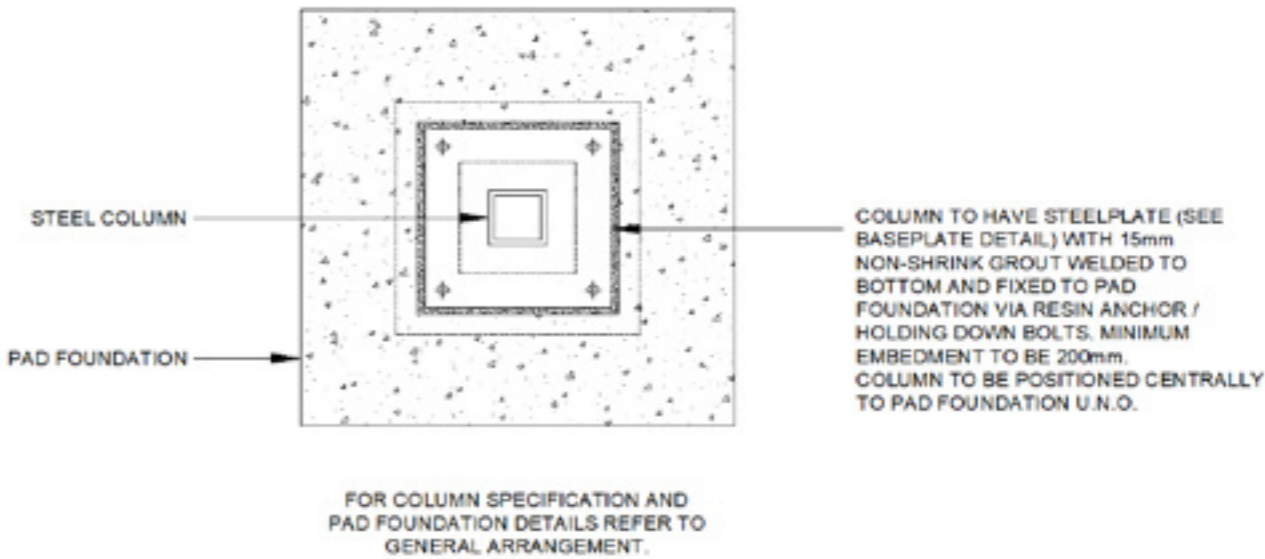
COLUMN SUPPORTED ON EXISTING STRIP FOUNDATION



COLUMN SUPPORTED ON NEW PAD FOUNDATION



COLUMN SUPPORTED ON NEW PAD FOUNDATION  
A-A ELEVATION





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LOAD SUMMARY

<b>Beam &amp; Block Floor</b>	
Finishes	0.20 kN/m2
75mm Screed	1.80 kN/m2
Insulation	0.10 kN/m2
150mm B&B Floor	2.20 kN/m2
<b>Total Dead load</b>	<b>4.30 kN/m2</b>
<b>Imposed load</b>	<b>1.50 kN/m2</b>
<b>Balcony</b>	
Finishes & Boarding	1.00 kN/m2
Insulation	0.10 kN/m2
Joists	0.10 kN/m2
Ceiling / Plasterboard	0.20 kN/m2
<b>Total Dead load</b>	<b>1.40 kN/m2</b>
<b>Imposed load</b>	<b>1.50 kN/m2</b>
<b>Timber Floor</b>	
Finishes & Boarding	0.20 kN/m2
Insulation	0.10 kN/m2
Joists	0.10 kN/m2
Ceiling / Plasterboard	0.20 kN/m2
Partition Walls	0.50 kN/m2
<b>Total Dead load</b>	<b>1.10 kN/m2</b>
<b>Imposed load</b>	<b>1.50 kN/m2</b>
<b>Ceiling</b>	
Finishes	0.05 kN/m2
Insulation	0.10 kN/m2
Joists	0.10 kN/m2
Ceiling / Plasterboard	0.20 kN/m2
<b>Total Dead load</b>	<b>0.45 kN/m2</b>
<b>Imposed load</b>	<b>0.25 kN/m2</b>
<b>Pitched Roof</b>	
Finishes / Tiles	0.50 kN/m2
Battens / Felt / Insulation	0.10 kN/m2
Structure	0.20 kN/m2
Ceiling / Plasterboard	0.20 kN/m2
<b>Total Dead load</b>	<b>1.00 kN/m2</b>
<b>Imposed load</b>	<b>0.75 kN/m2</b>
<b>Fiat Roof</b>	
Finishes	0.50 kN/m2
Felt / Insulation	0.10 kN/m2
Joists	0.20 kN/m2
Ceiling / Plasterboard	0.20 kN/m2
<b>Total Dead load</b>	<b>1.00 kN/m2</b>
<b>Imposed load</b>	<b>0.75 kN/m2</b>
<b>WALLS</b>	
Dormer Wall / External Timber Wall	1.00 kN/m2
Timber Partition Wall	0.35 kN/m2
Solid 215mm Masonry Wall / Cavity Wall	4.20 kN/m2
100mm Brickwork /Dense Blockwork Wall	2.10 kN/m2
100mm Lightweight Blockwork Wall	0.90 kN/m2
New Cavity Wall	4.20 kN/m2
<b>OTHERS</b>	
Bi-folds Doors	0.50 kN/m2
Glazing	0.50 kN/m2
Chimney	2.10 kN/m2
PV Panels	0.30 kN/m2
Balustrade	0.50 kN/m2

Site altitude Δs	=	13 m
Snow zone	=	B



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ALLOWABLE JOISTS SPAN DUE TO TRADA

<b>Flat Roof Joists</b>					
For Dead Load more than 0.75kN/m2 but not more than 1.00 kN/m2 ; For Imposed Load 0.75 kN/m2					
Section (RJ):	150 x 50 C24 @400mm c/c	Span	2.70 m	<=	Allowable Span
					3.11 m
					OK



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**TIMBER BEAM T1**  
Beam Span L = 1.75 m

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
Timber floor (1st)	0.00	1.75	5.50 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m
-	0.00	1.75	0.00 m

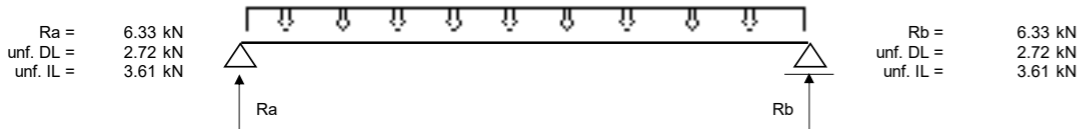
/ 2.00 = 2.75 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m

<b>UDL LOADING</b>									
<b>UDL Dead Loading</b>									
Beam Self Weight									
Timber floor (1st)	1.10 kN/m2	x	2.75 m	=	0.08 kN/m	x	1.00	=	0.08 kN/m
-	0.00 kN/m2	x	0.00 m	=	3.03 kN/m	x	1.00	=	3.03 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					3.11 kN/m				
					3.11 kN/m				

<b>UDL Imposed Loading</b>									
Timber floor (1st)	1.50 kN/m2	x	2.75 m	=	4.13 kN/m	x	1.00	=	4.13 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					4.13 kN/m				
					4.13 kN/m				

Point Load P1 @	0.00 m	Point Load P2 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN	DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN	IL =	0.00 kN x 1.00 = 0.00 kN

Point Load P3 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN



<b>FORCES IN BEAM</b>		<b>DEFLECTION CRITERIA</b>		<b>USAGE OF TIMBER BEAM T1</b>	
Moment =	2.77 kNm	0.003L / 14mm		Compression perpendicular to grain	18.16 %
Shear Force =	6.33 kN			Shear parallel to grain	63.49 %
Axial Force =	0.00 kN	<b>DURATION OF LOADING</b>		Bending parallel to grain	66.96 %
		Long-term		Vertical deflection	63.76 %

TIMBER BEAM T1 = 3No 150x50mm C24

BEARING CHECK

Beam No	Total Vertical Load From kN	Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
T1 (LHS):	T1 9.58	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	100	132	0.73	-	-	-	-	Satisfactory
T1 (RHS):	T1 9.58	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	100	132	0.73	-	-	-	-	Satisfactory

Beam Support Summary:  
T1 (LHS): Provide Minimum 100mm End Bearing Length  
T1 (RHS): Provide Minimum 100mm End Bearing Length  
Refer To G.A. for more details.



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TIMBER BEAM T1 - DESIGN DUE TO BS 5268

<b>Properties of 3No 150x50mm</b>			
Depth h =	145 mm	Timber grade:	C24
Overall breadth of member b =	132 mm	Service Class:	1
Length of bearing lb_l =	100 mm	Load Duration:	Long-term
Length of bearing lb_r =	100 mm	Loadsharing system:	No
Area of beam A =	19140 mm^2	Depth to Breadth Ratio:	5
Min modulus of elasticity Emin =	7.20 GPa		
Modified min modulus of elasticity E =	8.71 GPa	K2 =	1.00 (Service class 1)
Modulus of rigidity G =	0.54 Gpa	K3 =	1.00 (Long-term)
Moment of inertia Iy =	3353 cm^4	K4 =	1.00 (Conservative approach)
Section modulus Zy =	463 cm^3	K5 =	1.00 (Beam without notch)
Root radius ry =	4.19 cm	K7 =	1.08 (72mm < h ≤ 300mm)
		K8 =	1.10 (3No element)
		K9 =	1.21 (3No softwoods element)

Forces in beam

Moment =	2.77 kNm
Shear Force =	6.33 kN
Axial Force =	0.00 kN

Lateral support

Ends held in position and members held in line, as by direct connection of sheathing, deck or joists.

Permissible depth-to-breadth ratio =	5.000
Actual depth-to-breadth ratio =	1.098 OK

Compression perpendicular to grain

Permissible bearing stress σc_adm =	2.640 N/mm^2
Applied bearing stress σc_a =	0.479 N/mm^2 OK

Shear parallel to grain

Permissible shear stress τadm =	0.781 N/mm^2
Applied shear stress τa =	0.496 N/mm^2 OK

Bending parallel to grain

Permissible bending stress σm_adm =	8.937 N/mm^2
Applied bending stress σm_a =	5.984 N/mm^2 OK

Vertical deflection

Total dead and imposed load =	12.65 kN
Shear area for beam Ay =	15950 mm
Beam effective span leff =	1.85 m
Shear deflection δv=	0.319 mm
Bending deflection δb=	3.028 mm
Total deflection δa=	3.347 mm
Limiting deflection =	5.250 mm (0.003L / 14mm) OK

TIMBER BEAM T1 TO BE 3No 150x50mm C24



PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

TIMBER BEAM T2

Beam Span L = 1.50 m

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
Roof (flat)	0.00	1.50	2.50 m
-	0.00	1.50	0.00 m
-	0.00	1.50	0.00 m
-	0.00	1.50	0.00 m
-	0.00	1.50	0.00 m
-	0.00	1.50	0.00 m
-	0.00	1.50	0.00 m

/	2.00	=	1.25 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m

UDL LOADING

UDL Dead Loading

Beam Self Weight									
Roof (flat)	1.00 kN/m2	x	1.25 m	=	0.05 kN/m	x	1.00	=	0.05 kN/m
-	0.00 kN/m2	x	0.00 m	=	1.25 kN/m	x	1.00	=	1.25 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					1.30 kN/m				1.30 kN/m

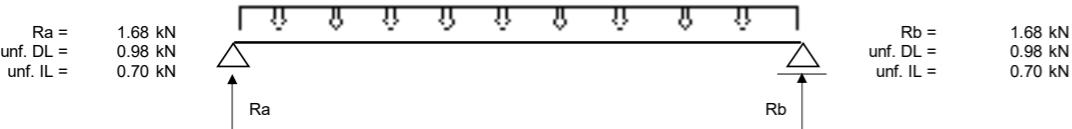
UDL Imposed Loading

Roof (flat)	0.75 kN/m2	x	1.25 m	=	0.94 kN/m	x	1.00	=	0.94 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					0.94 kN/m				0.94 kN/m

Point Load P1 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN

Point Load P2 @	0.00 m
From Beam =	1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN

Point Load P3 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN



FORCES IN BEAM

Moment	=	0.63 kNm
Shear Force	=	1.68 kN
Axial Force	=	0.00 kN

DEFLECTION CRITERIA

0.003L

DURATION OF LOADING

Medium-term (K3 = 1.25)

USAGE OF TIMBER BEAM T2

Compression perpendicular to grain	5.79 %
Shear parallel to grain	20.24 %
Bending parallel to grain	18.30 %
Vertical deflection	20.50 %

TIMBER BEAM T2 = 2No 150x50mm C24

BEARING CHECK

Beam No	Total Vertical Load From kN	Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
T2 (LHS):	T2 2.49	Beam Connection										
T2 (RHS):	T2 2.49	Beam Connection										

Beam Support Summary:

T2 (LHS):	Provide Steel Beam/Column/Timber Post Connection
T2 (RHS):	Provide Steel Beam/Column/Timber Post Connection
	Refer To G.A. for more details.



PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

TIMBER BEAM T2 - DESIGN DUE TO BS 5268

Properties of 2No 150x50mm

Depth h =	145 mm	Timber grade:	C24
Overall breadth of member b =	88 mm	Service Class:	1
Length of bearing lb_l =	100 mm	Load Duration:	Medium-term
Length of bearing lb_r =	100 mm	Loadsharing system:	No
Area of beam A =	12760 mm^2	Depth to Breadth Ratio:	5
Min modulus of elasticity Emin =	7.20 GPa		
Modified min modulus of elasticity E =	8.21 GPa	K2 =	1.00 (Service class 1)
Modulus of rigidity G =	0.51 Gpa	K3 =	1.25 (Medium-term)
Moment of inertia Iy =	2236 cm^4	K4 =	1.00 (Conservative approach)
Section modulus Zy =	308 cm^3	K5 =	1.00 (Beam without notch)
Root radius ry =	4.19 cm	K7 =	1.08 (72mm < h ≤ 300mm)
		K8 =	1.10 (2No element)
		K9 =	1.14 (2No softwoods element)

Forces in beam

Moment	=	0.63 kNm
Shear Force	=	1.68 kN
Axial Force	=	0.00 kN

Lateral support

Ends held in position and members held in line, as by direct connection of sheathing, deck or joists.

Permissible depth-to-breadth ratio =	5.000
Actual depth-to-breadth ratio =	1.648 OK

Compression perpendicular to grain

Permissible bearing stress σc_adm =	3.300 N/mm^2
Applied bearing stress σc_a =	0.191 N/mm^2 OK

Shear parallel to grain

Permissible shear stress τadm =	0.976 N/mm^2
Applied shear stress τa =	0.198 N/mm^2 OK

Bending parallel to grain

Permissible bending stress σm_adm =	11.171 N/mm^2
Applied bending stress σm_a =	2.044 N/mm^2 OK

Vertical deflection

Total dead and imposed load =	3.36 kN
Shear area for beam Ay =	10633 mm
Beam effective span leff =	1.60 m
Shear deflection δv =	0.116 mm
Bending deflection δb =	0.807 mm
Total deflection δa =	0.922 mm
Limiting deflection =	4.500 mm (0.003L) OK

TIMBER BEAM T2 TO BE 2No 150x50mm C24



PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

TIMBER BEAM T3

Beam Span L = 2.70 m

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
Roof (flat)	0.00	2.70	1.90 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m

/	2.00	=	0.95 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m

UDL LOADING

UDL Dead Loading

Beam Self Weight

Roof (flat)	1.00 kN/m2	x	0.95 m	=	0.05 kN/m	x	1.00	=	0.05 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					1.00 kN/m				1.00 kN/m

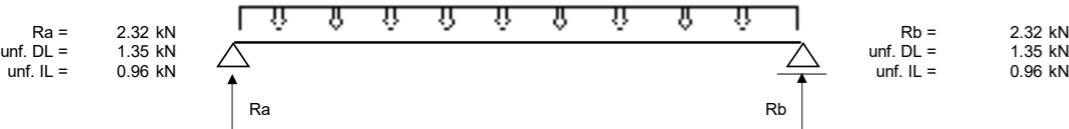
UDL Imposed Loading

Roof (flat)	0.75 kN/m2	x	0.95 m	=	0.71 kN/m	x	1.00	=	0.71 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					0.71 kN/m				0.71 kN/m

Point Load P1 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN

Point Load P2 @	0.00 m
From Beam =	1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN

Point Load P3 @	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)
DL =	0.00 kN x 1.00 = 0.00 kN
IL =	0.00 kN x 1.00 = 0.00 kN



FORCES IN BEAM

Moment	=	1.56 kNm
Shear Force	=	2.32 kN
Axial Force	=	0.00 kN

DEFLECTION CRITERIA

0.003L

DURATION OF LOADING

Medium-term (K3 = 1.25)

USAGE OF TIMBER BEAM T3

Compression perpendicular to grain	7.98 %
Shear parallel to grain	27.90 %
Bending parallel to grain	45.40 %
Vertical deflection	83.60 %

TIMBER BEAM T3 = 2No 150x50mm C24

BEARING CHECK

Beam No	Total Vertical Load From kN	Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
T3 (LHS):	T3 3.44	3.6N Blocks	3.5	1.25x1k/3.5 1.25	100	88	0.39	-	-	-	-	Satisfactory
T3 (RHS):	T3 3.44	Beam Connection										

Beam Support Summary:

T3 (LHS):	Provide Minimum 100mm End Bearing Length
T3 (RHS):	Provide Steel Beam/Column/Timber Post Connection
	Refer To G.A. for more details.



PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

TIMBER BEAM T3 - DESIGN DUE TO BS 5268

Properties of 2No 150x50mm

Depth h =	145 mm	Timber grade:	C24
Overall breadth of member b =	88 mm	Service Class:	1
Length of bearing lb_l =	100 mm	Load Duration:	Medium-term
Length of bearing lb_r =	100 mm	Loadsharing system:	No
Area of beam A =	12760 mm^2	Depth to Breadth Ratio:	5
Min modulus of elasticity Emin =	7.20 GPa		
Modified min modulus of elasticity E =	8.21 GPa	K2 =	1.00 (Service class 1)
Modulus of rigidity G =	0.51 Gpa	K3 =	1.25 (Medium-term)
Moment of inertia Iy =	2236 cm^4	K4 =	1.00 (Conservative approach)
Section modulus Zy =	308 cm^3	K5 =	1.00 (Beam without notch)
Root radius ry =	4.19 cm	K7 =	1.08 (72mm < h ≤ 300mm)
		K8 =	1.10 (2No element)
		K9 =	1.14 (2No softwoods element)

Forces in beam

Moment	=	1.56 kNm
Shear Force	=	2.32 kN
Axial Force	=	0.00 kN

Lateral support

Ends held in position and members held in line, as by direct connection of sheathing, deck or joists.

Permissible depth-to-breadth ratio =	5.000
Actual depth-to-breadth ratio =	1.648 OK

Compression perpendicular to grain

Permissible bearing stress σc_adm =	3.300 N/mm^2
Applied bearing stress σc_a =	0.263 N/mm^2 OK

Shear parallel to grain

Permissible shear stress τadm =	0.976 N/mm^2
Applied shear stress τa =	0.272 N/mm^2 OK

Bending parallel to grain

Permissible bending stress σm_adm =	11.171 N/mm^2
Applied bending stress σm_a =	5.071 N/mm^2 OK

Vertical deflection

Total dead and imposed load =	4.63 kN
Shear area for beam Ay =	10633 mm
Beam effective span leff =	2.80 m
Shear deflection δv=	0.287 mm
Bending deflection δb=	6.484 mm
Total deflection δa=	6.771 mm
Limiting deflection =	8.100 mm (0.003L) OK

TIMBER BEAM T3 TO BE 2No 150x50mm C24

Beam Span  $L =$  2.70 m

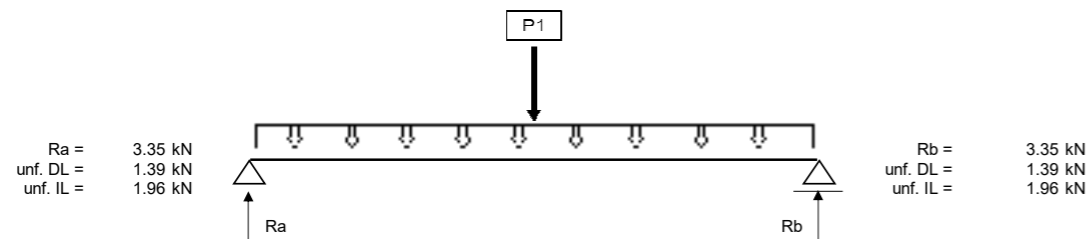
Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
Roof (flat)	0.00	2.70	1.20 m
Roof (flat)	0.00	2.70	0.70 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m
-	0.00	2.70	0.00 m

/	2.00	=	0.60 m	
/	2.00	=	0.35 m	as Glazing
/	1.00	=	0.00 m	
/	1.00	=	0.00 m	
/	1.00	=	0.00 m	

Roof (flat)	1.00 kN/m <sup>2</sup>	x	0.60 m	=	0.60 kN/m	x	1.00	=	0.60 kN/m
Roof (flat)	1.00 kN/m <sup>2</sup>	x	0.35 m	=	0.35 kN/m	x	1.00	=	0.35 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>1.03 kN/m</b>				<b>1.03 kN/m</b>

Roof (flat)	0.75 kN/m <sup>2</sup>	x	0.60 m	=	0.45 kN/m	x	1.00	=	0.45 kN/m
Roof (flat)	0.75 kN/m <sup>2</sup>	x	0.35 m	=	0.26 kN/m	x	1.00	=	0.26 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m <sup>2</sup>	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>0.71 kN/m</b>				<b>0.71 kN/m</b>

<b>Point Load P1 @</b>	1.35 m	<b>(CONSERVATIVE APPROACH)</b>				<b>Point Load P2 @</b>	0.00 m				
From Beam	=	1.00 x AIR SOURCE HEAT PUMP(MAX) + 1.00 x (MAX) + 1.0				From Beam	=	1.00 x (MAX)			
DL	=	0.00 kN	x	1.00 =	0.00 kN	DL	=	0.00 kN	x	1.00 =	0.00 kN
IL	=	2.00 kN	x	1.00 =	2.00 kN	IL	=	0.00 kN	x	1.00 =	0.00 kN
<b>Point Load P3 @</b>	0.00 m										
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)									
DL	=	0.00 kN	x	1.00 =	0.00 kN						
IL	=	0.00 kN	x	1.00 =	0.00 kN						



Moment	=	2.94 kNm
Shear Force	=	3.35 kN
Axial Force	=	0.00 kN

**DURATION OF LOADING**  
Long-term

Compression perpendicular to grain	9.63 %
Shear parallel to grain	33.65 %
Bending parallel to grain	71.08 %
Vertical deflection	90.08 %

**TIMBER BEAM T4 = 3No 150x50mm C24**

## BEARING CHECK

[illegible]

**T4 (LHS):** Provide Minimum 100mm End Bearing Length  
**T4 (RHS):** Provide Steel Beam/Column/Timber Post Connection  
Refer To G.A. for more details.

**TIMBER BEAM T4 - DESIGN DUE TO BS 5268**

Depth h =	145 mm	Timber grade:	C24
Overall breadth of member b =	132 mm	Service Class:	1
Length of bearing lb_l =	100 mm	Load Duration:	Long-term
Length of bearing lb_r =	100 mm	Loadsharing system:	No
Area of beam A =	19140 mm <sup>2</sup>	Depth to Breadth Ratio:	5
Min modulus of elasticity Emin =	7.20 GPa		
Modified min modulus of elasticity E =	8.71 GPa	K2 =	1.00 (Service class 1)
Modulus of rigidity G =	0.54 GPa	K3 =	1.00 (Long-term)
Moment of inertia Iy =	3353 cm <sup>4</sup>	K4 =	1.00 (Conservative approach)
Section modulus Zy =	463 cm <sup>3</sup>	K5 =	1.00 (Beam without notch)
Root radius ry =	4.19 cm	K7 =	1.08 (72mm < h ≤ 300mm)
		K8 =	1.10 (3No element)
<b>Forces in beam</b>		K9 =	1.21 (3No softwoods element)

Moment	=	2.94 kNm
Shear Force	=	3.35 kN
Axial Force	=	0.00 kN

Permissible depth-to-breadth ratio = 5.000  
Actual depth-to-breadth ratio = 1.098 OK

Permissible bearing stress  $\sigma_{c\_adm} = 2.640 \text{ N/mm}^2$   
Applied bearing stress  $\sigma_{c\_a} = 0.254 \text{ N/mm}^2$

Permissible shear stress $\tau_{adm}$ =	0.781 N/mm <sup>2</sup>	
Applied shear stress $\tau_a$ =	0.263 N/mm <sup>2</sup>	OK

Permissible bending stress $\sigma_{m\_adm}$ =	8.937 N/mm <sup>2</sup>	
Applied bending stress $\sigma_{m\_a}$ =	6.352 N/mm <sup>2</sup>	OK

Total dead and imposed load =	6.71 kN	
Shear area for beam $A_y$ =	15950 mm	
Beam effective span $l_{eff}$ =	2.80 m	
Shear deflection $\delta_v$ =	0.338 mm	
Bending deflection $\delta_b$ =	6.958 mm	
Total deflection $\delta_a$ =	7.296 mm	
Limiting deflection =	8.100 mm (0.003L)	OK

**TIMBER BEAM T4 TO BE 3No 150x50mm C24**

LINTEL L1  
Clear Span L = 1.00 m  
Total Span = 1.30 m  
Effective Span = 1.15 m

Load	Load Positioned		Element Span/Height				
	from (m)	to (m)					
Ceiling	0.00	1.00	3.70 m	/	2.00	=	1.85 m
Roof (sloping)	0.00	1.00	2.15 m	/	2.00	=	1.08 m
215mm/Cavity Wall	0.00	1.00	0.40 m	/	1.00	=	0.40 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m	/	1.00	=	0.00 m
-	0.00	1.00	0.00 m				
-	0.00	1.00	0.00 m				

UDL LOADING  
UDL Dead Loading

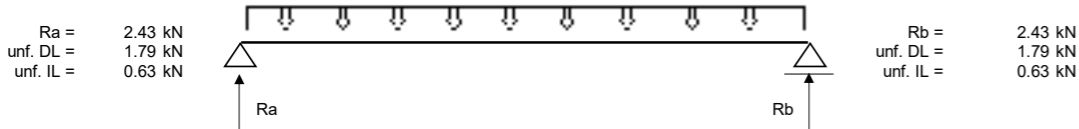
Ceiling	0.45 kN/m2	x	1.85 m	=	0.83 kN/m
Roof (sloping)	1.00 kN/m2	x	1.08 m	=	1.08 kN/m
215mm/Cavity Wall	4.20 kN/m2	x	0.40 m	=	1.68 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
					<b>3.59 kN/m</b>

UDL Imposed Loading

Ceiling	0.25 kN/m2	x	1.85 m	=	0.46 kN/m
Roof (sloping)	0.75 kN/m2	x	1.08 m	=	0.81 kN/m
215mm/Cavity Wall	0.00 kN/m2	x	0.40 m	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
					<b>1.27 kN/m</b>

Total Loads = 4.86 kN/m

Total Loads acting on Lintel = 1.15 m x 4.86 kN/m = 5.58 kN < 29.00 kN Satisfactory



Standard Duty				
	standard lengths are available in 150mm increments.			
	<b>CN71A</b>			
	Standard lengths (mm)	750-1500	1650-2100	2250-2700
	SWL (kN)	29	27	20
		Weight (kg/m)	9.3	9.3
		Nominal height 'h' (mm)	143	143

LINTEL L2  
Clear Span L = 0.90 m  
Total Span = 1.10 m  
Effective Span = 1.00 m

Load	Load Positioned		Element Span/Height				
	from (m)	to (m)					
Timber floor (1st)	0.00	0.90	3.60 m	/	2.00	=	1.80 m
Ceiling	0.00	0.90	5.50 m	/	2.00	=	2.75 m
Roof (sloping)	0.00	0.90	5.50 m	/	2.00	=	2.75 m
100mm Thick Wall	0.00	0.90	2.70 m	/	1.00	=	2.70 m
-	0.00	0.90	0.00 m	/	1.00	=	0.00 m
T1	0.00	0.90	1.50 m				
-	0.00	0.90	0.00 m				

(RHS)

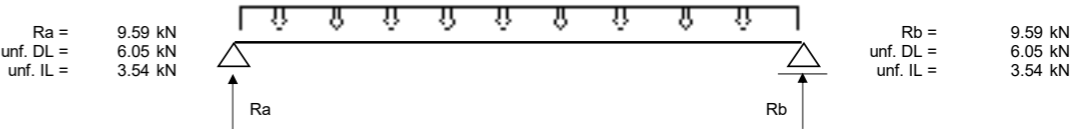
UDL LOADING  
UDL Dead Loading

Timber floor (1st)	1.10 kN/m2	x	1.80 m	=	1.98 kN/m
Ceiling	0.45 kN/m2	x	2.75 m	=	1.24 kN/m
Roof (sloping)	1.00 kN/m2	x	2.75 m	=	2.75 kN/m
100mm Thick Wall	2.10 kN/m2	x	2.70 m	=	5.67 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
T1	2.72 kN	/	1.50 m	=	1.81 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
					<b>13.45 kN/m</b>

UDL Imposed Loading

Timber floor (1st)	1.50 kN/m2	x	1.80 m	=	2.70 kN/m
Ceiling	0.25 kN/m2	x	2.75 m	=	0.69 kN/m
Roof (sloping)	0.75 kN/m2	x	2.75 m	=	2.06 kN/m
100mm Thick Wall	0.00 kN/m2	x	2.70 m	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m
T1	3.61 kN	/	1.50 m	=	2.41 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m
					<b>7.86 kN/m</b>

Total Loads acting on Lintel = 21.31 kN/m < 30.87 kN/m Satisfactory



Hi-Spec Range		R6	R6	R6	R12
Load Table Units suitable for 100mm wide walls					
Fire Resistance Available (mins)		30	30	30	30
Suitable For Foundation Use		Yes	Yes	Yes	Yes
Maximum Stock Length Available		3000mm	3000mm	3600mm	3600mm
Available Range Finish		Faced	Faced	Faced	Faced
UNFACTORED LOADS IN kN/m					
Length	Clear Span	100x100	100x140	100x215	100x290
900mm	700mm	15.77	38.72	96.25	127.77
1200mm	1000mm	10.90	30.87	62.92	83.26

LINTEL L3  
Clear Span L = 3.00 m  
Total Span = 3.30 m  
Effective Span = 3.15 m

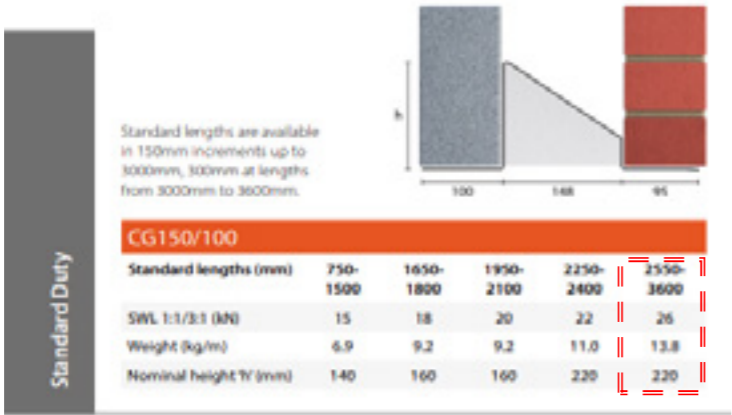
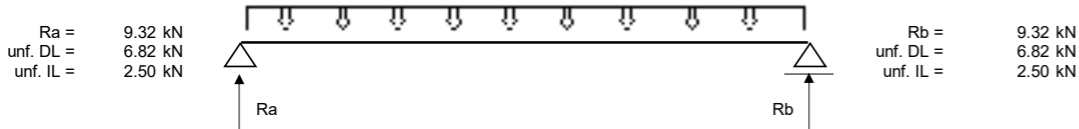
Load	Load Positioned		Element Span/Height			
	from (m)	to (m)				
Roof (flat)	0.00	3.00	2.70 m	/	2.00	= 1.35 m
-	0.00	3.00	0.00 m	/	1.00	= 0.00 m
215mm/Cavity Wall	0.00	3.00	0.65 m	/	1.00	= 0.65 m
-	0.00	3.00	0.00 m	/	1.00	= 0.00 m
-	0.00	3.00	0.00 m	/	1.00	= 0.00 m
T4	0.00	3.00	3.00 m			
-	0.00	3.00	0.00 m			

UDL LOADING						
UDL Dead Loading						
Roof (flat)	1.00 kN/m2	x	1.35 m	=	1.35 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
215mm/Cavity Wall	4.20 kN/m2	x	0.65 m	=	2.73 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
T4	1.39 kN	/	3.00 m	=	0.46 kN/m	
-	0.00 kN	/	0.00 m	=	0.00 kN/m	
					4.54 kN/m	

UDL Imposed Loading						
Roof (flat)	0.75 kN/m2	x	1.35 m	=	1.01 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
215mm/Cavity Wall	0.00 kN/m2	x	0.65 m	=	0.00 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	
T4	1.96 kN	/	3.00 m	=	0.65 kN/m	
-	0.00 kN	/	0.00 m	=	0.00 kN/m	
					1.67 kN/m	

Total Loads = 6.21 kN/m

Total Loads acting on Lintel = 3.15 m x 6.21 kN/m = 19.56 kN < 26.00 kN Satisfactory



BEAM EB1 (Calculated For Loading Purposes Only)  
Beam Span L = 3.70 m

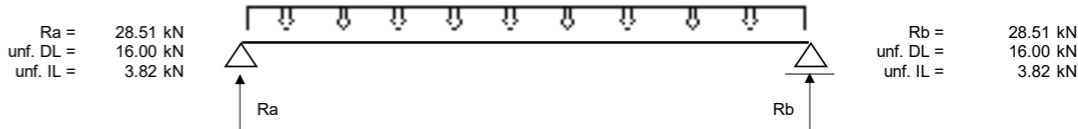
Load	Load Positioned		Element Span/Height			
	from (m)	to (m)				
100mm Thick Wall	0.00	3.70	2.70 m	/	1.00	= 2.70 m
Roof (sloping)	0.00	3.70	5.50 m	/	2.00	= 2.75 m
-	0.00	3.70	0.00 m	/	1.00	= 0.00 m
-	0.00	3.70	0.00 m	/	1.00	= 0.00 m
-	0.00	3.70	0.00 m	/	1.00	= 0.00 m
-	0.00	3.70	0.00 m			
-	0.00	3.70	0.00 m			

UDL LOADING						
UDL Dead Loading						
Beam Self Weight					0.23 kN/m	x 1.40 = 0.32 kN/m
100mm Thick Wall	2.10 kN/m2	x	2.70 m	=	5.67 kN/m	x 1.40 = 7.94 kN/m
Roof (sloping)	1.00 kN/m2	x	2.75 m	=	2.75 kN/m	x 1.40 = 3.85 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.40 = 0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.40 = 0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.40 = 0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x 1.40 = 0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x 1.40 = 0.00 kN/m
					8.65 kN/m	12.11 kN/m

UDL Imposed Loading						
100mm Thick Wall	0.00 kN/m2	x	2.70 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
Roof (sloping)	0.75 kN/m2	x	2.75 m	=	2.06 kN/m	x 1.60 = 3.30 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x 1.60 = 0.00 kN/m
					2.06 kN/m	3.30 kN/m

Point Load P1 @ 0.00 m				Point Load P2 @ 0.00 m			
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)		From Beam	=	1.00 x (MAX)	
DL	=	0.00 kN x 1.40 = 0.00 kN		DL	=	0.00 kN x 1.40 = 0.00 kN	
IL	=	0.00 kN x 1.60 = 0.00 kN		IL	=	0.00 kN x 1.60 = 0.00 kN	

Point Load P3 @ 0.00 m			
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	
DL	=	0.00 kN x 1.40 = 0.00 kN	
IL	=	0.00 kN x 1.60 = 0.00 kN	



**BEAM B1**  
Beam Span L = 3.75 m

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
Roof (flat)	0.00	3.75	2.70 m
Timber floor (1st)	0.00	3.75	3.70 m
Ceiling	0.00	3.75	3.70 m
Roof (sloping)	0.00	3.75	2.15 m
215mm/Cavity Wall	0.00	3.75	3.00 m
-	0.00	3.75	0.00 m
-	0.00	3.75	0.00 m

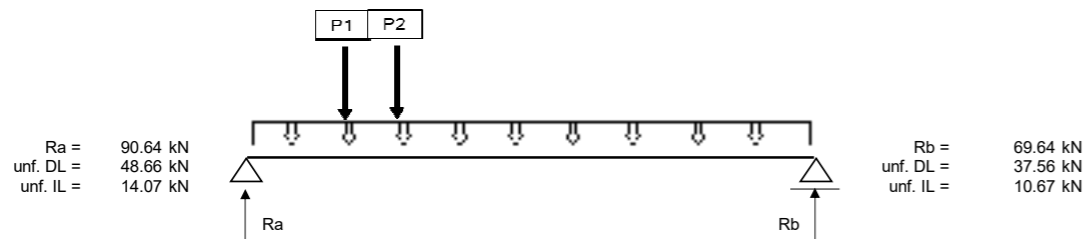
/ 2.00 = 1.35 m  
/ 2.00 = 1.85 m  
/ 2.00 = 1.85 m  
/ 2.00 = 1.08 m  
/ 1.00 = 3.00 m  
Avg. - due to window openings

<b>UDL LOADING</b>									
<b>UDL Dead Loading</b>									
Beam Self Weight									
Roof (flat)	1.00 kN/m2	x	1.35 m	=	0.46 kN/m	x	1.40	=	0.65 kN/m
Timber floor (1st)	1.10 kN/m2	x	1.85 m	=	1.35 kN/m	x	1.40	=	1.89 kN/m
Ceiling	0.45 kN/m2	x	1.85 m	=	2.04 kN/m	x	1.40	=	2.85 kN/m
Roof (sloping)	0.45 kN/m2	x	1.85 m	=	0.83 kN/m	x	1.40	=	1.17 kN/m
215mm/Cavity Wall	1.00 kN/m2	x	1.08 m	=	1.08 kN/m	x	1.40	=	1.51 kN/m
-	4.20 kN/m2	x	3.00 m	=	12.60 kN/m	x	1.40	=	17.64 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.40	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.40	=	0.00 kN/m
					<b>18.35 kN/m</b>				<b>25.69 kN/m</b>

<b>UDL Imposed Loading</b>									
Roof (flat)	0.75 kN/m2	x	1.35 m	=	1.01 kN/m	x	1.60	=	1.62 kN/m
Timber floor (1st)	1.50 kN/m2	x	1.85 m	=	2.78 kN/m	x	1.60	=	4.44 kN/m
Ceiling	0.25 kN/m2	x	1.85 m	=	0.46 kN/m	x	1.60	=	0.74 kN/m
Roof (sloping)	0.75 kN/m2	x	1.08 m	=	0.81 kN/m	x	1.60	=	1.29 kN/m
215mm/Cavity Wall	0.00 kN/m2	x	3.00 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
					<b>5.06 kN/m</b>				<b>8.09 kN/m</b>

<b>Point Load P1 @</b> 0.65 m					<b>Point Load P2 @</b> 1.00 m				
From Beam	=	1.00 x EB1(MAX) + 1.00 x (MAX) + 1.00 x (MAX)			From Beam	=	1.00 x T4(RHS)		
DL	=	16.00 kN x 1.40 = 22.40 kN			DL	=	1.39 kN x 1.40 = 1.95 kN		
IL	=	3.82 kN x 1.60 = 6.11 kN			IL	=	1.96 kN x 1.60 = 3.14 kN		

<b>Point Load P3 @</b> 0.00 m				
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)		
DL	=	0.00 kN x 1.40 = 0.00 kN		
IL	=	0.00 kN x 1.60 = 0.00 kN		



<b>FORCES IN BEAM</b>			<b>DEFLECTION CRITERIA</b>			<b>USAGE OF STEEL BEAM B1</b>		
Moment	=	71.78 kNm	L/300; Brittle finishes (all loads)			Shear capacity		29.09 %
Shear Force	=	90.64 kN	L/360 (imposed loads only)			Moment capacity		44.94 %
Axial Force	=	0.00 kN				Buckling resistance moment		57.91 %
						Vertical deflection		63.15 %

**STEEL BEAM B1 = 203 x 203 x 46 UKC S355** **BEAM WITH PLATE. SEE DETAILS ON SUMMARY PAGE**

## BEARING CHECK

Beam No	Total Vertical Load From kN	Type of Support	Charact. Compr. Strength f <sub>k</sub> , N/mm <sup>2</sup>	Local Strength y <sub>b</sub> *f <sub>k</sub> /γ <sub>m</sub> N/mm <sup>2</sup>	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm <sup>2</sup>	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm <sup>2</sup>	Summary
B1 (LHS):	90.64	Beam Connection										
B1 (RHS):	69.64	Beam Connection										

**Beam Support Summary:**  
**B1 (LHS):** Provide Steel Beam/Column/Timber Post Connection  
**B1 (RHS):** Provide Steel Beam/Column/Timber Post Connection  
Refer To G.A. for more details.

**Beam bearing design details:**  
Restraint Condition Coef. Support A: 1.0 + 2 x D  
Restraint Condition Coef. Support B: 1.0 + 2 x D

## STEEL BEAM B1 - DESIGN DUE TO BS 5950-1

### Properties of 203 x 203 x 46 UKC Section

Design strength of steel p <sub>y</sub> =	355.00 N/mm <sup>2</sup>	Total beam span L =	3.75 m
Half of flange b =	101.80 mm	Web depth d =	160.80 mm
Flange thickness T =	11.0 mm	Web thickness t =	7.2 mm
Area of cross-section A =	58.7 cm <sup>2</sup>	Overall depth D =	203.2 mm
Rad of gyration (minor axis) r =	5.13 cm	Overall breadth B =	203.6 mm
Modulus of elasticity E =	205.00 GPa	Moment of inertia I <sub>x</sub> =	4570 cm <sup>4</sup>
Elastic modulus Z <sub>x</sub> =	450 cm <sup>3</sup>	Plastic modulus S <sub>x</sub> =	497 cm <sup>3</sup>
		Root radius r =	10.20 mm

### Forces in beam

Moment	=	71.78 kNm
Shear Force	=	90.64 kN
Axial Force	=	0.00 kN

### Beam bearing design details

Restraint Condition Coef. Support A:	1.0 + 2 x D
Restraint Condition Coef. Support B:	1.0 + 2 x D

### Classification of cross-section

Parameter ε =	0.880	
Web d/t =	22.33	
Web (d/t)/ε =	25.37 ≤ 80	Class 1 plastic
Flanges b/t =	9.25	
Flanges (b/t)/ε =	10.51 ≤ 15	Class 3 semi-compact

### Section is class 3 semi-compact

### Shear capacity

Shear area A <sub>v</sub> =	1463.04 mm (A <sub>v</sub> = tD, UC section)
Web (d/t)/ε =	25.37 ≤ 70 (Web does not need to be checked for shear buckling)
Shear capacity P <sub>v</sub> =	311.63 kN
Design shear force =	90.64 kN <b>OK</b>

### Moment capacity

Design bending moment M =	71.78 kNm
Moment capacity low shear M <sub>c</sub> =	159.75 kNm (M <sub>c</sub> = p <sub>y</sub> *Z) <b>OK</b>

### Effective length for lateral-torsional buckling

Total Beam Span =	3750 mm
Effective length L <sub>e</sub> =	4156 mm
Slenderness ratio λ =	81.02

### Equivalent slenderness

Buckling parameter u =	0.847
Torsional index x =	17.7
Slenderness factor v =	0.836
Ratio β <sub>w</sub> =	0.905 (Z/S)
Equivalent slenderness λ <sub>LT</sub> =	54.59
Limiting slenderness λ <sub>L0</sub> =	30.20
<b>λ<sub>LT</sub> &gt; λ<sub>L0</sub> (Allowance should be made for lateral-torsional buckling)</b>	

### Bending strenght

Bending strenght p <sub>b</sub> =	275.48 N/mm <sup>2</sup> (With Table 16)
-----------------------------------	--

### Buckling resistance moment

Equivalent uniform moment factor m <sub>LT</sub> =	1.00 (Conservative approach)
Buckling resistance moment M <sub>b</sub> =	123.97 kNm
Design bending moment	71.78 kNm <b>OK</b>

### Vertical dead & imposed load deflection

Limiting deflection =	12.500 mm (L/300; Brittle finishes)
Maximum deflection =	7.893 mm <b>OK</b>

### Vertical imposed load deflection

Limiting deflection =	10.417 mm (L/360)
Maximum deflection =	1.783 mm <b>OK</b>

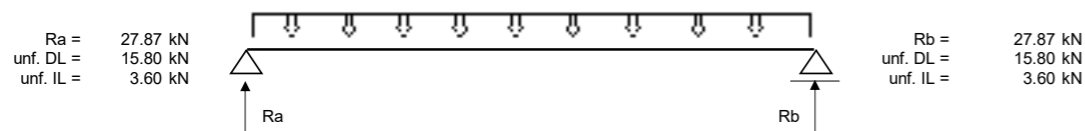
**STEEL BEAM B1 = 203 x 203 x 46 UKC**

Load	Load Positioned		Element
	from (m)	to (m)	Span/Height
Roof (flat)	0.00	1.70	2.70 m
Timber floor (1st)	0.00	1.70	2.60 m
Ceiling	0.00	1.70	3.70 m
Roof (sloping)	0.00	1.70	2.15 m
215mm/Cavity Wall	0.00	1.70	3.20 m
-	0.00	1.70	0.00 m
-	0.00	1.70	0.00 m

UDL LOADING									
UDL Dead Loading									
Beam Self Weight									
Roof (flat)	1.00 kN/m <sup>2</sup>	x	1.35 m	=	0.46 kN/m	x	1.40	=	0.65 kN/m
Timber floor (1st)	1.10 kN/m <sup>2</sup>	x	1.30 m	=	1.43 kN/m	x	1.40	=	2.00 kN/m
Ceiling	0.45 kN/m <sup>2</sup>	x	1.85 m	=	0.83 kN/m	x	1.40	=	1.17 kN/m
Roof (sloping)	1.00 kN/m <sup>2</sup>	x	1.08 m	=	1.08 kN/m	x	1.40	=	1.51 kN/m
215mm/Cavity Wall	4.20 kN/m <sup>2</sup>	x	3.20 m	=	13.44 kN/m	x	1.40	=	18.82 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.40	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.40	=	0.00 kN/m
					<b>18.59 kN/m</b>				<b>26.02 kN/m</b>

UDL Imposed Loading									
Roof (flat)	0.75 kN/m <sup>2</sup>	x	1.35 m	=	1.01 kN/m	x	1.60	=	1.62 kN/m
Timber floor (1st)	1.50 kN/m <sup>2</sup>	x	1.30 m	=	1.95 kN/m	x	1.60	=	3.12 kN/m
Ceiling	0.25 kN/m <sup>2</sup>	x	1.85 m	=	0.46 kN/m	x	1.60	=	0.74 kN/m
Roof (sloping)	0.75 kN/m <sup>2</sup>	x	1.08 m	=	0.81 kN/m	x	1.60	=	1.29 kN/m
215mm/Cavity Wall	0.00 kN/m <sup>2</sup>	x	3.20 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.60	=	0.00 kN/m
					<b>4.23 kN/m</b>				<b>6.77 kN/m</b>

<b>Point Load P1 @</b>	0.00 m	<b>Point Load P2 @</b>	0.00 m
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	From Beam =	1.00 x (MAX)
DL =	0.00 kN x 1.40 = 0.00 kN	DL =	0.00 kN x 1.40 = 0.00 kN
IL =	0.00 kN x 1.60 = 0.00 kN	IL =	0.00 kN x 1.60 = 0.00 kN
 <b>Point Load P3 @</b>	0.00 m		
From Beam =	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)		
DL =	0.00 kN x 1.40 = 0.00 kN		
IL =	0.00 kN x 1.60 = 0.00 kN		

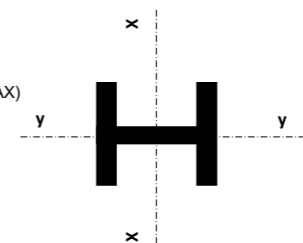
[illegible]

PROJECT No. <b>K-25-02-80-C01</b>	DATE <b>24.02.25</b>	REV <b>0</b>
ENG. <b>PP</b>	CHD. <b>KJ</b>	CHD. <b>KJ</b>
PROJECT <b>10 Trelawn, London E10 5QD</b>		

Slenderness factor:  $v = 1 / [1 + 0.05 (\lambda y / x)^2]^{0.25} = 0.75$   
 Equiv. Slenderness:  $\lambda_{LT} = u v \lambda y \sqrt{\beta_w} = 85.68$

From Beam =  $1.00 \times (\text{MAX}) + 1.00 \times (\text{MAX}) + 1.00 \times (\text{MAX})$   
DL = 0.00 kN  
IL = 0.00 kN  
Eccentricity =  $B/2 = 76.10 \text{ mm}$

From Beam = 1.00 x B1.(RHS) + 1.00 x (MAX) + 1.00 x (MAX)		From Beam = 1.00 x B1.(LHS) + 1.00 x (MAX) + 1.00 x (MAX)
DL = 15.80 kN		DL = 48.66 kN
IL = 3.60 kN		IL = 14.07 kN
Excentricity = D/2 = 76.20 mm		Excentricity = D/2 = -76.20 mm



From Beam =  $1.00 \times (\text{MAX}) + 1.00 \times (\text{MAX}) + 1.00 \times (\text{MAX})$   
DL = 0.00 kN  
IL = 0.00 kN  
Eccentricity =  $B/2 = -76.10 \text{ mm}$

Wind Load	=	0.00 kN/m2
Area	=	0.00 m2
Total Horizontal Load	=	0.00 kN
Construction	=	Simply Supported
Wind Load Applied in	=	Major Axis (x-x)

Load Combination 1 1.4 DL + 1.6 IL			Load Combination 2 1.4 DL + 1.4 WL			Load Combination 3 1.2 DL + 1.2 IL + 1.2 WL		
Axial Force	=	118.52 kN	Axial Force	=	90.25 kN	Axial Force	=	98.56 kN
Shear Force	=	0.00 kN	Shear Force	=	0.00 kN	Shear Force	=	0.00 kN
Moment x-x	=	4.78 kNm	Moment x-x	=	3.51 kNm	Moment x-x	=	3.96 kNm
Moment y-y	=	0.00 kNm	Moment y-y	=	0.00 kNm	Moment y-y	=	0.00 kNm

<b>Factored Forces</b>			<b>Unfactored Forces</b>		
Max. Axial Force, Fc	=	118.52 kN	Max. Axial Force DL	=	64.46 kN
Max. Shear Force	=	0.00 kN	Max. Axial Force IL	=	17.67 kN
Max. Major Moment x-x, Mx	=	4.78 kNm	Max. Shear Force	=	0.00 kN
Max. Minor Moment y-y, My	=	0.00 kNm	Max Moment x-x	=	3.30 kNm
			Max Moment y-y	=	0.00 kNm

Design Strength of Steel	py	=	355.00 N/mm2	
Compressive Strength	pcy	=	87.00 N/mm2	(table 24, curve c)
Bending Strength	pb	=	175.00 N/mm2	(table 16 for I-sections, pb = py for SHS sections)

<b>ACTUAL</b>			
Compression Resistance	$P_{cy} = A_g \cdot \phi_y$	=	254.04 kN
Moment Capacity (Major Axis)	$M_{c,x} = \phi_y \cdot Z_x$	=	58.22 kNm
Moment Capacity (Minor Axis)	$M_{c,y} = \phi_y \cdot Z_y$	=	18.67 kNm
Buckling Resistance Moment	$M_b = \phi_b \cdot Z_x$	=	28.70 kNm (For SHS Sections $M_b = M_{c,x}$ )

[1] Fc / Pcy	=	0.47	OK
[2] mLT * Mx / Mb ; mLT = 1.0	=	0.17	OK
[3] my * My / Mc,y ; my = 1.0	=	0.00	OK

$[1] + [2] + [3] = 0.63 < 1.00$  OK

Allowable Deflection	L/300	=	11.17 mm
Moment from vertical loads: x-x	M	=	3.30 kNm
Vertical loads max deflection: x-x	$M^*L^2 / 16EI$	=	0.90 mm
Moment from vertical loads: y-y	M	=	0.00 kNm
Vertical loads max deflection: y-y	$M^*L^2 / 16EI$	=	0.00 mm
Wind load Horizontal force	H	=	0.00 kN
Wind loads maximum deflection	$H * L^3 / 48EI$	=	0.00 mm
<b>Max Deflection</b>		=	<b>0.90 mm</b>

STEEL COLUMN C2 = 152 x 152 x 23 UKC (S355)

PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

## LOADS ACTING ON THE FOOTING (BELOW COLUMN C1)

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m

/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m

<b>UDL LOADING</b>									
<b>UDL Dead Loading</b>									
Selfweight	24.00 kN/m3	x	0.10 m2	=	2.43 kN/m	x	1.00	=	2.43 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>2.43 kN/m</b>				<b>2.43 kN/m</b>

<b>UDL Imposed Loading</b>									
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>0.00 kN/m</b>				<b>0.00 kN/m</b>

<b>Point Load P1</b>									
From Beam	=	1.00 x B1.(LHS) + 1.00 x (MAX) + 1.00 x (MAX)							
DL	=	15.80 kN	x	1.00	=	15.80 kN			
IL	=	3.60 kN	x	1.00	=	3.60 kN			
				SUM:		19.40 kN			

<b>Point Load P2</b>									
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)							
DL	=	0.00 kN	x	1.00	=	0.00 kN			
IL	=	0.00 kN	x	1.00	=	0.00 kN			
				SUM:		0.00 kN			

## DESIGN FORCES

<b>STRIP FOOTING OPTION</b>				
Vertical Force	N	=	20.85 kN	1*B1. (LHS)+UDL*Load Dispersion Length

<b>PAD FOUNDATION OPTION</b>				
Vertical Force	Pz	=	19.40 kN	1*B1. (LHS)+UDL*Pad Dimension
Horizontal Force in x direction	Fx	=	0.00 kN	
Horizontal Force in y direction	Fy	=	0.00 kN	

Major axis moment x-x	Mxx	=	0.00 kNm	
Major axis moment y-y	Myy	=	0.00 kNm	

Eccentricity x-x	ex	=	225.00 mm	
Eccentricity y-y	ey	=	0.00 mm	

Allowable Bearing Capacity of Soil	=	100.00 kN/m2
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PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

## LOCATION: COLUMN C1 STRIP FOOTING OPTION

Plan Area Required	N/Allowable Bearing Capacity of Soil	=	0.21 m2
Minimum Footing Width	W	=	0.45 m
Minimum Footing Depth	D	=	0.60 m

Plan Area Provided	W*(D)	=	0.27 m2
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Plan Area Required	<	Plan Area Provided	Satisfactory (0.77)
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## BEARING CHECK BELOW COLUMN C1 PADSTONE @ GROUND FLOOR LEVEL

Total Vertical Load From		Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
C1	27.87	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	-	-	-	300	215	0	0.43	Satisfactory

<b>COLUMN C1 Padstone Summary:</b>	
Provide MIN 300x(Wall Width)x215 Concrete Padstone	

<b>STRIP FOOTINGS ARE SATISFACTORY IF BELOW CRITERIA ARE FULFILLED:</b>	
<b>- DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL IS NOT LESS THAN 0.60m</b>	
<b>- FOOTING WIDTH IS NOT LESS THAN 0.45m; FOOTING THICKNESS IS NOT LESS THAN 0.225m FOR NEW STRIP FOOTING</b>	

## PAD FOUNDATION OPTION

### FOUNDATION DIMENSIONS

Length of Pad Footing	L	=	0.80 m
Width of Pad Footing	B	=	0.80 m
Depth of Pad Footing	H	=	0.30 m

Pad Foundation Selfweight	Sf	=	7.20 kN/m2
Area of Pad Foundation	A=L*B	=	0.64 m2

Bearing Pressure	(Pz+Sf)/A	=	37.51 kN/m2	Satisfactory
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### CHECK STABILITY AGAINST OVERTURNING IN X-DIRECTION

Total Overturning Moment	Mox=Myy+Fx*H	=	0.00 kNm
Total Restoring Moment	Mrx=Pz*(L/2-ex)+Sf*A*L/2	=	5.24 kNm
Overturning Safety Factor	FOS=Mrx/Mox	=	Correct

### CHECK STABILITY AGAINST OVERTURNING IN Y-DIRECTION

Total Overturning Moment	Moy=Mxx+Fy*H	=	0.00 kNm
Total Restoring Moment	Mry=Pz*(B/2-ey)+Sf*A*B/2	=	9.60 kNm
Overturning Safety Factor	FOS=Mry/Moy	=	Correct

### PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN X-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	24.00 kN
Total Pad Base Moment	Mbx=Myy+Pz*ex+Fx*H	=	4.36 kNm

Maximum Base Pressure	qxmax=T/A+6*Mbx/(B*L*L)	=	88.65 kN/m2	Satisfactory	(0.89)
Minimum Base Pressure	qxmin=T/A-6*Mbx/(B*L*L)	=	-13.64 kN/m2	Uplift	

### PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN Y-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	24.00 kN
Total Pad Base Moment	Mby=Mxx+Pz*ey+Fy*H	=	0.00 kNm

Maximum Base Pressure	qymax=T/A+6*Mby/(L*B*B)	=	37.51 kN/m2	Satisfactory	(0.38)
Minimum Base Pressure	qymin=T/A-6*Mby/(L*B*B)	=	37.51 kN/m2	Satisfactory	(0.38)

### CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN X-DIRECTION

Half of base	l=L/2	=	0.40 m
Middle Third of Base	tx=L/6	=	0.13 m
Eccentricity of Base Reaction	ebx=Mbx/T	=	0.18 m

Outside Middle Third of Base  
**Need to Check Critical Edge Pressure**

### CRITICAL EDGE PRESSURE IN X-DIRECTION

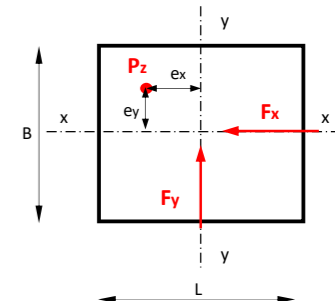
Length of Base in Contact	$L_e = 3 \cdot (l - e_{bx})$	=	0.65 m		
Critical Bearing Pressure	$Q_x = 2 \cdot T / (B \cdot L_e)$	=	91.68 kN/m <sup>2</sup>	Satisfactory	(0.92)

### CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN Y-DIRECTION

Half of base	b=B/2	=	0.40 m	
Middle Third of Base	ty=B/6	=	0.13 m	
Eccentricity of Base Reaction	eby=Mby/T	=	0.00 m	Within Middle Third of Base

Bearing Pressure	Qy=qymax	=	37.51 kN/m2	Satisfactory	(0.38)
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**PROVIDE 0.80m x 0.80m PAD FOOTING WITH 0.30m PAD THICKNESS  
AND 2No A393 MESH (1 TOP & 1 BOTTOM)**



## LOADS ACTING ON THE FOOTING (BELOW COLUMN C2)

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m

/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m  
/ 1.00 = 0.00 m

### UDL LOADING

#### UDL Dead Loading

Selfweight	24.00 kN/m3	x	0.10 m2	=	2.43 kN/m	x	1.00	=	2.43 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					2.43 kN/m				
					2.43 kN/m				

#### UDL Imposed Loading

-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					0.00 kN/m				
					0.00 kN/m				

### Point Load P1

From Beam	=	1.00 x B1.(RHS) + 1.00 x B1(LHS) + 1.00 x (MAX)	
DL	=	64.46 kN	x 1.00 = 64.46 kN
IL	=	17.67 kN	x 1.00 = 17.67 kN
		SUM:	82.13 kN

### Point Load P2

From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)	
DL	=	0.00 kN	x 1.00 = 0.00 kN
IL	=	0.00 kN	x 1.00 = 0.00 kN
		SUM:	0.00 kN

### DESIGN FORCES

#### STRIP FOOTING OPTION

Vertical Force	N	=	86.99 kN	1*B1. (RHS) +1*B1 (LHS)+UDL*Load Dispersion Length
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#### PAD FOUNDATION OPTION

Vertical Force	Pz	=	82.13 kN	1*B1. (RHS) +1*B1 (LHS)+UDL*Pad Dimension
Horizontal Force in x direction	Fx	=	0.00 kN	
Horizontal Force in y direction	Fy	=	0.00 kN	

Major axis moment x-x	Mxx	=	0.00 kNm
Major axis moment y-y	Myy	=	0.00 kNm

Eccentricity x-x	ex	=	0.00 mm
Eccentricity y-y	ey	=	0.00 mm

Allowable Bearing Capacity of Soil	=	100.00 kN/m2
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## LOCATION: COLUMN C2 STRIP FOOTING OPTION

Plan Area Required	N/Allowable Bearing Capacity of Soil	=	0.87 m2
Minimum Footing Width	W	=	0.45 m
Minimum Footing Depth	D	=	1.00 m

Plan Area Provided	W*(2*D)	=	0.90 m2
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Plan Area Required < Plan Area Provided Satisfactory (0.97)

### BEARING CHECK BELOW COLUMN C2 PADSTONE @ GROUND FLOOR LEVEL

Total Vertical Load From		Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
C2	118.52	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	-	-	-	700	215	0	0.79	Satisfactory

#### COLUMN C2 Padstone Summary:

Provide MIN 700x(Wall Width)x300 Concrete Padstone

STRIP FOOTINGS ARE SATISFACTORY IF BELOW CRITERIA ARE FULFILLED:  
- DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL IS NOT LESS THAN 1.00m  
- FOOTING WIDTH IS NOT LESS THAN 0.45m; FOOTING THICKNESS IS NOT LESS THAN 0.225m FOR NEW STRIP FOOTING

### PAD FOUNDATION OPTION

#### FOUNDATION DIMENSIONS

Length of Pad Footing	L	=	1.00 m
Width of Pad Footing	B	=	1.00 m
Depth of Pad Footing	H	=	0.40 m

Pad Foundation Selfweight	Sf	=	9.60 kN/m2
Area of Pad Foundation	A=L*B	=	1.00 m2

Bearing Pressure	(Pz+Sf)/A	=	91.73 kN/m2	Satisfactory
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#### CHECK STABILITY AGAINST OVERTURNING IN X-DIRECTION

Total Overturning Moment	Mox=Myy+Fx*H	=	0.00 kNm
Total Restoring Moment	Mrx=Pz*(L/2-ex)+Sf*A*L/2	=	45.87 kNm
Overturning Safety Factor	FOS=Mrx/Mox	=	Correct

#### CHECK STABILITY AGAINST OVERTURNING IN Y-DIRECTION

Total Overturning Moment	Moy=Mxx+Fy*H	=	0.00 kNm
Total Restoring Moment	Mry=Pz*(B/2-ey)+Sf*A*B/2	=	45.87 kNm
Overturning Safety Factor	FOS=Mry/Moy	=	Correct

#### PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN X-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	91.73 kN
Total Pad Base Moment	Mbx=Myy+Pz*ex+Fx*H	=	0.00 kNm

Maximum Base Pressure	qxmax=T/A+6*Mbx/(B*L*L)	=	91.73 kN/m2	Satisfactory	(0.92)
Minimum Base Pressure	qxmin=T/A-6*Mbx/(B*L*L)	=	91.73 kN/m2	Satisfactory	(0.92)

#### PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN Y-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	91.73 kN
Total Pad Base Moment	Mby=Mxx+Pz*ey+Fy*H	=	0.00 kNm

Maximum Base Pressure	qymax=T/A+6*Mby/(L*B*B)	=	91.73 kN/m2	Satisfactory	(0.92)
Minimum Base Pressure	qymin=T/A-6*Mby/(L*B*B)	=	91.73 kN/m2	Satisfactory	(0.92)

#### CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN X-DIRECTION

Half of base	$l=L/2$	=	0.50 m	
Middle Third of Base	$tx=L/6$	=	0.17 m	
Eccentricity of Base Reaction	$ebx=Mbx/T$	=	0.00 m	Within Middle Third of Base

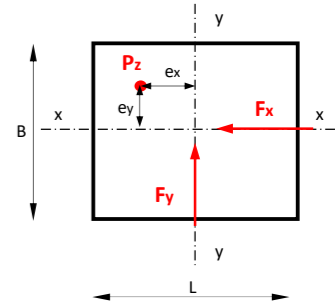
Bearing Pressure	Qx=qxmax	=	91.73 kN/m2	Satisfactory	(0.92)
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#### CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN Y-DIRECTION

Half of base	b=B/2	=	0.50 m	
Middle Third of Base	ty=B/6	=	0.17 m	
Eccentricity of Base Reaction	eby=Mby/T	=	0.00 m	Within Middle Third of Base

Bearing Pressure	Qy=qymax	=	91.73 kN/m2	Satisfactory	(0.92)
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PROVIDE 1.00m x 1.00m PAD FOOTING WITH 0.40m PAD THICKNESS  
AND 3No A393 MESH (1 TOP & 2 BOTTOM)



PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

## LOADS ACTING ON THE FOOTING (BELOW COLUMN C3)

Load	Load Positioned		Element Span/Height
	from (m)	to (m)	
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m
-	0.00	1.00	0.00 m

/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m
/	1.00	=	0.00 m

<b>UDL LOADING</b>									
<b>UDL Dead Loading</b>									
Selfweight	24.00 kN/m3	x	0.10 m2	=	2.43 kN/m	x	1.00	=	2.43 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>2.43 kN/m</b>				<b>2.43 kN/m</b>

<b>UDL Imposed Loading</b>									
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN/m2	x	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
-	0.00 kN	/	0.00 m	=	0.00 kN/m	x	1.00	=	0.00 kN/m
					<b>0.00 kN/m</b>				<b>0.00 kN/m</b>

<b>Point Load P1</b>									
From Beam	=	1.00 x B1(RHS) + 1.00 x (MAX) + 1.00 x (MAX)							
DL	=	37.56 kN	x	1.00	=	37.56 kN			
IL	=	10.67 kN	x	1.00	=	10.67 kN			
					SUM:	48.22 kN			

<b>Point Load P2</b>									
From Beam	=	1.00 x (MAX) + 1.00 x (MAX) + 1.00 x (MAX)							
DL	=	0.00 kN	x	1.00	=	0.00 kN			
IL	=	0.00 kN	x	1.00	=	0.00 kN			
					SUM:	0.00 kN			

## DESIGN FORCES

<b>STRIP FOOTING OPTION</b>				
Vertical Force	N	=	51.14 kN	1*B1 (RHS)+UDL*Load Dispersion Length

<b>PAD FOUNDATION OPTION</b>				
Vertical Force	Pz	=	48.22 kN	1*B1 (RHS)+UDL*Pad Dimension
Horizontal Force in x direction	Fx	=	0.00 kN	
Horizontal Force in y direction	Fy	=	0.00 kN	

Major axis moment x-x	Mxx	=	0.00 kNm	
Major axis moment y-y	Myy	=	0.00 kNm	

Eccentricity x-x	ex	=	517.50 mm	
Eccentricity y-y	ey	=	0.00 mm	

Allowable Bearing Capacity of Soil	=	100.00 kN/m2
------------------------------------	---	--------------

PROJECT No.	DATE	REV
K-25-02-80-C01	24.02.25	0
ENG.	CHD.	CHD.
PP	KJ	KJ
PROJECT		
10 Trelawn, London E10 5QD		

## LOCATION: COLUMN C3 STRIP FOOTING OPTION

Plan Area Required	N/Allowable Bearing Capacity of Soil	=	0.51 m2
Minimum Footing Width	W	=	0.45 m
Minimum Footing Depth	D	=	1.20 m

Plan Area Provided	W*(D)	=	0.54 m2
--------------------	-------	---	---------

Plan Area Required	<	Plan Area Provided	Satisfactory (0.95)
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## BEARING CHECK BELOW COLUMN C3 PADSTONE @ GROUND FLOOR LEVEL

Total Vertical Load From		Type of Support	Charact. Compr. Strength fk, N/mm2	Local Strength yb*fk/ym N/mm2	Bearing Length mm	Bearing Width mm	Stress Below Bearing N/mm2	Padstone Length mm	Padstone Width mm	Ecc mm	Stress Below Padstone N/mm2	Summary
C3	69.64	Ex. Historic Brick	2.25	1.25xfk/3.5 0.80	-	-	-	440	215	0	0.74	Satisfactory

**COLUMN C3 Padstone Summary:**  
Provide MIN 440x(Wall Width)x215 Concrete Padstone

**STRIP FOOTINGS ARE SATISFACTORY IF BELOW CRITERIA ARE FULFILLED:**  
- DISTANCE MEASURED FROM BASEPLATE TO UNDERSIDE OF FOOTING LEVEL IS NOT LESS THAN 1.20m  
- FOOTING WIDTH IS NOT LESS THAN 0.45m; FOOTING THICKNESS IS NOT LESS THAN 0.225m FOR NEW STRIP FOOTING

## PAD FOUNDATION OPTION

<b>FOUNDATION DIMENSIONS</b>			
Length of Pad Footing	L	=	1.40 m
Width of Pad Footing	B	=	1.40 m
Depth of Pad Footing	H	=	0.60 m

Pad Foundation Selfweight	Sf	=	14.40 kN/m2
Area of Pad Foundation	A=L*B	=	1.96 m2

Bearing Pressure	(Pz+Sf)/A	=	39.00 kN/m2	Satisfactory
------------------	-----------	---	-------------	--------------

## CHECK STABILITY AGAINST OVERTURNING IN X-DIRECTION

Total Overturning Moment	Mox=Myy+Fx*H	=	0.00 kNm
Total Restoring Moment	Mrx=Pz*(L/2-ex)+Sf*A*L/2	=	28.56 kNm
Overturning Safety Factor	FOS=Mrx/Mox	=	Correct

## CHECK STABILITY AGAINST OVERTURNING IN Y-DIRECTION

Total Overturning Moment	Moy=Mxx+Fy*H	=	0.00 kNm
Total Restoring Moment	Mry=Pz*(B/2-ey)+Sf*A*B/2	=	53.51 kNm
Overturning Safety Factor	FOS=Mry/Moy	=	Correct

## PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN X-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	76.45 kN
Total Pad Base Moment	Mbx=Myy+Pz*ex+Fx*H	=	24.96 kNm

Maximum Base Pressure	qxmax=T/A+6*Mbx/(B*L*L)	=	93.57 kN/m2	Satisfactory	(0.94)
Minimum Base Pressure	qxmin=T/A-6*Mbx/(B*L*L)	=	-15.56 kN/m2	Uplift	

## PAD FOUNDATION BASE REACTIONS AND BASE PRESSURES IN Y-DIRECTION

Total Pad Base Reaction	T=Pz+Sf*A	=	76.45 kN
Total Pad Base Moment	Mby=Mxx+Pz*ey+Fy*H	=	0.00 kNm

Maximum Base Pressure	qymax=T/A+6*Mby/(L*B*B)	=	39.00 kN/m2	Satisfactory	(0.39)
Minimum Base Pressure	qymin=T/A-6*Mby/(L*B*B)	=	39.00 kN/m2	Satisfactory	(0.39)

## CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN X-DIRECTION

Half of base	$l=L/2$	=	0.70 m	
Middle Third of Base	$tx=L/6$	=	0.23 m	
Eccentricity of Base Reaction	$ebx=Mbx/T$	=	0.33 m	Outside Middle Third of Base

## CRITICAL EDGE PRESSURE IN X-DIRECTION

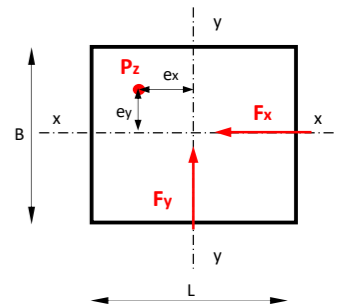
Length of Base in Contact	$Le=3*(l-ebx)$	=	1.12 m		
Critical Bearing Pressure	$Qx=2*T/(B*Le)$	=	97.45 kN/m2	Satisfactory	(0.97)

## CHECK PAD BASE REACTION ECCENTRICITY AND BEARING PRESSURE IN Y-DIRECTION

Half of base	$b=B/2$	=	0.70 m
Middle Third of Base	$ty=B/6$	=	0.23 m
Eccentricity of Base Reaction	$eby=Mby/T$	=	0.00 m
			Within Middle Third of Base

Bearing Pressure	Qy=qymax	=	39.00 kN/m2	Satisfactory	(0.39)
------------------	----------	---	-------------	--------------	--------

**PROVIDE 1.40m x 1.40m PAD FOOTING WITH 0.60m PAD THICKNESS AND 3No A393 MESH (1 TOP & 2 BOTTOM)**

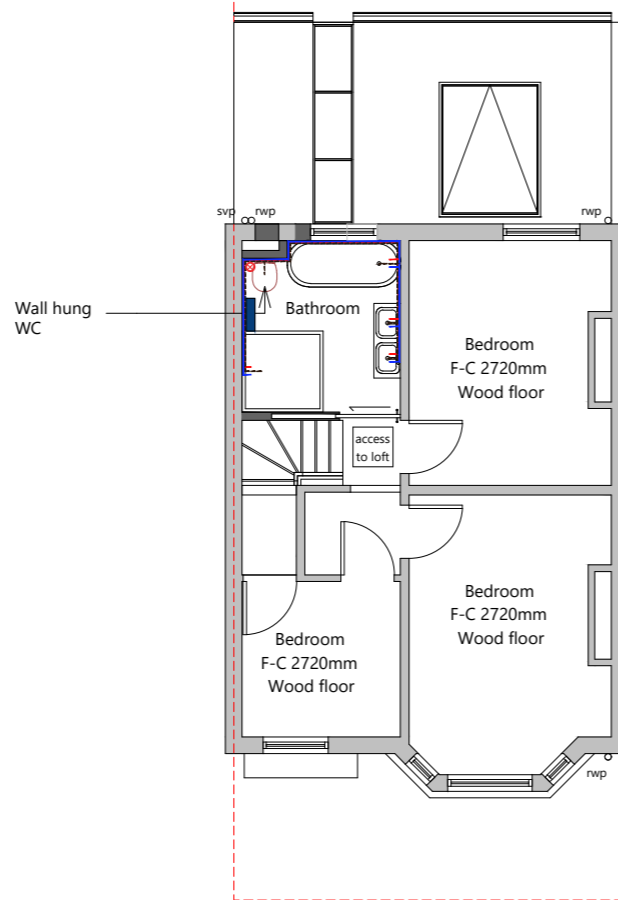
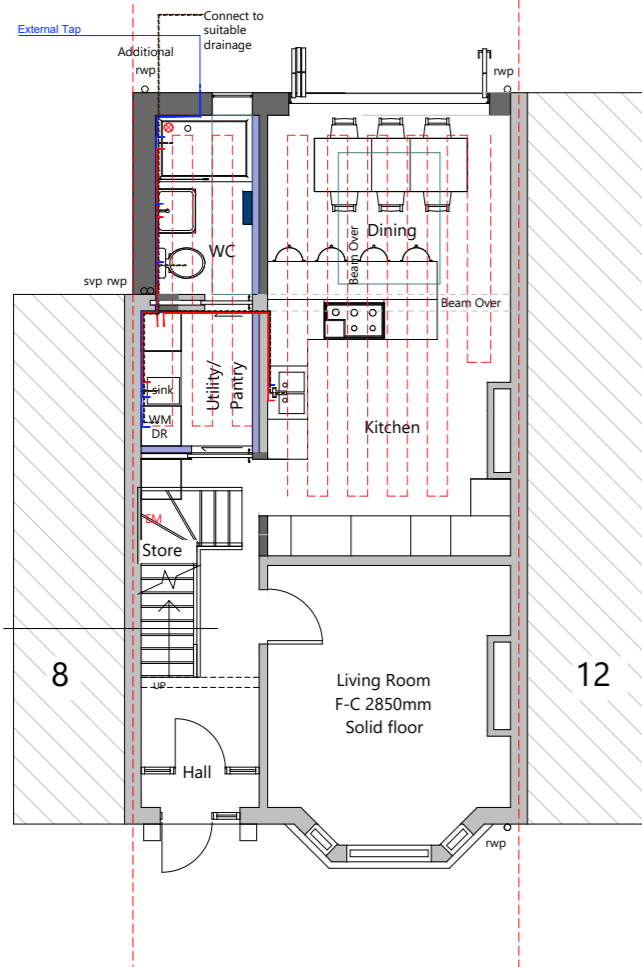













PROJECT ADDRESS

M & E P L A N S

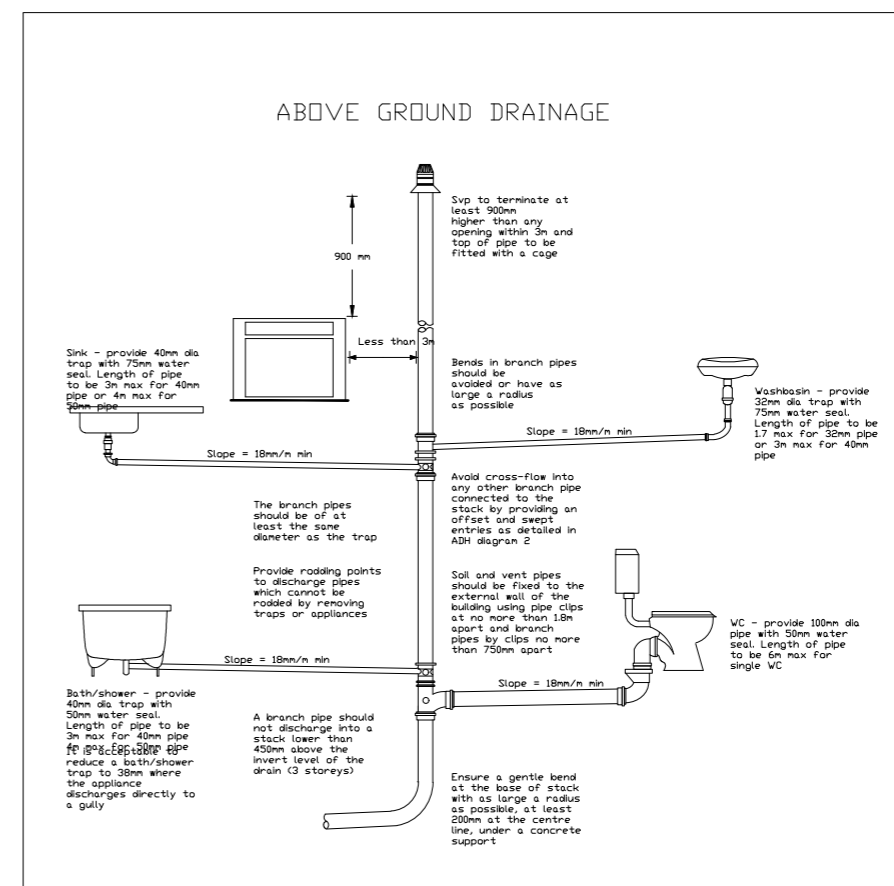
# PLUMBING PLAN



EXISTING SEWER	
PROPOSED SEWER	
HOT WATER	
COLD WATER	
EXISTING RADIATOR	
NEW RADIATOR	
NEW TOWEL RAIL	
MECHANICAL EXTRACTION UNIT	
UNDERFLOOR HEATING	

New Radiator BTU calculation to be carried out by heating engineer

Final positioning to be adjusted accordingly with the existing, new furniture and in conjunction with the manufacturers specifications.



LINEAR SCALE 1:50 & 1:100

LINEAR SCALE 1:50 & 1:100

Site address 10 Trelawn, London, E10 5QD

project details M & E

revision No. **B**

drawn by SB

drawing type SOW

date Mar 03

drawing no MEC 01 - 10 TR - B

checked by O.P.N

client ref

1:100 @ A3 page

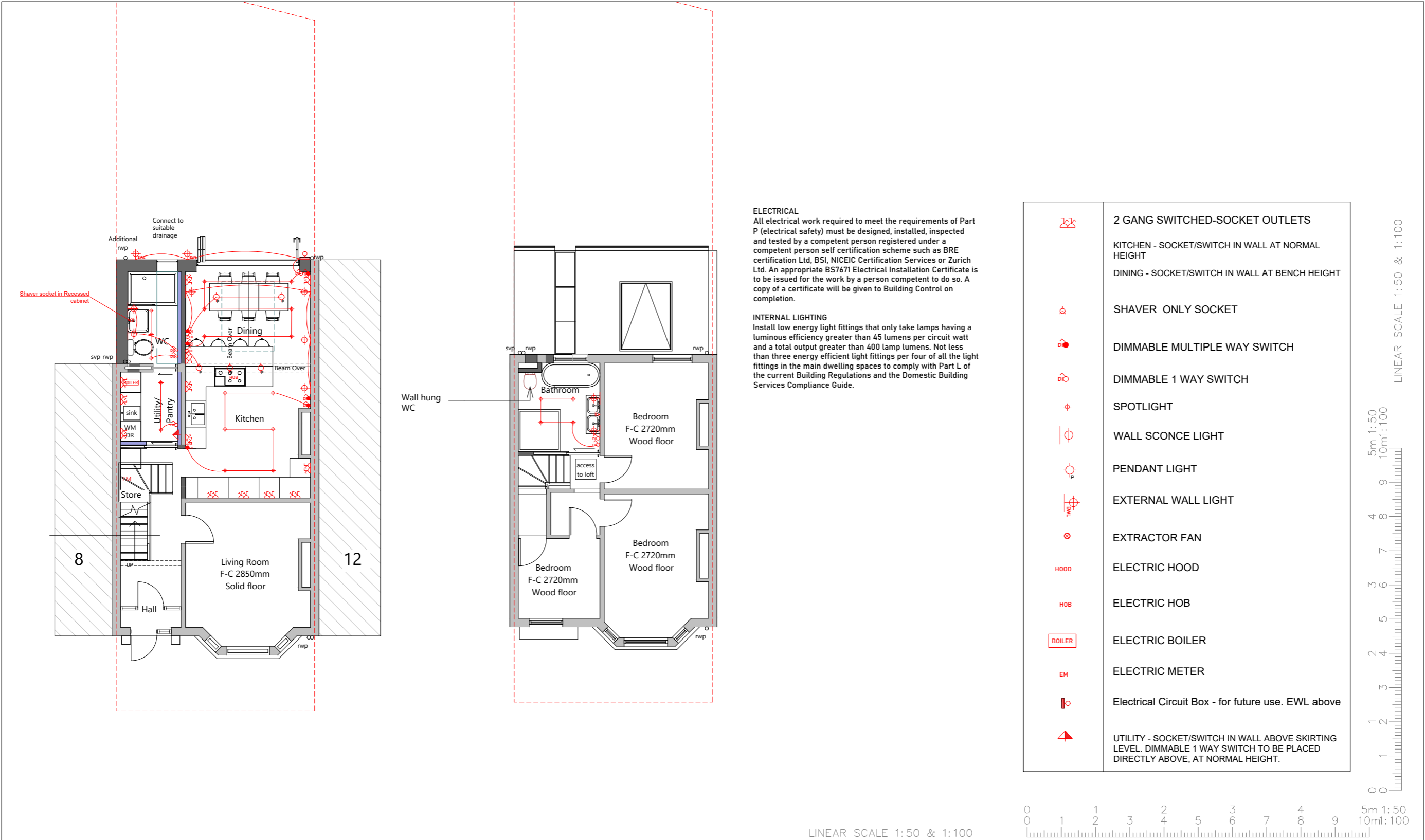
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ELECTRICAL PLAN

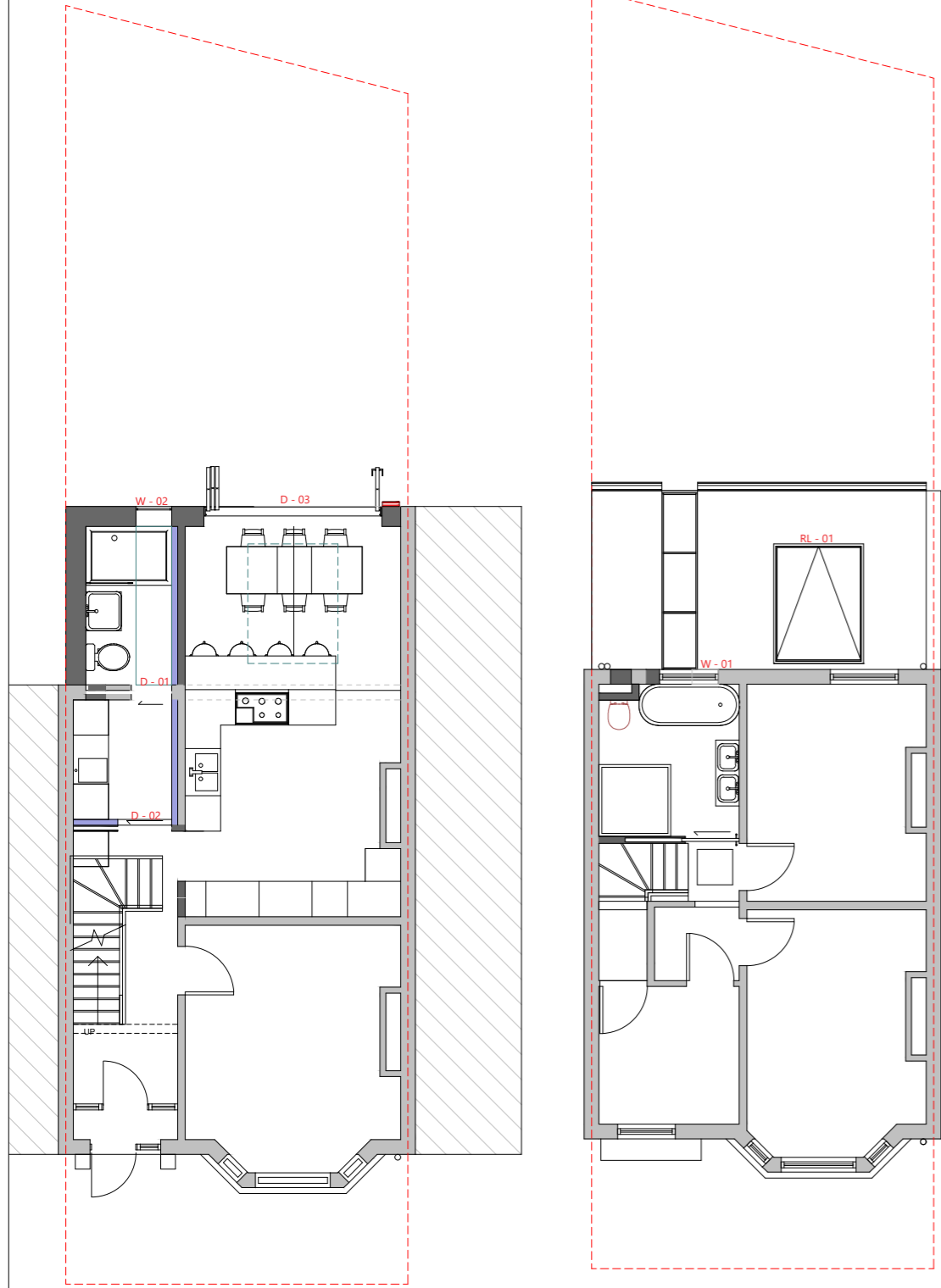


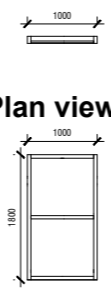
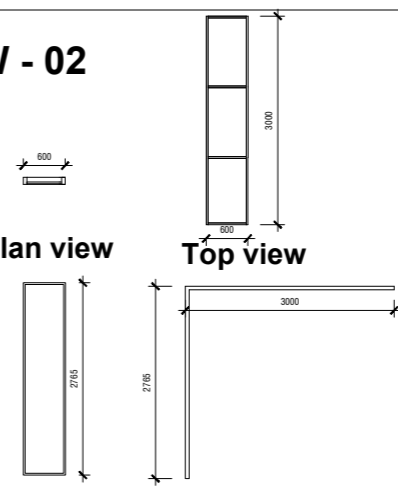
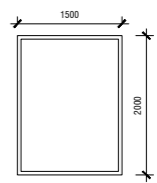
Site address	10 Trelawn, London, E10 5QD	project details	M & E	revision No.	C	1:100 @ A3 page	This drawing is protected under copyright
		drawn by	SB	drawing type	SOW		
		date	Mar 04	drawing no	EL 01 - 10 TR - C		
		checked by	O.P.N	client ref			
						Go Plans hello@goplans.co.uk 20-22 Wenlock Rd London N1 7GU	

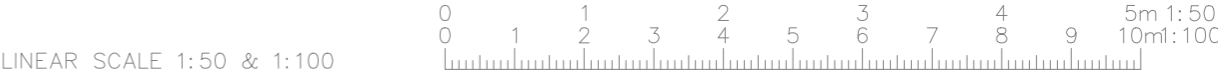
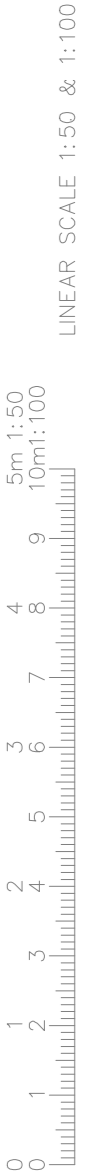
PROJECT ADDRESS

DOOR & WINDOW PLAN





Proposed Windows Schedule		Scale - 1: 100
( Final Measurements TBC On Site)		
<div><div>W - 01</div><div></div><div>Plan view</div><div>Elevation view</div></div>	<div><div>W - 02</div><div></div><div>Plan view</div><div>Top view</div><div>Rear view</div><div>Side view</div></div>	<div><div>RL - 01</div><div></div></div>
Quantity x 01	Quantity x 01	Quantity x 01
New External Glass Window	New External Glass Window	New Rooflight
Window Size - 1000mm x 1800mm Style and color TBC with SOW	Style and color TBC with SOW	



Site address 10 Trelawn, London, E10 5QD

project details DaW

drawn by SB

date Mar 14

checked by O.P.N

revision No. A

drawing type SOW

drawing no EL 01 - 10 TR - A

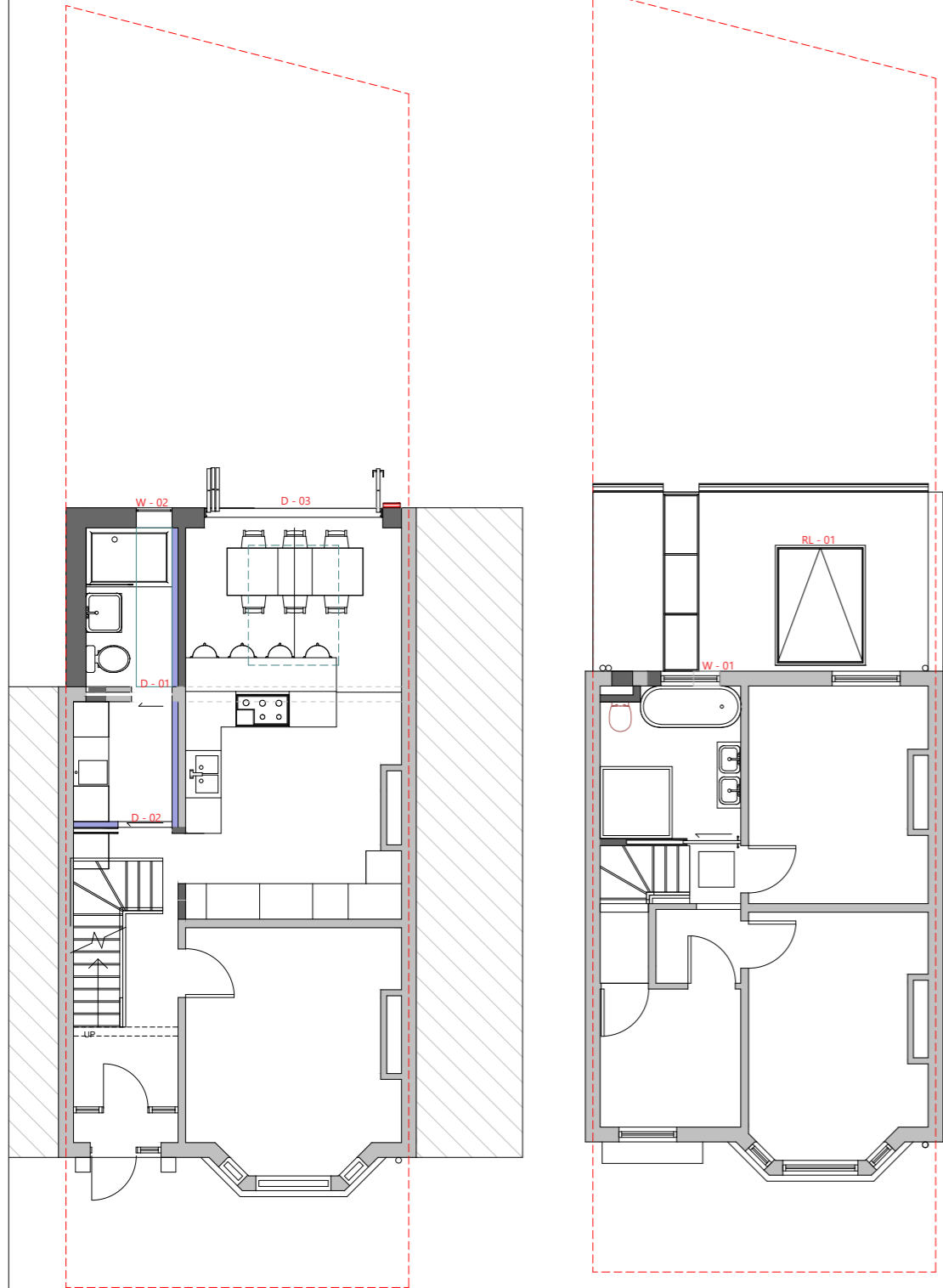
client ref

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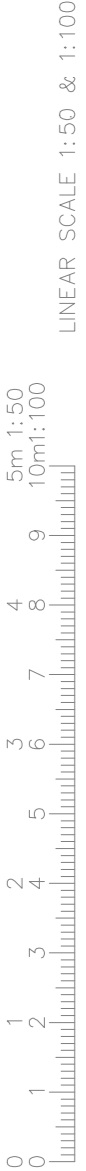




Proposed Doors Schedule Scale - 1: 100 ( Final Measurements TBC On Site)  
( Fire Rated Door TBC On Site With Building Regulation )

D - 01	D - 02	D - 03
<p><b>Plan view</b></p> <p><b>Elevation view</b></p>	<p><b>Plan view</b></p> <p><b>Elevation view</b></p>	<p><b>Plan view</b></p> <p><b>Elevation view</b></p>
Quantity x 01	Quantity x 01	Quantity x 01
New Internal Single Panel Pocket Door	New Internal Single Panel Pocket Door	New External Bi - Fold Door
Door Size - 686mm x 1981mm	Door Size - 762mm x 1981mm	
Clear Opening - 635mm x 1970mm	Clear Opening - 711mm x 1970mm	
Structural Opening - 1390mm x 2050mm	Structural Opening - 1545mm x 2050mm	Structural Opening - 3000mm x 2100mm
Style and color TBC with SOW	Style and color TBC with SOW	Style and color TBC with SOW

LINEAR SCALE 1:50 & 1:100



Site address 10 Trelawn, London, E10 5QD

project details DaW

drawn by SB

date Mar 14

checked by O.P.N

revision No. A

drawing type SOW

drawing no EL 01 - 10 TR - A

client ref

1:100 @ A3 page

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## PROJECT ADDRESS

FIXTURES, FITTINGS  
& FINISHES

# G R O U N D F L O O R



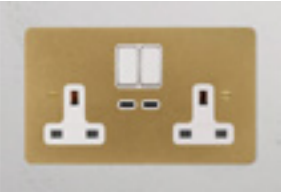





GF Kitchen/Dining Room


GF Utility Room

GF Bathroom





KITCHEN/DINING ROOM

PRODUCT	PRODUCT NAME	PRODUCT LINK	BUILDER SUPPLY?
	<b>InfiniGlide6 Sliding Doors</b>	<a href="https://www.finepoint.glass/aluminium-sliding-doors-london/#infiniglide-6">https://www.finepoint.glass/aluminium-sliding-doors-london/#infiniglide-6</a>	YES
	<b>COR Vision Plus Sliding(alternative door option)</b>	<a href="https://www.cortizo.com/en/sistemas/quenecesitas/grandes_dimensiones/93/cor-vision-plus-sliding.html">https://www.cortizo.com/en/sistemas/quenecesitas/grandes_dimensiones/93/cor-vision-plus-sliding.html</a>	YES
	<b>Double Socket with USB-C Fast Charge</b>	<a href="https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique-brass-white">https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique-brass-white</a>	NO
	<b>Antique Brass triple dimmer switch</b>	<a href="https://www.dowsingandreynolds.com/shop/antique-brass-triple-dimmer-switch/">https://www.dowsingandreynolds.com/shop/antique-brass-triple-dimmer-switch/</a>	NO
LIGHTING	<b>LED downlights (white), task lighting (pendants) over kitchen peninsula &amp; dining table and wall sconces</b>		NO
HEATING	<b>Underfloor Heating</b>		N/A
	<b>Victorian 1 MDF Skirting Board</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/">https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/</a>	YES
	<b>Victorian 1 MDF Architrave</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/">https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/</a>	YES



KITCHEN/DINING ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
	<b>Sandbank Engineered Wooden Floor (Plank Style)</b>	<a href="https://www.tedtodd.co.uk/product/sandbank/">https://www.tedtodd.co.uk/product/sandbank/</a>	NO
WALLS	<b>Plasterboard &amp; skimmed</b>		YES
CEILING	<b>Plasterboard &amp; skimmed</b>		YES
CABINETRY	<b>No cabinets (we will source via family)</b>		N/A







UTILITY ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
DOORS	Pocket Door		YES
	Regent Recessed Small Pull	<a href="https://www.corston.com/products/regent-recessed-small-pull-antique-brass">https://www.corston.com/products/regent-recessed-small-pull-antique-brass</a>	NO
	Double Socket with USB-C Fast Charge	<a href="https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique-brass-white">https://www.corston.com/products/double-socket-with-usb-c-fast-charge-antique-brass-white</a>	NO
	Antique Brass double dimmer switch	<a href="https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch/">https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch/</a>	NO
	Calla - 2 light Calacatta marble and aged brass wall light	<a href="https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass-wall-light">https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass-wall-light</a>	NO
LIGHTING	LED Downlights		YES
HEATING	Underfloor Heating		N/A
FLOORING	TBC		





UTILITY ROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
	<b>Victorian 1 MDF Skirting Board</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/">https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/</a>	YES
	<b>Victorian 1 MDF Architrave</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/">https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/</a>	YES
FLOORING	<b>Calacatta Amber Honed Marble</b>	<a href="https://www.mandarinstone.com/product/calacatta-amber-honed-marble/">https://www.mandarinstone.com/product/calacatta-amber-honed-marble/</a>	NO
WALLS	<b>Plasterboard &amp; skimmed</b>		YES
CEILING	<b>Plasterboard &amp; skimmed</b>		YES
CABINETRY	<b>No cabinets</b>		N/A

BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
DOORS	Pocket door with lock		YES
	Regent Recessed Small Pull	<a href="https://www.corston.com/products/regent-recessed-small-pull-antique-brass">https://www.corston.com/products/regent-recessed-small-pull-antique-brass</a>	NO
	Regent Recessed Thumbturn	<a href="https://www.corston.com/products/regent-recessed-thumbturn-antique-brass">https://www.corston.com/products/regent-recessed-thumbturn-antique-brass</a>	NO
	50mm Hook Lock	<a href="https://www.corston.com/products/50mm-hook-lock-antique-brass">https://www.corston.com/products/50mm-hook-lock-antique-brass</a>	NO
	Shaver Socket	<a href="https://www.corston.com/products/shaver-socket-antique-brass-white">https://www.corston.com/products/shaver-socket-antique-brass-white</a>	NO
	Antique Brass double dimmer switch	<a href="https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch">https://www.dowsingandreynolds.com/shop/antique-brass-double-dimmer-switch</a>	NO
	Calla - 2 light Calacatta marble and aged brass wall light	<a href="https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass-wall-light">https://lightsandlamps.com/products/calla-2-light-calacatta-marble-and-aged-brass-wall-light</a>	NO
LIGHTING	LED Downlights		YES

BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
HEATING	<b>Underfloor Heating</b>		N/A
	<b>Victorian 1 MDF Skirting Board</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/">https://mdfskirtingworld.co.uk/victorian-1-mdf-skirting-board/</a>	YES
	<b>Victorian 1 MDF Architrave</b>	<a href="https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/">https://mdfskirtingworld.co.uk/victorian-1-mdf-architrave/</a>	YES
	<b>Arezzo Brushed Brass Concealed Individual Diverter + Thermostatic Control Valve with Handset + Wall Mounted Shower Head</b>	<a href="https://www.victorianplumbing.co.uk/arezzo-brushed-brass-concealed-individual-diverter-thermostatic-control-valve-with-handset-wall-mounted-shower-head">https://www.victorianplumbing.co.uk/arezzo-brushed-brass-concealed-individual-diverter-thermostatic-control-valve-with-handset-wall-mounted-shower-head</a>	YES
	<b>Arezzo Round Brushed Brass Wall Mounted (2TH) Basin Mixer Tap</b>		YES
WALL HUNG WC	<b>TBC</b>		YES
WALL HUNG VANITY	<b>TBC</b>		YES
CEILING	<b>Plasterboard &amp; skimmed</b>		YES

BATHROOM

PRODUCT	PRODUCT DESCRIPTION	PRODUCT LINK	BUILDER SUPPLY?
FLOORING	<b>Calacatta Amber Honed Marble</b>	<a href="https://www.mandarinstone.com/product/calacatta-amber-honed-marble/">https://www.mandarinstone.com/product/calacatta-amber-honed-marble/</a>	NO
WALLS	<b>Calacatta Amber Honed Marble</b>	<a href="https://www.mandarinstone.com/product/calacatta-amber-honed-marble/">https://www.mandarinstone.com/product/calacatta-amber-honed-marble/</a>	NO

## A D D I T I O N A L   I N F O R M A T I O N

- The client is only proceeding with the ground floor works at this stage, please exclude the first floor bathroom renovation.
- Garden works: External Tap (plumbing) and Lights, along with electrical box for future landscaping lighting (these lights have not been incorporatred on M&E drawings).

# SITE INFORMATION

PRE-CONSTRUCTION	
Can the contractor use site utilities (water/electric)?	YES
Builder to provide welfare facilities (inc. toilet)?	YES
Do you require a temporary kitchen setting up?	NO
Does the site require hoarding?	NO

EXTERNAL FINISHES	
Garden works?	YES
Make good around extension?	YES
Tarmac?	NO
Grass?	NO
Artificial grass?	NO

WALLS	
Brick finish?	YES
Render?	NO
Does the extension match?	YES

ROOFING	
Pitched roof tile type?	N/A
Flat roof type?	FELT

FASCIA AND GUTTER	
Would you like to match the existing fascia and guttering? If no, please specify desired finish	YES

SKYLIGHTS	
Does the project have skylights?	YES


EXTERNAL DOORS	
Which type of door would you like? Please specify	W&D PLANS
Would you prefer to supply the doors?	YES

WINDOWS	
Which type of windows would you like? Please specify	W&D PLANS
Would you prefer to supply the windows?	YES

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